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THERMODYNAMICS
STATISTICAL MECHANICS

PH332

1

Feb 6, 2019

Thermodynamics

- macroscopic properties of system P, V, T , etc
- used w/ system that are large enough that microscopic fluctuations can be ignored

Stat mech

- individual states of atoms / microscopic states of particles in system & use statistics to describe macroscopic behavior

This course focuses on systems of large numbers of particles.

Large? 1 mole $\rightarrow N_A = 6.022 \times 10^{23}$ particles \rightarrow Avogadro's #

Why need statistics? \rightarrow Ex Say we want to count # of particles in a mole of water.

3GHz $\rightarrow 3 \times 10^9 \text{ s}^{-1}$ count rate $\rightarrow 2 \times 10^{14} \text{ s} = 6.4 \times 10^6 \text{ yrs}$.
 \rightarrow needs stats models...

What is a mole?

\rightarrow A mole is the amount of matter that contains as much matter as 12g of ^{12}C

Molar mass

M: mass of 1 mole of a substance in grams.

Ex $M_{^{12}\text{C}} = 12 \text{ g/mol}$ $M_{\text{H}_2\text{O}} = 18 \text{ g/mol}$
 $M_{\text{He}} = 4 \text{ g/mol}$

Temperature

\rightarrow always use K. Don't use Fahrenheit.

Fahrenheit scale \rightarrow freezing point of water: 32°F
Boiling point of water: 212°F

Celsius \rightarrow 0°C
 100°C

$$^\circ\text{F} = 32 + \frac{9}{5}^\circ\text{C}$$

$$T_{(K)} = T_{(C)} + 273.15$$

What is temperature?

0th law of thermodynamics

IF A is in thermoequilibrium with B (A) ↔ (B)
 but C is in thermoequilibrium with B (B) ↔ (C)
 then A ... C (A) ↔ (C)
 → "thermoequilibrium" ≡ same T.

Temperature: a measure of how likely it is for a system to give up energy to another system. Generally, higher T → more likely to give off energy

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Ideal Gas Law

$$PV = nRT \quad \text{vs} \quad PV = NkT$$

n: # of moles R: Gas constant 8.31 J/moleK

N: # of particles k_B : Boltzmann Constant = 1.38×10^{-23} J/K

∴ $nR = Nk_B$

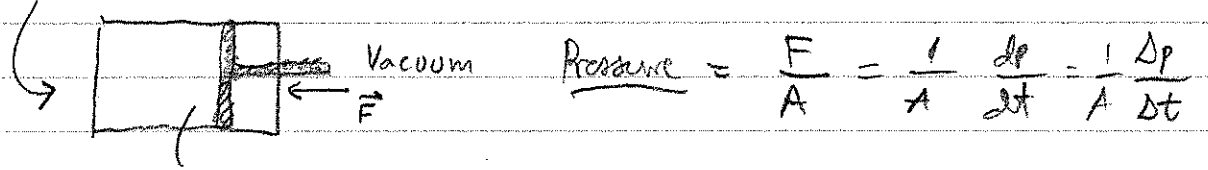
Note $N = nN_A$ ∴

$$R = N_A k_B$$

$$k_B = \frac{R}{N_A}$$

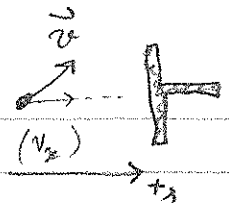
Assumptions: point-like particles, don't interact

How does temperature T of ideal gas relate to its KE?



* assume perfectly elastic collisions

(1) Change in momentum of single particle.

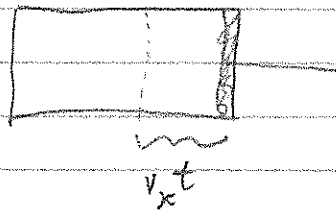


$$\Delta p = mv_f - mv_i$$

$$= -mv_x - mv_x = -2mv_x$$

∴ $\Delta p_{piston} = 2mv_x$

(2) # of collisions?



assume N molecules in volume V

→ density = $\frac{N}{V}$

∴ # of collisions = $\frac{N}{V} \cdot (v_x \cdot A)$

∴ # collision/sec = $\frac{N}{V} (v_x A)$

(3) Force on piston

$$F = \frac{\Delta p}{\Delta t} = (2mv_x) \left(\frac{N}{V} v_x A \right)$$

$$= 2mv_x^2 \frac{N}{V} A$$

∴
$$p = \frac{F}{A} = 2mv_x^2 \frac{N}{V}$$

Now, corrections. Not all particles have the same v_x

→ $\langle v_x^2 \rangle$ instead of v_x . Also, $\frac{1}{2}$ of particles are moving in the other direction ($-v_x$) → divide by 2

∴
$$p = m \langle v_x^2 \rangle \frac{N}{V}$$

Now $v^2 = v_x^2 + v_y^2 + v_z^2$

⇒
$$pV = m \langle v_x^2 \rangle N$$

⇒ Assume $\langle v_i^2 \rangle$ equal

⇒
$$\frac{1}{3} \langle v^2 \rangle = \langle v_x^2 \rangle$$

So $PV = NkT = \frac{1}{3} m \langle v^2 \rangle N$ ~~is~~ $= \frac{2}{3} \left[\frac{1}{2} m \langle v^2 \rangle \right] N$

So $kT = \frac{2}{3} \langle KE \rangle$

So $\langle KE \rangle = \frac{3kT}{2}$

Average speed of the particles?

Naively $\frac{1}{2} m \langle v^2 \rangle = \frac{3}{2} kT$ (g), not $M = m/N_A^{-1}$

$\rightarrow \langle v^2 \rangle = \frac{3kT}{m}$

So $v_{rms} = \sqrt{\langle v^2 \rangle} = \sqrt{\frac{3kT}{m}}$

But this is NOT $\langle v \rangle$

$\langle v \rangle = \sqrt{\langle v_x^2 \rangle + \langle v_y^2 \rangle + \langle v_z^2 \rangle}$

We will (can) show that

But $\sqrt{\langle v^2 \rangle} = \sqrt{\langle v_x^2 \rangle + \langle v_y^2 \rangle + \langle v_z^2 \rangle}$
 v_{rms}

$\langle v \rangle = \sqrt{\frac{8kT}{\pi m}} < v_{rms}$

Ex Find rms v of N_2 molecules at room temp, $\sim 300K$

$v_{rms} = \sqrt{\frac{3k \cdot 300}{28/N_A}}$

or $v_{rms} = \sqrt{\frac{3kT}{m}} = \sqrt{\frac{3nRT}{nM}} = \sqrt{\frac{3RT}{M}} \approx \sqrt{\frac{3 \cdot 8.31 J/mol \cdot K \cdot 300K}{28g/mol}}$

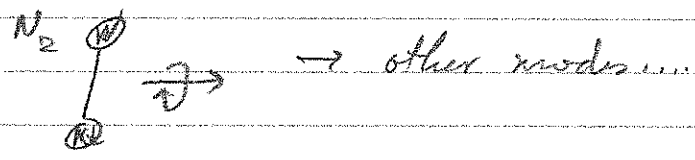
Now $28g/mol = 28 \times 10^{-3} kg/mol \rightarrow v_{rms} \approx 517 m/s$

What's the total thermal energy of a gas? ^{or internal}

$$U = \frac{3}{2} kT \cdot N = \langle KE \rangle N$$

but only true for monatomic ideal gas
↳ like noble gas.

Why? Degrees of freedom



If translational motion is not the only contributing factor

↳ Equipartition theorem

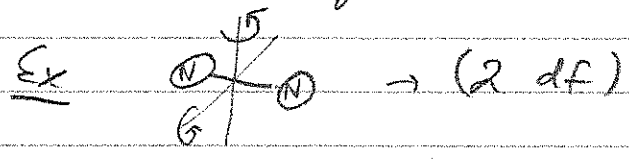
At same temp T, the average energy for every quadratic degree of freedom = $\frac{1}{2} kT$
↳ ex. $\frac{1}{2} m \langle v_x^2 \rangle$

So
$$U_{\text{thermal}} = Nf \frac{1}{2} kT \quad f = \# \text{ of quadratic df.}$$

Degrees of freedom

↳ for a gas

- ↳ translational : x, y, z (3 df)
- ↳ Rotational : how many axes of rotations introduce asymmetry?



\underline{Ex}  $\rightarrow (3 df)$

• vibrational $(N) \text{---} \text{---} (N)$ \rightarrow classical mech tells us this

$\langle KE \rangle = \langle PE \rangle$ for SHO \rightarrow 2 degrees of freedom, both quadratic.

\rightarrow at normal temp \rightarrow small effect. Most diatomic molecules only have (5) df at typical room temp, as vibr. df are frozen out.

$\rightarrow U_{\text{thermal } N_2} \approx N \cdot \left(\frac{3+2+0}{2} \right) kT$

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Heat = Work \rightarrow Exchange in energy

Last time $U = \frac{f}{2} N kT$

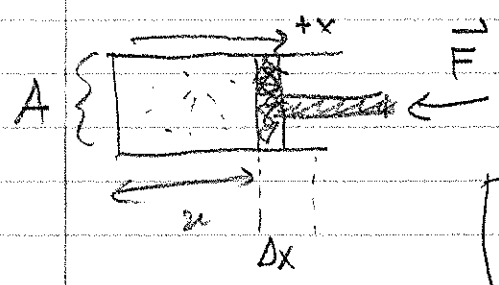
{ Heat (Q) \rightarrow spontaneous flow of energy from one system to another due to a ΔT }

So $\text{if } \Delta T \neq 0, \text{ then } Q \neq 0$ (Heat) Spontaneously

{ Work \rightarrow (W) non-spontaneous transfer of energy \rightarrow need an "agent" to transfer energy } }

Heat & Work are not intrinsic to system. \rightarrow they're processes.

Compression work



$P = \frac{F}{A}$ positive, since $\Delta x < 0$

$W_{\text{on gas}} = -F\Delta x = -P\Delta x = -P\Delta V$

So $W_{\text{on gas}} = -P\Delta V$

Should use differentials, but they are not exact difs. because of path-dependence.

$$W = \int_p \vec{F} \cdot d\vec{r}$$

A differential is exact if $\exists f = f(x,y)$ such that

$$df = \left(\frac{\partial f}{\partial x}\right)_y dx + \left(\frac{\partial f}{\partial y}\right)_x dy$$

→ True for conservative vector fields $\vec{v} = \nabla f$

$$A = \frac{\partial f}{\partial x}$$

$$B = \frac{\partial f}{\partial y}$$

In other words, $df = A dx + B dy$ exact diff. if

$$\vec{\nabla} \times [A, B] = \begin{vmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \\ A & B \end{vmatrix} = \frac{\partial^2 f}{\partial x \partial y} - \frac{\partial^2 f}{\partial y \partial x} = 0$$

Can use Euler's test to determine if we have an exact diff.

let $df = A dx + B dy$

check if $\frac{\partial A}{\partial y} = \frac{\partial B}{\partial x} \rightarrow \text{Yes?} \rightarrow \text{Exact}$

\downarrow No? \rightarrow Not exact

Inexact differentials are written as \rightarrow dW or dQ

\hookrightarrow path-dependence!

Irreversible differentials can become exact by multiplying by some integrating factor.

e.g. $\left\{ \begin{array}{l} \frac{dw}{P} = dV \rightarrow \text{volume} \quad dV \rightarrow \text{exact diff} \\ \frac{dq}{T} = ds \rightarrow \text{entropy} \quad ds \rightarrow \text{exact diff} \end{array} \right.$

If Q & W are the only ways energy is transferred, their conservation of energy

$\Delta U = Q + W_{on} \rightarrow 1^{st} \text{ law of thermodynamics}$

Q : heat added to system, W : work done on system

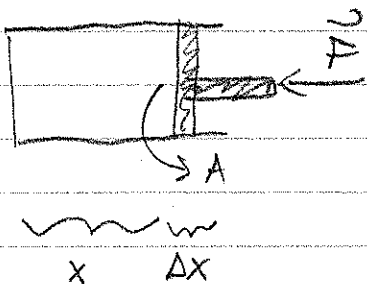
In differential $\rightarrow dU = \delta Q + \delta W_{on} = \delta Q - \delta W_{by}$

Units of energy $\rightarrow 1 \text{ J} \rightarrow 1 \text{ kg m}^2/\text{s}^2$

$1 \text{ cal} \rightarrow 4.186 \text{ J}$

$1 \text{ cal} \rightarrow \neq$ heat needed to raise 1 g of H_2O by 1 C or 1 K

Compression Work



$W_{on} = -F\Delta x \stackrel{?}{=} -PA\Delta x$

let $P \rightarrow P(V)$

Before, we assumed that P is constant over the process \rightarrow assumed piston movement was slow

Quasi-static process → slow process, allow P to equilibrate

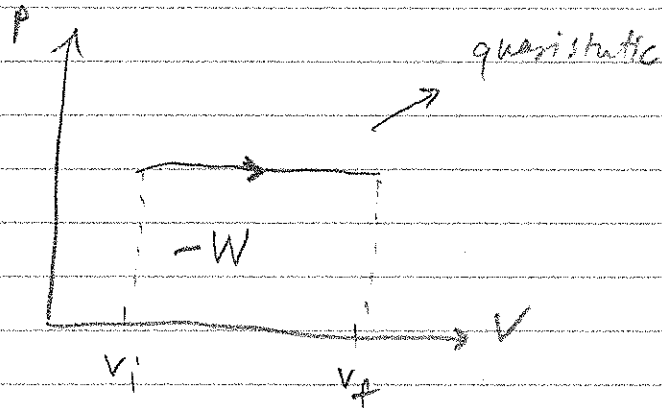
↳ $W_{on} = -P\Delta V$ or $dW_{on} = PdV$

Note there is heat flow in quasi-static process

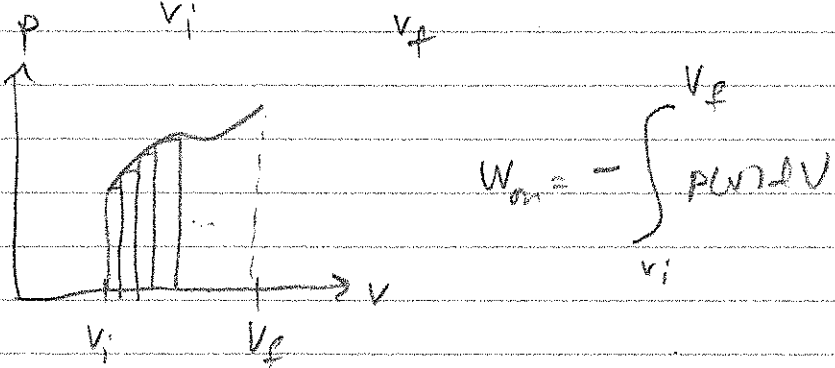
▣ We often consider infinitesimal changes that are each quasi-static & then integrate

$$W_{on} = - \int_{V_i}^{V_f} P(V) dV$$

P-V diagrams

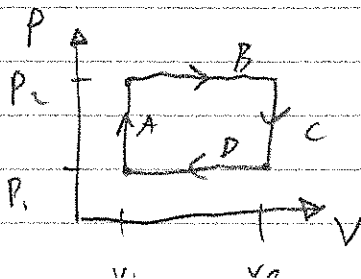


Non quasi-static



Example of PV diagram

Interpreting PV diagrams



An ideal diatomic gas (N_2)

For steps $A \rightarrow D$, we want to determine W_{on} , Q_{add} , ΔU , and W_{total} or Q_{tot}

	A	B	C	D	Σ
W_m	0	$P_2(V_1 - V_2)$	0	$P_1(V_2 - V_1)$	< 0
Q	$\frac{f}{2} V_1 (P_2 - P_1)$	$\frac{f}{2} P_2 (V_2 - V_1)$	\vdots	\vdots	> 0
ΔU	$\frac{f}{2} V_1 (P_2 - P_1)$	$\frac{f}{2} P_2 (V_2 - V_1)$	\vdots	\vdots	0

A: $W = 0, \Delta U = \frac{f}{2} NkT = \frac{f}{2} Nk \frac{PV}{Nk} = \frac{f}{2} PV$

$\int_0^1 \Delta U_A = \frac{f}{2} V_1 \Delta P$

$\Delta U = Q + W$

B $\Delta U = \int P dV = \int P_2 (V_2 - V_1)$

$Q = \Delta U - W = \int P_2 (V_2 - V_1) - P_2 (V_1 - V_2)$

Note $\left\{ \begin{array}{l} W_{on, total} < 0 \\ \Delta U = 0 \end{array} \right. \quad Q > 0$

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Quasistatic review "slow" \rightarrow so that system can equilibrate
 \rightarrow pressure is uniform over system

$W_{on} = -F\Delta x \rightarrow -P\Delta V$

Not-quasistatic "fast" \rightarrow pressure depends on position

Compression of an ideal gas

Isothermal compression

"slow" compression such that $T = \text{constant}$

Temp down + increase
 $\rightarrow Q$ leaves system $\rightarrow \Delta U = 0$

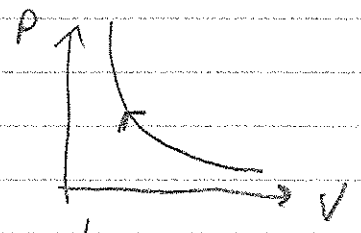
$\Delta U = W_m + Q_{add}$

Adiabatic compression → "fast" compression. So fast that no heat can escape

$Q=0$ $\int \Delta U = W_{on} + Q_{add} = W_{on}$

Temp increases

P-V diagram



Isothermal process → Quasistatic

$W_{on} = - \int_{V_i}^{V_f} P(V) dV = - \int_{V_i}^{V_f} \frac{NkT}{V} dV$

$PV = \text{const}$

$= -NkT \int_{V_i}^{V_f} \frac{dV}{V}$

$W_{on} = -NkT \ln \left(\frac{V_f}{V_i} \right)$

Work done on system in isothermal compression.

Since T does not increase, how much heat is lost?

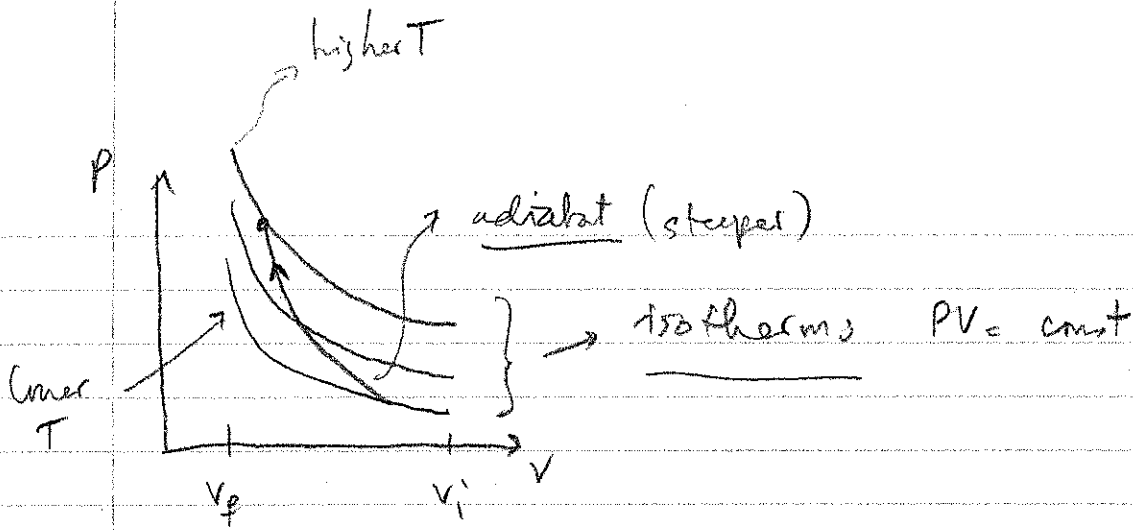
$\Delta U = W_{on} + Q_{add} = 0$ or $W_{on} = Q_{out}$

\downarrow
 dT

$Q_{add} = -W_{on} = NkT \ln \left(\frac{V_f}{V_i} \right)$

Adiabatic process → fast

Assume quasistatic process... $\Delta U = W_{on} + Q_{add}$
By definition of adiabatic → $Q=0$ } → $\Delta U = W_{on}$



How different parameters change during adiabatic compression?

↳ Ideal gas $\Delta U = W + Q = W$

$$U = \frac{f}{2} NkT \rightarrow dU = \frac{f}{2} Nk dT = dW = -PdV$$

$$\int \frac{f}{2} Nk dT = - \frac{NkT}{V} dV$$

$$\int \frac{f}{2} \frac{dT}{T} = - \int \frac{dV}{V}$$

$$\int \frac{f}{2} \ln\left(\frac{T_f}{T_i}\right) = - \ln\left(\frac{V_f}{V_i}\right)$$

$$\left(\frac{T_f}{T_i}\right)^{f/2} = \left(\frac{V_f}{V_i}\right)^{-1} \rightarrow V_i T_i^{f/2} = T_f^{f/2} V_f$$

$\int VT^{f/2} \rightarrow \text{constant}$ → adiabatic compression/expansion of ideal gas

Can write this in volume & pressure

$$T = \frac{PV}{Nk} \rightarrow V \cdot \left(\frac{PV}{Nk}\right)^{f/2} \rightarrow \text{constant}$$

$$\rightarrow P^{f/2} V^{1+f/2} \rightarrow \text{constant}$$

$$\rightarrow PV^{(1+f/2)/f/2} \rightarrow \text{constant}$$

$$\Rightarrow PV^{1+2/f} = \text{constant}$$

$$\text{Call } \gamma = 1 + \frac{2}{f} = \frac{f+2}{f}$$

$$\Rightarrow PV^\gamma = \text{constant}$$

We call $\gamma \rightarrow$ "adiabatic exponent" $\gamma = \frac{f+2}{f}$

$$\gamma = \frac{f+2}{f} \quad \underline{C_0} \quad \left. \begin{array}{l} PV^\gamma = \text{constant} \\ VT^{1/\gamma-1} = \text{constant} \end{array} \right\}$$

Now, pressure & temp.

$$\hookrightarrow \underline{V^\gamma P = \text{constant}} \quad \downarrow \quad \underline{V^{-\gamma} T^{-\gamma/(\gamma-1)} = \text{constant}}$$

$$\underline{\underline{\delta}} \quad (V^\gamma P)(V^{-\gamma} T^{-\gamma/(\gamma-1)})$$

$$= PT^{-\gamma/(\gamma-1)} \text{ constant}$$

$$\underline{\underline{\delta}} \quad \boxed{P^{1-\gamma} T^\gamma \text{ constant}}$$

Ex Diesel engine (no spark plugs...)

↳ atm air is quickly compressed to 1/20 original volume
→ Estimate temp of air in cylinder...

Well $\frac{V_f}{V_i} = \frac{1}{20}$ • assume ideal gas (diatomic $\rightarrow f=5$)

Ok $VT^{f/2} = \text{constant}$

↳ $\left(\frac{T_f}{T_i}\right)^{5/2} = \left(\frac{1}{20}\right)^{-1} = 20$

$$\underline{\underline{\delta}} \quad T_f = \sqrt[5/2]{20 T_i^{5/2}} = \sqrt[5/2]{20} T_i$$

~ 3 $\nearrow \sim 300$

$\underline{\underline{\delta}} \quad \boxed{T_f = 1000\text{k} > 700^\circ\text{C}}$

→ hot enough to ignite Diesel without spark plug.

Heat capacity

↳ the amount of heat necessary to raise a substance by 1°C

$$C \equiv \frac{Q}{\Delta T}$$

$$Q = C \Delta T = mc \Delta T$$

Specific heat capacity

$$c \equiv \frac{C}{m}$$

First recall → $Q_{in} = \Delta U - W_{out}$, limiting case → $W = 0$
→ no change in V
get heat capacity at constant volume, C_v

not the most physical

$$C_v = \frac{\Delta U - W}{\Delta T} = \frac{\Delta U}{\Delta T} = \left(\frac{\partial U}{\partial T} \right)_{V \text{ constant}}$$

Ex for 1g of H_2O $C_v = 1 \text{ cal/K}$

Feb 13, 2019

Heat Capacity

limiting cases → $W = 0, \Delta V = 0 \rightarrow C_v = \frac{\Delta U - W}{\Delta T} = \left(\frac{\partial U}{\partial T} \right)_{V \text{ const}}$
↳ Constant volume
↳ Constant pressure

Heat capacity at constant pressure

$$C_p = \frac{Q}{\Delta T} = \frac{\Delta U - W}{\Delta T} = \left(\frac{\Delta U - (-P \Delta V)}{\Delta T} \right)_{p \text{ const}}$$

$$C_p = \left(\frac{\partial u}{\partial T} + p \frac{\partial v}{\partial T} \right)_{p \text{ const}}$$

heat needed to compensate for expansion

Note $\left(\frac{\partial u}{\partial T} \right)_p \approx \left(\frac{\partial u}{\partial T} \right)_v \rightarrow$

(energy loss at work due to expansion)

Suppose we have a system that obeys equipartition theorem

$$U = \frac{fNR}{2}T$$

if we can measure C_v then we can find f .

Press $C_v = \left(\frac{\partial U}{\partial T}\right)_{V \text{ constant}} = \frac{fNR}{2}$

Ex

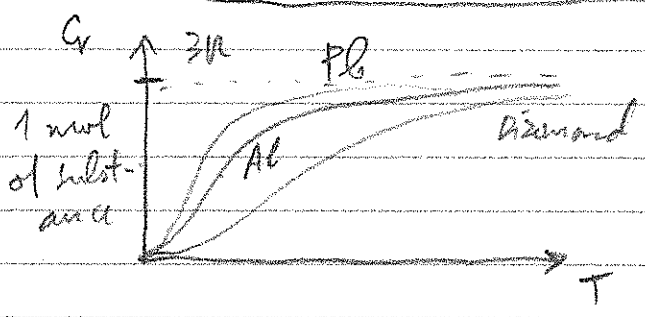


Consider solids/crystal no rotation/translation

→ only it is rotation.

→ Solid should have 6 d.o.f

$C_v = \frac{6}{2}NR = 3NR = 3nR$ → for solids



Heat capacity at constant pressure for ideal gas.

$$C_p = \left(\frac{\partial U}{\partial T}\right)_p + \left(p \frac{\partial V}{\partial T}\right)_p$$

↓ obeys eq. partition.

$$= \frac{fNR}{2} + p \frac{\partial}{\partial T} \left[\frac{NRT}{p} \right]$$

$$nR = C_v + NR = C_p = \frac{p}{2}NR + NR$$

Recall $\gamma = \frac{f+2}{f} = 1 + \frac{2}{f}$

$$= \left(\frac{p}{2} + 1\right)NR$$

$$\rightarrow \gamma - 1 = \frac{2}{f}$$

$$C_p = \frac{\gamma}{\gamma - 1} NR$$

$$\frac{p}{2} + 1 = \frac{1}{\gamma - 1} + 1$$

Recall the Adiabatic exponent γ

Definition

$$\gamma \equiv \frac{C_p}{C_v} = \frac{C_v + nR}{C_v} = \frac{f/2 + 1}{f/2} = \frac{2+f}{f}$$

Example of heat capacity

Heat capacity of a star

Well $U_{pot} = -\frac{GMm}{r}$ $KE = \frac{1}{2}mv^2$ $v = \sqrt{\frac{GM}{r}}$

Σ

$$K = \frac{1}{2} m \frac{GM}{r}$$

Virial Theorem

$$\rightarrow U_{tot} = U_{pot} + KE = \frac{1}{2} m \frac{GM}{r} - \frac{GMm}{r} = -\frac{1}{2} \frac{GMm}{r}$$

\downarrow
-2KE

$$\rightarrow U_{pot} = -K = -\frac{1}{2} \frac{GMm}{r}$$

Star H gas (3 d.f.)

obeys eq. part. then $K = \frac{1}{2}mv^2 = \frac{f}{2} NkT = \frac{3}{2} NkT$ quadratic

Σ

$$U_{tot} = -\frac{3}{2} NkT$$

Σ

$$C_v = \left(\frac{\partial U}{\partial T} \right)_v = -\frac{3}{2} Nk \rightarrow \text{negative heat capacity}$$

\hookrightarrow So, as a star radiates ϵ , it gets hotter.

Latent heat → useful for phase transitions.

e.g. melting ice Solid → liquid → Vapor

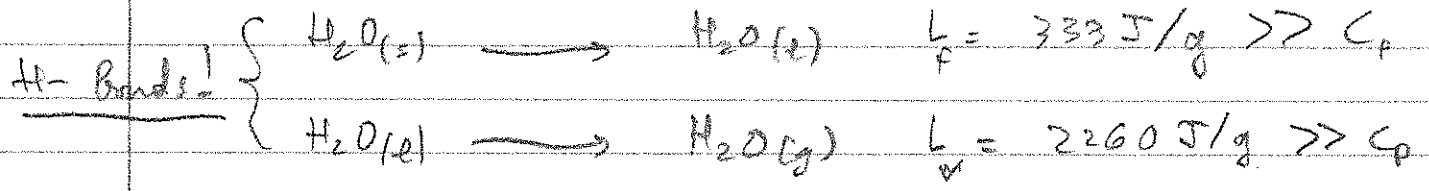
Note temperature stays constant during phase transitions.

↳ need to know how much heat is needed to complete phase transitions.

latent heat $L \equiv \frac{Q}{m}$

- Assume that $P = \text{constant}$ over phase transitions
- Assume that no other work besides expansion/compression

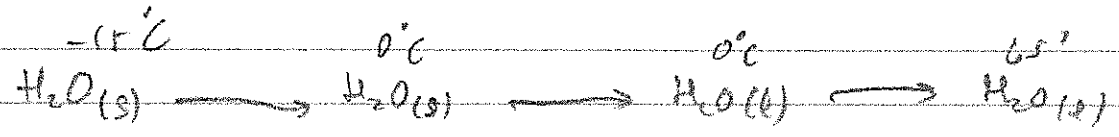
Ex latent heat of fusion



Ex 200g cup of tea that is @ boiling pt (212°F / 100°C)
 & wants to cool down to drink... 150°F ~ 65°C
 How much ice do we want?

$T_{ice, i} = -15^\circ\text{C}$ $C_{ice} = 0.5 \text{ cal/gC}$
 $C_{\text{H}_2\text{O}(l)} = 1 \text{ cal/gC}$ $L_f = 80 \text{ cal/g}$

@ (lost tea) = $m_{\text{tea}} \Delta T C_{\text{H}_2\text{O}} = 200 (100 - 65) 1 \text{ cal} = 7000 \text{ cal}$



7000 cal = $m C_{ice} \Delta T + L \cdot m + m C \Delta T$

$$\underline{Ex} \quad m = \frac{7000 \text{ cal}}{C_{ice}(0 - (-15)) + L + (65 - 0) C_{H_2O(l)}} \approx 46 \text{ g of ice}$$

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Enthalpy \rightarrow total heat content of a system

$$\boxed{H \equiv U + PV} \rightarrow \text{useful for constant } P \text{ processes}$$

H is useful for constant - pressure processes.

Ex Add heat to a system at constant pressure, then U, V, H change.

$$\underline{Ex} \quad H + \Delta H = U + \Delta U + P(V + \Delta V)$$

$$H + \Delta H = \underbrace{(U + PV)}_H + (\Delta U + P\Delta V)$$

$$\underline{Ex} \quad \boxed{\Delta H = \Delta U + P\Delta V} \rightarrow \text{@ constant pressure.}$$

First law $\Delta U = Q + (-P\Delta V)$ \rightarrow Compression work $\rightarrow + W_{\text{other}}$

then $\Delta H = \Delta U + P\Delta V = Q + W_{\text{other}}$

$$\underline{Ex} \quad \boxed{\Delta H = Q_{\text{add}} + W_{\text{other}}} \rightarrow \text{true for constant } P \text{ processes.}$$

Heat capacity at constant pressure

$$\boxed{C_p = \left(\frac{\partial H}{\partial T} \right)_P}$$

Examples ΔH for boiling H_2O (phase transition...)

$$\Delta H = 40660 \text{ J/mol at 1 atm, } 298\text{K}$$

$$\Delta H = \frac{40660 \text{ J/mol}}{18 \text{ g/mol}} \approx 2260 \text{ J/g} = L_{H_2O}$$

↳ latent heat of vaporization

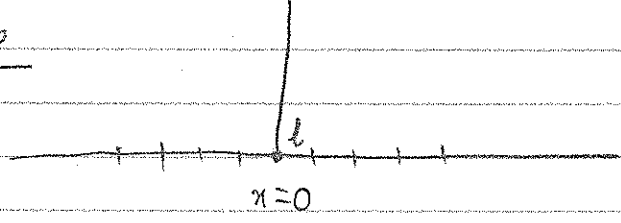
How much work is needed to create space for H_2O vapor.

$$V_i = 0 \quad V_f \approx \frac{nRT}{P} = \frac{RT}{P} \quad (n=1)$$

$$\Delta V = \frac{RT}{P} \rightarrow W = P\Delta V = RT = \frac{8.314 \text{ J}}{\text{mol K}} \cdot 298\text{K} \approx 2478 \text{ J}$$

Statistics

Random Walk problem



$$\begin{cases} P(\text{left}) = 1-p = q \\ P(\text{right}) = p \end{cases}$$

Final position $x = ml$ after N total steps where N, m are integers. $-N \leq m \leq N$

↳ $P_N(m)$ = Probability of finding our drunk at $x = ml$ after N steps.

$$\begin{cases} n_R = \# \text{ steps to } R \\ n_L = \# \text{ steps to } L \end{cases} \quad N = n_R + n_L$$

And $m = n_R - n_L = n_R - (N - n_R) = -N + 2n_R$

Probability of any sequence of steps (ass. independence) is the products

$$p^{n_R} (1-p)^{n_L} = p^{n_R} (1-p)^{N-n_R}$$

But there are many ways of taking N steps with $n_R = n_L$
 The number of ways is called "Multiplicity", Ω
 \hookrightarrow "# of microstates"

$$\Omega = \frac{N!}{n_1! n_2!} = C_{n_R}^N$$

Say there are N objects \rightarrow N! permutations. But this is only true for distinguishable objects, since order matters.

What about the # of ways N objects can be arranged into n_R spaces? where $n_R < N$

$$\hookrightarrow P_{n_R}^N = (N)(N-1) \dots (N-n_R) \dots (N-n_R+1) \dots (N-n_R+1) \dots (N-n_R+1)!$$

If we have indistinguishable objects, we have all $n_1!$ ways of arranging N into n_R spaces are the same \rightarrow divide them out

$$\rightarrow \frac{N!}{(N-n_R)! n_R!} = \frac{N!}{n_R! n_1!}$$

\rightarrow For indistinguishable objects, we combine us... Total multiplicity of outcomes

$$\Omega(n_R) = \frac{N!}{n_1! (N-n_1)!} = \binom{N}{n_R}$$

$$P_N(n_R, n_L) = \binom{N}{n_R} p^{n_R} (1-p)^{N-n_R}$$

or other notation

$$W_N(n_R) = \binom{N}{n_R} p^{n_R} (1-p)^{N-n_R} \rightarrow \text{same thing}$$

Binomial distribution

$$\sum_{n=0}^N W_N(n) = 1 \quad E(n) = Np \quad \text{Var} = Np(1-p)$$

Ex 18, 2019

Binomial Distribution

$$P_N(n) = \binom{N}{n} p^n q^{N-n}$$

$$\sum_{n=0}^N P_N(n) = 1$$

More generally, $\sum_{n=0}^N W_N(n) = (p+q)^N$

Example Roll 4 dice

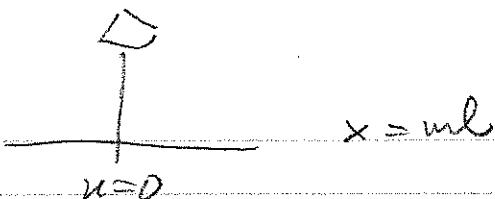
$$P(\text{one of 4 is } \square) = \binom{4}{1} \left(\frac{1}{6}\right)^1 \left(\frac{5}{6}\right)^{4-1} = 1 - \left(\frac{5}{6}\right)^4 \approx 39\%$$

Example Roll 2 1s, 4 dice

$$P_4(2) = \binom{4}{2} \left(\frac{1}{6}\right)^2 \left(\frac{5}{6}\right)^{4-2} = \frac{\binom{4}{2}}{6} \approx 12\%$$

Note high multiplicity, just not likely outcome.

Random Walk



What is the probability that we're back at $m=0$ after N steps?

(a) If N is even?

(i) If N is odd?

$$P_N(m) = \frac{N!}{n_R!(N-n_R)!} p^{n_R} (1-p)^{N-n_R}$$

$$N = n_R + n_L \\ m = n_R - n_L$$

$$= \frac{(n_R + n_L)!}{n_R! n_L!} p^{n_R} (1-p)^{N-n_R}$$

$$\text{So } N = 2n_1 - m$$

$$= \frac{N!}{\left(\frac{N+m}{2}\right)! \left(\frac{N-m}{2}\right)!} p^{\frac{N+m}{2}} (1-p)^{\frac{N-m}{2}}$$

Assume that $p = 1-p = \frac{1}{2}$

$$\text{So } P_N(m) = \frac{N!}{\left(\frac{N+m}{2}\right)! \left(\frac{N-m}{2}\right)!} \cdot \left(\frac{1}{2}\right)^N$$

$$\text{So } P_N(m=0) = \frac{N!}{\left(\frac{N}{2}\right)! \left(\frac{N}{2}\right)!} \left(\frac{1}{2}\right)^N \Rightarrow \text{if } N \text{ even}$$

if N is odd, then $m \neq 0$

Since $N = 2n_1 - m$

$$\text{So } P_N(m=0) = 0$$

\uparrow \uparrow \uparrow
 odd even odd

Determination of mean values

Random walk with $N = 2$ steps. Let's say after 2 steps, drunk finds \$ and pick it up.

@ $x = -2l$ \$1
 @ $x = 0$ \$5
 @ $x = 2l$ \$20

Question on average, how much \$ would you pick up?

Well $P_2(-2l) = ?$ $P_2(2l) = ?$; $P_2(0) = ?$

$$\rightarrow \left. \begin{array}{l} P_2(0) = 1/2 \\ P_2(-2l) = P_2(2l) = 1/4 \end{array} \right\} \text{ "by inspection"}$$

Let $f(x)$ be the amount of \$ at location x .

In general , $\langle x \rangle = E(x) = \sum_{x=0}^{\infty} x P_N(x)$

$$\text{or } \bar{x} = \frac{\sum_{x_i=0}^{\infty} P(x_i) x_i}{\sum_{x_i=1}^{\infty} P(x_i)}$$

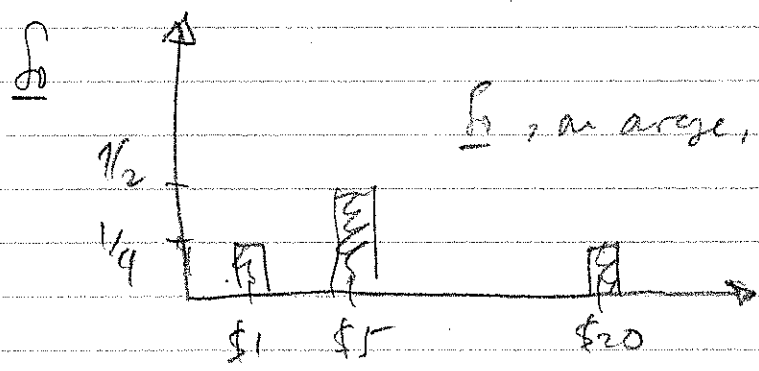
But since we're dealing w probabilities, $\sum_0^{\infty} P(x_i) = 1$

↳ Mean value of f_n .

$$E[f(x)] = \sum_{x=0}^{\infty} f(x) P(x)$$

Note $E[f(x) + g(x)] = E(f(x)) + E(g(x))$

if $s E(f(x)) = E(s f(x))$, $s \in \mathbb{R}$



\$, on average, $E(\$) = \frac{1}{4} \cdot 1 + \frac{1}{2} \cdot 5 + \frac{1}{4} \cdot 20$
 $= \frac{1}{4} + \frac{5}{2} + 5$
 $= \$ \frac{10 + 11}{4}$

On average, how far away from the average are we?

$E(x - E(x)) = ? = E(x) - E(x) = 0$

What about $E((x - E(x))^2)$?

Second moment about the mean? \rightarrow Variance

$$\overline{\Delta u^2} = \sigma^2 = E[(x - E(x))^2]$$

$$= E(x^2) - 2E(x)E(x) + E(E(x)^2)$$

$$\text{Var}(x) = E(x^2) - E(x)^2$$

Standard deviation $\rightarrow \sqrt{\text{Var}(x)} = \sigma_x = \sqrt{E(x^2) - E(x)^2}$

Mean values - Random Walk problems

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Recall

$$P_N(n_R) = \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$$

$$E[f(n_R)] = \sum_{n_R=0}^N f(n_R) P_N(n_R)$$

↳

Average # steps to the right

$$E[n_R] = \sum_{n_R=0}^N n_R P(n_R) = \sum_{n_R=0}^N n_R \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$$

Notice $n_R p^{n_R} = p \frac{\partial}{\partial p} (p^{n_R})$

$$E[n_R] = \sum_{n_R=0}^N \frac{N!}{n_R!(N-n_R)!} p \frac{\partial}{\partial p} (p^{n_R}) q^{N-n_R}$$

$$= p \frac{\partial}{\partial p} \sum_{n_R=0}^N \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$$

$$= p \frac{\partial}{\partial p} (p+q)^N$$

$$= p \cdot N \frac{\partial}{\partial p} (p+q)^{N-1}$$

But $p+q=1$

↳ $E[n_R] = pN$

Similarly $E[n_L] = qN = N(1-p)$

$$\left. \begin{aligned} E[n] &= E[n_R - n_L] \\ &= E[n_R] - E[n_L] \\ &= N(p-q) \end{aligned} \right\}$$

$E(m) = N(p-q)$

If $p=q$, then $E(m) = 0$.

Variance

$Var(n_R) = E(n_R^2) - E(n_R)^2$

$E(n_R^2) = \sum_{n_R=0}^N n_R^2 P(n_R)$
 $= \sum_{n_R=0}^N n_R^2 \frac{N!}{n_R!(N-n_R)!} p^{n_R} q^{N-n_R}$

Same trick as before $n_R^2 p^{n_R} = n_R p \frac{\partial}{\partial p} p^{n_R} = p \frac{\partial}{\partial p} (n_R p^{n_R})$

$E(n_R^2) = \sum_{n_R=0}^N \binom{N}{n_R} \left(p \frac{\partial}{\partial p} \right)^2 p^{n_R} q^{N-n_R} = \left(p \frac{\partial}{\partial p} \right)^2 p^N$

$= \sum_{n_R=0}^N \binom{N}{n_R} \left(p \frac{\partial}{\partial p} \right)^2 p^{n_R} q^{N-n_R}$

$= \left(p \frac{\partial}{\partial p} \right)^2 \sum_{n_R=0}^N \binom{N}{n_R} p^{n_R} q^{N-n_R}$

$= \left(p \frac{\partial}{\partial p} \right)^2 [p+q]^N$

$= \left[p \frac{\partial}{\partial p} \right] (p - N(p+q)^{N-1})$

$q+p=1 \rightarrow = p [N(p+q)^{N-1} + pN(N-1)(p+q)^{N-2}]$

$= pN + p^2 N(N-1) = pN + (pN)^2 - p^2 N$

$$\begin{aligned} \text{Var}(n_R) &= pN + (pN)^2 - p^2N - (pN)^2 \\ &= pN(1-p) \end{aligned}$$

$$\text{Var}(n_R) = Npq$$

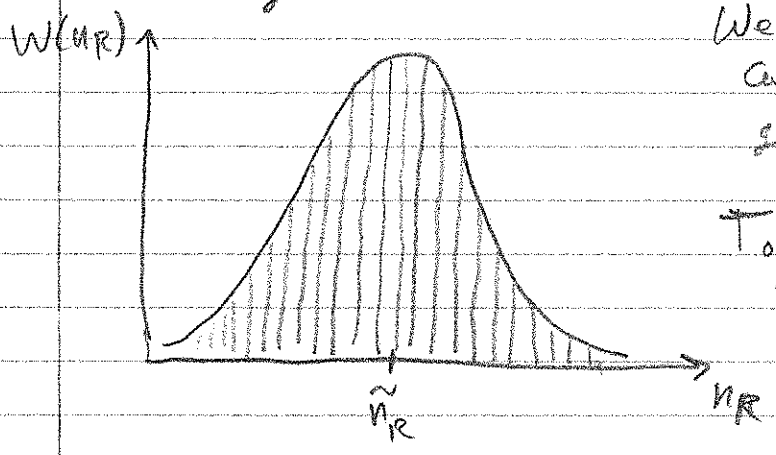
Relative Width of a distribution

$$\frac{\sigma_{n_R}}{E(n_R)} = \frac{\sigma_{n_R}}{Np} = \frac{\sqrt{Npq}}{Np} = \frac{\sqrt{q}}{\sqrt{Np}} = \frac{q}{\sqrt{Np}}$$

when $p=q$, $\frac{\sigma_{n_R}}{E(n_R)} = \frac{1}{\sqrt{N}}$

→ relative width is $\propto \frac{1}{\sqrt{N}}$ ($p \neq q$ in general)

For large N , there's a well defined peak in $W(n_R)$ at $n_R = \tilde{n}_R$, where \tilde{n}_R is the most likely value.



We can treat this as a continuous function as $N - n_R$ get large.

To find \tilde{n}_R as a fn of N, p, q , we need to look for where

$$\frac{\partial W(n_R)}{\partial n_R} = 0$$

Instead of evaluating $\frac{dW}{dn_R}$, we'll do

$\frac{d}{dn_R} \ln(W(n_R))$ since it has the same \tilde{n}_R & is a more gradually vary fn of n_R

$$\frac{dW_{ML}}{dn_{ML}} = 0 = \frac{d \ln(W(n_{ML}))}{dn_{ML}}$$

Taylor series expansion around \hat{a}^n

$$f(x) \approx f(a) + \frac{f'(a)}{1} (x-a) + \frac{f''(a)}{2!} (x-a)^2 + \dots$$

We want to expand $\ln W(n_{ML})$ around \tilde{n}_{ML} .

$$n_{ML} = \tilde{n}_{ML} + \epsilon \quad (\epsilon \ll \tilde{n}_{ML}) \quad \text{let's write } n \equiv n_{ML}$$

$$\ln(W(n)) = \ln(W(\tilde{n})) + \left. \frac{d \ln(W(n))}{dn} \right|_{\tilde{n}} \epsilon + \frac{1}{2} \left. \frac{d^2 \ln(W(n))}{dn^2} \right|_{\tilde{n}} \epsilon^2 + \dots$$

\downarrow
0 since \tilde{n} most likely...

$$= \ln(W(\tilde{n})) + \frac{1}{2} \left. \frac{d^2 \ln(W(n))}{dn^2} \right|_{\tilde{n}} \epsilon^2$$

$$\text{So } W(n) \approx W(\tilde{n}) \cdot \exp \left[\frac{1}{2} \left. \frac{d^2 \ln W(n)}{dn^2} \right|_{\tilde{n}} \epsilon^2 \right]$$

Next $\frac{d \ln W(n)}{dn} = \frac{d}{dn} \left(\ln \left[\binom{N}{n} p^n q^{N-n} \right] \right)$

$$= \frac{d}{dn} \left[\ln(N!) - \ln(n!) - \ln((N-n)!) + n \ln p + (N-n) \ln q \right]$$

Note that $\frac{d \ln x!}{dx} \approx \ln x$ for large x

$$\text{So } \left. \frac{d \ln(W(n))}{dn} \right|_{\tilde{n}} = -\ln \tilde{n} + \ln(N - \tilde{n}) + \ln p - \ln q$$

Recall

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$$W(n) = W(\tilde{n}) \exp \left[\frac{1}{2} (n - \tilde{n})^2 \frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} \right]$$

$$\frac{d \ln W}{dn} \Big|_{\tilde{n}} = -\ln \tilde{n} + \ln(N - \tilde{n}) + \ln p - \ln q$$

~~$$e^0 = \frac{N!}{\tilde{n}! (N - \tilde{n})!} p^{\tilde{n}} q^{N - \tilde{n}}$$~~

$$e^0 = e^{\ln \left(\frac{(N - \tilde{n})^p}{n^q} \right)} = E(n)$$

$$\text{So } 1 = \frac{(N - \tilde{n})^p}{n^q} \Rightarrow \boxed{\tilde{n} = \frac{Np}{p+q} = \frac{Np}{1}} \quad \leftarrow \text{arrow from } E(n)$$

Now, evaluate $\frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}}$

$$\frac{d^2 \ln W}{dn^2} = \frac{d}{dn} \left(\frac{d \ln W}{dn} \right) = \frac{d}{dn} \left[-\ln \tilde{n} + \ln(N - \tilde{n}) + \ln p - \ln q \right]$$

$$= \left. \left[-\frac{1}{n} - \frac{1}{N-n} \right] \right|_{\tilde{n}} = \left. \frac{-N+n-n}{n(N-n)} \right|_{\tilde{n}}$$

$$\text{So } \frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} = \frac{-N}{\tilde{n}(N - \tilde{n})} = \frac{-N}{Np(N - Np)} = \frac{-1}{Np(1-p)}$$

$$\boxed{\frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} = \frac{-1}{Np(1-p)}} \rightarrow < 0$$

Finally, we need $W(\tilde{n})$

$$\hookrightarrow W(\tilde{n}) = \frac{N!}{\tilde{n}!(N - \tilde{n})!} p^{\tilde{n}} q^{N - \tilde{n}} = \dots \text{ For large } N \dots$$

Use Stirling formula $n! \approx \sqrt{2\pi n} n^n e^{-n}$ for $n \gg 1$

$$W(\tilde{n}) = \frac{\sqrt{2\pi N} N^{N-N} e^{-N}}{\sqrt{2\pi N_p} (N_p)^{N_p} e^{-N_p} \cdot \sqrt{2\pi (N-N_p)} (N-N_p)^{N-N_p} e^{-(N-N_p)}} \cdot p^{N_p} q^{N_p}$$

→ $W(\tilde{n}) = \frac{1}{\sqrt{2\pi N_p q}}$ max of a Gaussian of $\sigma^2 = N_p q$

Now $W(n) = W(\tilde{n}) \exp \left[\frac{1}{2} (n - \tilde{n})^2 \frac{d^2 \ln W}{dn^2} \Big|_{\tilde{n}} \right]$

$$W(n) = \frac{1}{\sqrt{2\pi N_p q}} e^{-\frac{(n - N_p)^2}{2 N_p q}}$$

→ Gaussian Normal

→ Random walk for large N .

$$W(n) = \frac{1}{\sqrt{2\pi \sigma^2}} e^{-\frac{(n - E(n))^2}{2\sigma^2}}$$

Example large N . A penny is tossed 400 times
 Find the probability of exactly 215 heads

$p = q = \frac{1}{2}$
 $N = 400$
 $n = 215$
 $N_p = 200$

$$W(215) = \frac{1}{\sqrt{2\pi \cdot 100}} \cdot \exp \left[-\frac{1}{2} \frac{(215 - 200)^2}{100} \right]$$

= 1.3% → very unlikely? ...

More generally,

$$f(x) dx = \frac{1}{\sqrt{2\pi}\sigma} e^{-\frac{(x-\mu)^2}{2\sigma^2}} dx$$

→ probability density function — PDF

$$\int_a^b f(x) dx = P(a \leq x \leq b)$$

If probability dist. that depends on more than 1 var

$$P(u_i, v_i) = f(u_i) f(v_i) \rightarrow \text{as long as } u, v \text{ independent}$$

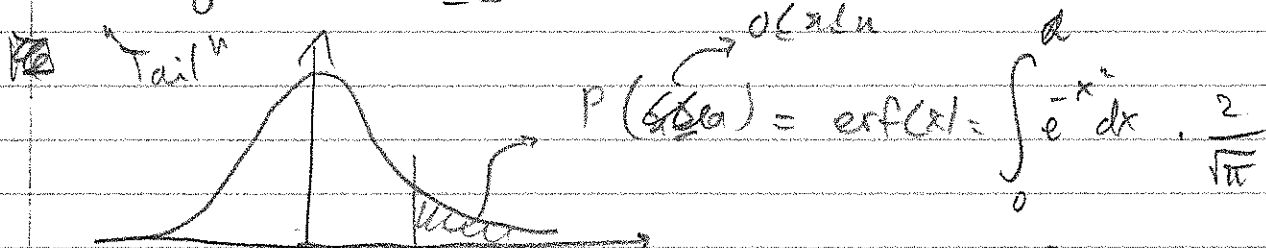
Gaussian integrals are difficult to evaluate analytically

But there are 2 cases when we can have precise answers.

$$\int_{-\infty}^{\infty} e^{-x^2} dx = \sqrt{\pi}$$

But since it's symmetrical about $x=0$

$$\int_0^{\infty} e^{-x^2} dx = \int_{-\infty}^0 e^{-x^2} dx = \frac{\sqrt{\pi}}{2}$$



$$P(x \geq a) = 1 - \Phi(a) = 1 - \int_{-\infty}^a f(x) dx$$

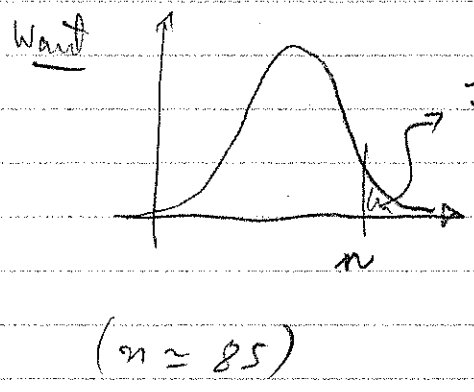
Ex

Town A has 2000 customers and they want to talk to town B. What is the minimum # lines needed such that at most 1% of town A's customers fail to have access to a line during the busiest hour of the day?

↳ assume each caller is on the line for 2 mins in that hr randomly dist.

$N = 2000$ $p = P(\text{line in use}) = \frac{2}{60} = \frac{1}{30}$
 $n = ?$ $q = \frac{29}{30}$

$$W(n) = \frac{1}{\sqrt{2\pi Npq}} \exp\left[-\frac{1}{2} \frac{(n - Np)^2}{Npq}\right]$$



$\text{let } x = \left(\frac{1}{2} \frac{(n - Np)^2}{Npq}\right)^{1/2}$
 $\frac{dx}{dn} = \frac{d}{dn} \left[\frac{1}{\sqrt{2}} \frac{n - Np}{\sqrt{Npq}} \right]$

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Back to Schroeder, Chap 2.

terminology → microstate → any individual outcome

↳ state of each individual particle in the system (order matters). $\Omega = 1$

macrostate → more general description of the system has some multiplicity. some microstates are indistinguishable ↑ multiplicity

→ multiplicity Ω → the number of microstates in a macrostate

▣ Example

4 dice rolled ⇒ outcome 1 3 1 5
microstate

Macrostate could be system where we roll two 2s in 4 dice

multiplicity → $\Omega = \binom{4}{2} = 6$

▣ Note that small multiplicity implies highly ordered system.

vs large multiplicity implies disorder.

Second Law of Thermodynamics

↳ systems tend towards more disorder because multiplicity is higher

↳ because these macrostates are more likely... (?)

Ω is related to Entropy

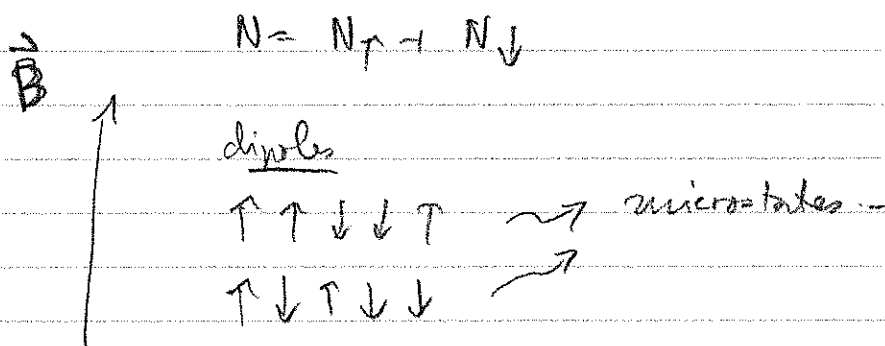
▣ Two physical systems where we see count individual microstate

ex (1) Two-state paramagnet → material in a B field

Individual dipoles line up in 1 or 2 states: aligned or anti-aligned.

microstate → specified by stating direction of all individual dipoles.

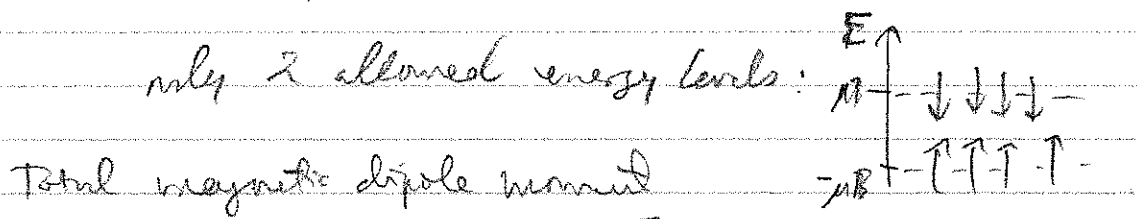
macrostate \rightarrow total # of dipoles that point up, N_{\uparrow}



Macrostate $5 \downarrow + 5 \uparrow$

$\mu \rightarrow$ magnetic moment of individual dipole

only 2 allowed energy levels:



$$\hookrightarrow \vec{M} = \vec{\mu} (N_{\uparrow} - N_{\downarrow})$$

$$\text{or } \vec{M} = \vec{\mu} (N_{\uparrow} - N + N_{\uparrow}) = \vec{\mu} (2N_{\uparrow} - N)$$

energy of single dipole $= -\vec{\mu} \cdot \vec{B} = \epsilon_i \rightarrow \pm \mu B$ for $\mu \uparrow \vec{B}$

So energy of paramagnet is $\rightarrow \propto -2N_{\uparrow} + N$

$$U = -M \cdot B = \mu B (N_{\downarrow} - N_{\uparrow})$$

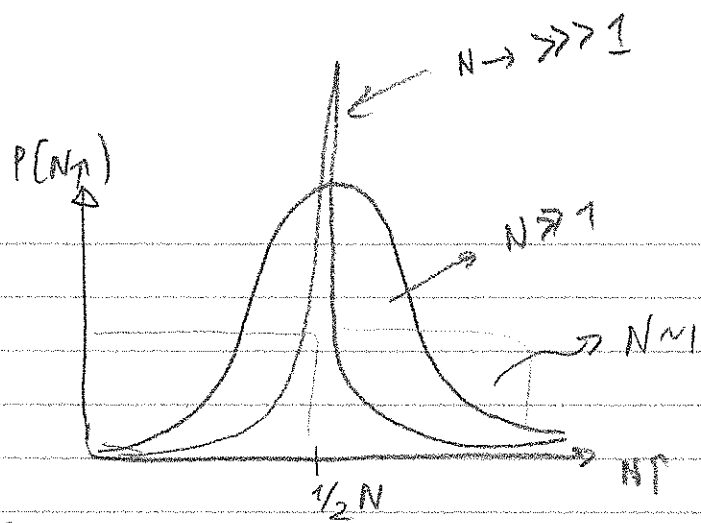
$$\text{or } U = \mu B (N - 2N_{\uparrow})$$

Calculate most probable energy

$$p = q = \frac{1}{2}$$

$$P(N_{\uparrow}) = \binom{N}{N_{\uparrow}} p^{N_{\uparrow}} q^{N - N_{\uparrow}} = \Omega(N_{\uparrow}) / 2^N$$

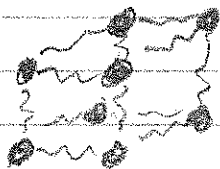
As $N \rightarrow \infty$



So, random orientation of dipoles is not possible
 → 2nd law of thermodynamics

there ρ & Ω

(2) Einstein's model of solid / bed spring model



N atoms which have $3N$ independent harmonic oscillators, which provide 6 degrees of freedom each. (per atom)
 (1 KE + 1 PE) per spring

Classical spring

$$U = \frac{1}{2} m v^2 + \frac{1}{2} k x^2 = KE + PE$$

$$= \frac{1}{2} m (v_x^2 + v_y^2 + v_z^2) + \frac{1}{2} k (x^2 + y^2 + z^2)$$

So here we have "unlimited" energy spectrum, but as quantum oscillator → discrete energies that are allowed

$$E_i = q_i h f = q_i \frac{1}{2} h \omega = q_i \frac{1}{2} h \nu$$

For $N = 3$ oscillators, the multiplicity of different energy levels

Osc	# 1	# 2	# 3	$\sum E_i$	Ω
	0	0	0	0	} 3
	0	1	0	$h\nu$	
	1	0	0	$h\nu$	
	0	0	1	$h\nu$	

# 1	# 2	# 3	ΣU	Ω
2	0	0	} $2h\nu$	6
0	2	0		
0	0	2		
1	1	0		
1	0	1		
0	1	1		
			} $3h\nu$	10

multiplicity of Einstein solid

↳ General expression for multiplicity:

$\Omega = \binom{N}{q}$ Instead

$$\Omega(N, q) = \binom{q+N-1}{q} = \frac{(q+N-1)!}{q!(N-1)!}$$

\uparrow # of oscillators
 \uparrow units of energy

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Heat flow & Irreversible Processes

Consider 2 Einstein solids that can interact

<u>Solid A</u>	<u>Solid B</u>	$U = qh\nu$
$N_A = 3$	$N_B = 3$	

single atom {

$$\left. \begin{aligned} q &= \text{total \# of energy quanta} = 6 = q_A + q_B \\ \sum_i & \quad 0 \leq q_A \leq 6, \quad 0 \leq q_B \leq 6 \end{aligned} \right\}$$

Multiplicity $\Omega = \binom{q+N-1}{q}$

For A $\Omega_A = \binom{q_A+N_A-1}{q_A}$

For B $\Omega_B = \binom{q_B+N_B-1}{q_B}$

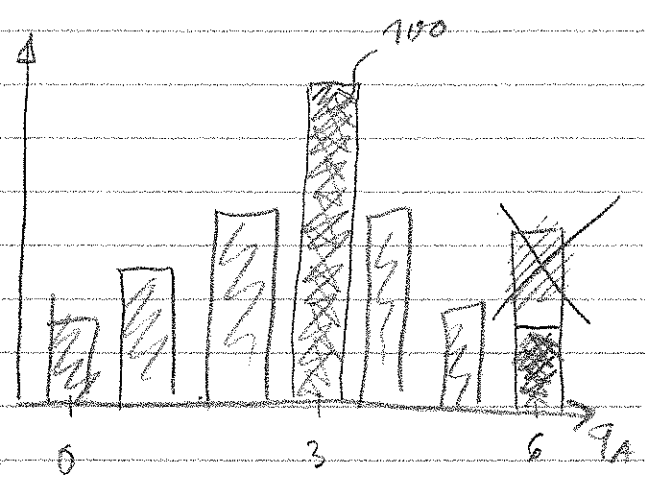
Since A & B independent

$\Omega_{tot} = \Omega_A \Omega_B$

Ex $\Omega_{tot} = \Omega_A \Omega_B$ Ω_{tot}

$\Omega_A(q_A=3) = \binom{3+3-1}{3} = 10$

$\Omega_B(q_B=3) = 10$



$\Omega_{tot} = \Omega_A \Omega_B = 100$

Ex $\Omega_A(q_A=6) = \binom{6+3-1}{6} = 28$

$\Omega_B(q_B=0) = \binom{0+3-1}{0} = 1$

($q_A + q_B = 6$)

$\Omega_A \Omega_B = \Omega_{tot} = 28 \times 1 = 28$

Fundamental assumption \rightarrow stat mech

Any given microstate is equally probable. But some macrostates will be more probable than others because of higher multiplicity Ω

If you start out with a system near most likely macrostate

very unlikely that it will move far away from this distribution.

Ex $N_A = 50, N_B = 50, N_{tot} = 50$

Case 1 $q_A = 50, q_B = 0 \rightarrow \Omega_A = \binom{100-1}{50} \binom{0+50-1}{0}$

Case 2 $q_A = q_B = 25$

$\Omega_{tot} \approx \binom{25+50-1}{25}^2 = 1 \times 10^{39}$

$= \binom{99}{50} \binom{49}{0} \approx 5 \times 10^{28}$

$\rightarrow q_A = 25 = q_B \leftarrow$ macrostate 20 billion times more probable than $q_A = 50, q_B = 0$.

Irreversible processes

\hookrightarrow Energy flows from system A to system B, increasing the total Ω of the interacting system.

Restate 2nd Law of thermodynamics

\hookrightarrow { Systems in thermal equilibrium will be arranged with the highest amount of disorder }

or

$\left\{ \begin{array}{l} \text{Spontaneous flow of energy stops when a system is} \\ \text{at or very near its most likely microstate} \\ \text{greatest } \Omega \end{array} \right\}$

impossible
not spontaneous

Large System

- (1) • Small # $\rightarrow (N < 100)$
- (2) • large # \rightarrow small # that are exponential 10^{23}
- (4) • very large # \rightarrow large # that are exponential or large # in factorial...
Ex $10^{10^{23}}$

Note some properties

$$(add) \cdot 10^{23} + 23 \approx 10^{23}$$

$$(mult.) \cdot 10^{23} \times 10^{23} = 10^{23+23} \approx 10^{46}$$

$$(Division) \cdot \frac{10^{46} \times 10^{23}}{10^{46}} = 10^{23}$$

Manipulating large numbers $e^{10^{23}} \rightarrow \ln[e^{10^{23}}] = 10^{23}$

$$\rightarrow e^{10^{23}} \approx 10^{4.34 \times 10^{22}}$$

$$e^{10^{23}} \text{ as } 10^x \rightarrow 10^{23} = x \ln 10 \rightarrow x = \frac{10^{23}}{\ln(10)} \approx 4.34 \times 10^{22}$$

Multiplicity of Einstein solid (large)

↳ at high $T \Rightarrow q \gg N \rightarrow N$ large

$$\Omega = \binom{q+N-1}{q} = \frac{(q+N-1)!}{q!(N-1)!} \approx \frac{(q+N)!}{q!N!}$$

Take the log

$$\ln \Omega = \ln \left[\frac{(q+N)!}{q!N!} \right] = \ln(q+N)! - \ln q! - \ln N!$$

Use Stirling's formula: $N! \sim N^N e^{-N} \sqrt{2\pi N}$

$$\hookrightarrow \ln(N!) \approx N \ln N - N$$

$$\text{So } \ln \Omega = (q+N) \ln(q+N) - (q+N) - [q \ln q - q] - [N \ln N - N]$$

→ next page

$\Omega = (q+N) \ln(N+q) - N \ln N - q \ln q$

Rewrite $\ln(q+N) = \ln\left(q\left(1+\frac{N}{q}\right)\right) \rightarrow \ll$
 $= \ln q + \ln\left(1+\frac{N}{q}\right)$
 $\approx \ln q + \frac{N}{q}$

$\ln \Omega \approx (q+N) \left[\ln q + \frac{N}{q} \right] - N \ln N - q \ln q \quad (q \gg N)$
 $= N \ln q + \frac{N^2}{q} - N \ln N + N \quad \left(\frac{N^2}{q} \approx 0 \right)$

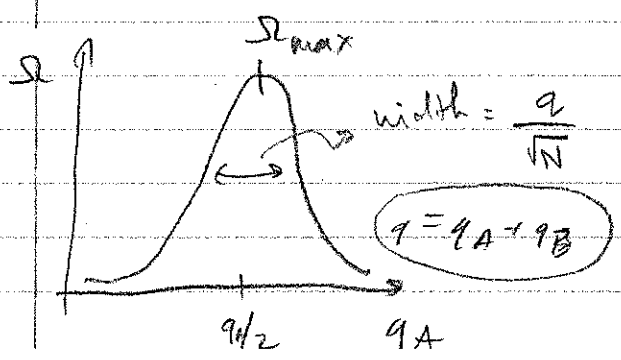
$\Omega = \exp\left[N \ln q - N \ln N + N\right]$
 $= \frac{e^{N \ln q} e^N}{e^{N \ln N}} = \frac{e^N \cdot q^N}{N^N} = \left(\frac{eq}{N}\right)^N$

$\Omega = \left(\frac{eq}{N}\right)^N$ $\left(q \gg N \right)$ \leftarrow total multiplicity of loose Einstein solid in high temp limit, (like room temp)

Feb 26, 2019

$\Omega_{tot} = \Omega_A \Omega_B$

For interacting solids $\rightarrow \Omega = \Omega_{max} e^{-N(2x/v)^2}$ \leftarrow Gaussian

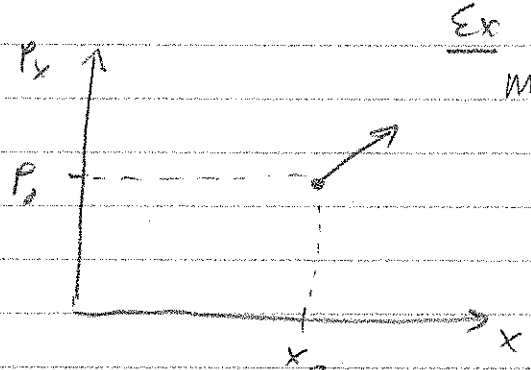


As $N \uparrow$, the fluctuations away from the most likely macrostate become increasingly improbable. \rightarrow Thermodynamic limit

Multiplicity of an ideal gas

* Specify the state of a system in classical mechanics using phase space.

☑ If an object's position & momentum is known, we can predict it's position & momentum at any other time.



Ex
 $m\dot{x} = \vec{p} = c\vec{x}$

We can determine $x(t)$ & $p(t)$ from initial conditions.

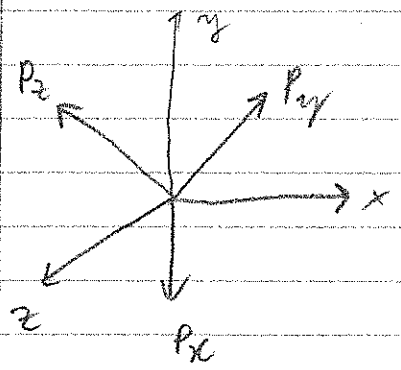
$$m \frac{dx}{dt} = cx \rightarrow \int_{x_0}^x \frac{m dx}{x} = \int c dt$$

So $\ln\left(\frac{x}{x_0}\right) = \frac{c}{m}(t-t_0)$

So $x(t) = x_0 e^{\frac{c}{m}(t-t_0)}$

To get $p(t)$
 $\rightarrow p = m\dot{x} = m \cdot \frac{c}{m} x_0 e^{\frac{c}{m}(t-t_0)} = cx_0 e^{\frac{c}{m}(t-t_0)}$

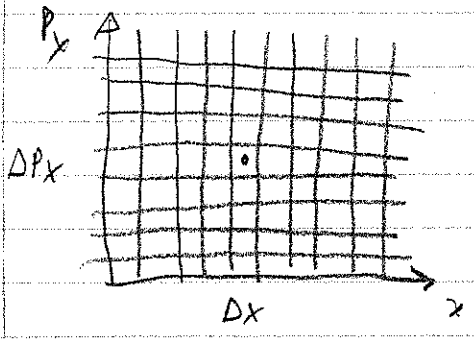
For particle in space



$$(x, y, z, p_x, p_y, p_z)$$

For N objects, we need 6N coordinates to describe its phase space.

To describe state of system in phase space



particle located between x & $x + \Delta x$
and $p_x = p_x + \Delta p_x$

Heisenberg Uncertainty principle

$$\Delta p \Delta x \geq \frac{h}{2} (?)$$

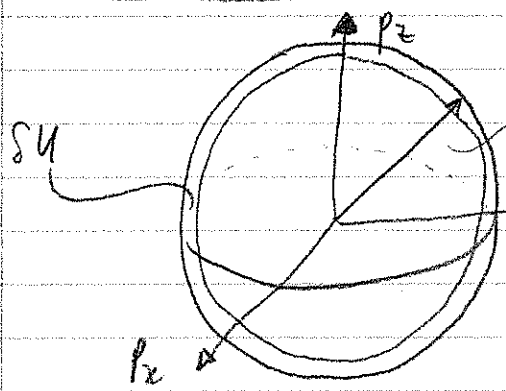
→ let $\Delta x \Delta p = h$

For a monatomic ideal gas, energy is all kinetic

$$U = \frac{1}{2} m (v_x^2 + v_y^2 + v_z^2) = \frac{1}{2m} (p_x^2 + p_y^2 + p_z^2)$$

$$p = \sqrt{p_x^2 + p_y^2 + p_z^2} = \sqrt{2mU}$$

For 3-D momentum space



inner radius = $\sqrt{2mU}$ outer radius = $\sqrt{2m(U + \Delta U)}$

$\Omega \propto V_x V_p$ multiplicity of 1 particle
 position volume momentum volume

And # states $\propto \frac{V_x}{\Delta x \Delta y \Delta z} \cdot \frac{V_p}{\Delta p_x \Delta p_y \Delta p_z}$

$$\Omega(u) \propto \int_u^{u+\Delta u} \int \int dx dy dz dp_x dp_y dp_z$$

$dp_x dp_y dp_z$ $\Delta p_x \Delta p_y \Delta p_z$

For N particles $\Omega(u) \propto \int_u^{u+\Delta u} \int \dots \int d^3r_1 \dots d^3r_N d^3p_1 \dots d^3p_N$

Volume is independent, so

$$\Omega(u) \propto V^N \int_u^{u+\delta u} \dots \int d^3 p_1 \dots d^3 p_N$$

$$\propto V^N \int_{\sqrt{2mU}}^{\sqrt{2m(U+\delta U)}} \underbrace{p^{3N-1}}_{\text{"surface area"}} \cdot \underbrace{dp}_{\text{thickness}}$$

$$\int \Omega(u) \propto V^N (\sqrt{2mU})^{3N-1} \left[\sqrt{2m(U+\delta U)} - \sqrt{2mU} \right]$$
$$= V^N \underbrace{\sqrt{2mU}^{3N-1}}_{\text{surface area}} \left[\underbrace{\sqrt{2mU}}_{\text{thickness}} \sqrt{1 + \frac{\delta u}{u}} - \sqrt{2mU} \right]$$

$$\Omega(u) \propto V^N (\sqrt{2mU})^{3N} \left[\sqrt{1 + \frac{\delta u}{u}} - 1 \right]$$

• Taylor expand $(1+x)^n \sim 1+nx$ ($x \ll 1$)

$$\int \Omega(u) \propto V^N (\sqrt{2mU})^{3N} \cdot \left(\frac{\delta u}{2u} \right)$$

$$\int \Omega(u) \propto V^N (\sqrt{2u})^{3N} \cdot \frac{\delta u}{u}$$

$$\Omega(u) \propto V^N u^{3N/2} \cdot (\delta u) u^{-1}$$

$$\int \Omega(u) \propto V^N u^{(3N/2-1)} \delta u$$

small number
ignore u^{-1} as well...

$$\int \Omega(u) \propto V^N u^{\frac{3N}{2}}$$

More careful derivation gives

multiplicity of monatomic ideal gas

$$\Omega(u) \approx \frac{\pi^{3N/2}}{N! h^{3N} (3N/2)!} V^N (\sqrt{2mU})^{3N}$$

$$\Omega \sim u^{(3/2)N}$$

For general result $\rightarrow \Omega \sim u^{NR/2}$, $f = \# \text{ dF for single particle}$

Feb 27, 1989

Result for monoatomic ideal gas

$$\Omega(u, V, N) \approx \frac{\pi^{3N/2}}{N! h^{3N} (3N/2)!} V^N (\sqrt{2mU})^{3N}$$

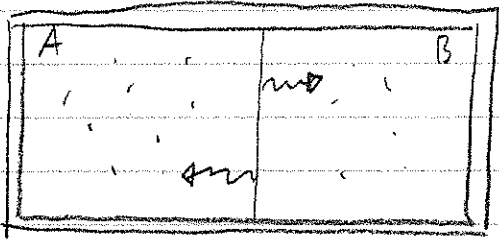
Interacting ideal gas

$$\Omega_{\text{tot}} = \Omega_A \Omega_B = [f(N)]^2 (V_A V_B)^N (u_A u_B)^{3N/2}$$

assuming $A \neq B$

3 ways to exchange multiplicity

(1) Exchange energy



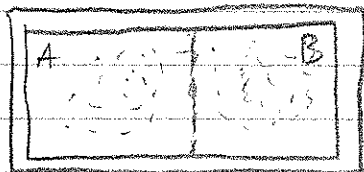
$$(\Omega \sim u^{3N/2})$$

Width of peak in the multiplicity function $\Omega_{\text{tot}} = \frac{u_{\text{tot}}}{\sqrt{3N/2}}$ and maximum u_{tot} is at $u_A = \frac{1}{2} u_{\text{tot}}$

(2) Exchange volume via a movable partition

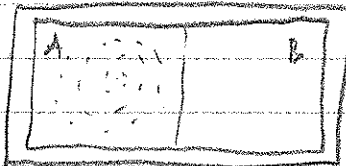
width of peak in $\Omega = \frac{V_{\text{tot}}}{\sqrt{N}}$ ($\Omega \sim V^N$)

③ Exchange particles via permeable membrane (membrane)



→ more complicated overall because of $f(N) \sim u(N)$

Consider specific case



Here $V_{tot} \downarrow \times 2 \rightarrow$ this reduces Ω_{tot} by 2^N

ENTROPY

$$S \equiv k \ln \Omega$$

where k is Boltzmann constant = 1.38×10^{-23} J/K
 Ω is the multiplicity.

$$2^{nd} \text{ Law of Thermodynamics: } \Delta S \geq 0$$

Note For interacting systems $\Omega_{tot} = \Omega_A \Omega_B$

$$\begin{aligned} S_{tot} &= k \ln \Omega_{tot} = k \ln (\Omega_A \Omega_B) \\ &= k \ln \Omega_A + k \ln \Omega_B \\ &= S_A + S_B \end{aligned}$$

$$S_{tot} = S_A + S_B$$

☑ Spontaneous processes occur due to a net increase in entropy.

Entropy of an ideal gas

$$S = k \ln \Omega$$

$$= k \ln \left[\frac{\pi^{3N/2}}{N! h^{3N} (3N/2)!} V^N (\sqrt{2mU})^{3N} \right]$$

Stirling's formula: $\ln N! \approx N \ln N - N$

$$S = k \left[\frac{3N}{2} \ln \pi + N \ln V + \frac{3N}{2} \ln(2mU) - (N \ln N - N) \right.$$

$$\left. - 3N \ln h - \left(\frac{3N}{2} \ln \frac{3N}{2} - \frac{3N}{2} \right) \right]$$

$$= Nk \left[\frac{3}{2} \ln \pi + \ln V + \frac{3}{2} \ln(2mU) - (\ln N - 1) \right.$$

$$\left. - 3 \ln h - \left(\frac{3}{2} \ln \frac{3N}{2} - \frac{3}{2} \right) \right]$$

$$S = Nk \left\{ \ln \left[\frac{V}{N} \left(\frac{400mU}{3Nh^2} \right)^{3/2} \right] + \frac{5}{2} \right\}$$

→ entropy of ideal monatomic gas

↑
Sackur - Tetrode equation

Ex Calc. S of 1 mole of He gas @ room temp = 1 atm.

Need V, N, U, m_{He}

$N \sim 10^{23}$

$V \sim \frac{RT}{P} \approx 25 \text{ l}$

$m_{He} =$

$U = \frac{3}{2} NkT = \frac{3}{2} RT = 3700 \text{ J}$

Get $S_{He} \approx 126 \text{ J/K}$

If we hold $N = U$ fixed and allow V to change

$S \sim Nk \ln(V)$

$\Delta S = Nk \ln\left(\frac{V_f}{V_i}\right)$

$\Delta S = Nk \ln\left(\frac{V_f}{V_i}\right)$

quasi-static isothermal expansion/compression

Note if $Q > 0$, then $\Delta S > 0$

Mar 1, 2019

How entropy is related to the heat input to system Q ?

Heat in = work done by system
= - work done on system

$\Delta u = 0$ (isothermal) $Q_{add} = W_{by} = -W_{on}$

$Q_{add} = -W_{on} = \int_{V_i}^{V_f} P(V) dV$

$= \int_{V_i}^{V_f} \frac{NkT}{V} dV = NkT \ln\left(\frac{V_f}{V_i}\right) = T \Delta S$

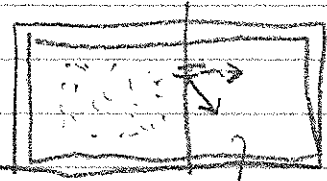
$\Delta S = \frac{Q_{add}}{T}$

quasi-static isothermal

more precisely

$ds = \frac{\delta Q}{T}$

Free expansion - non quasi-static



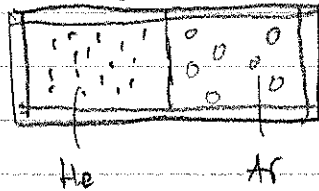
n, T constant $\rightarrow \Delta U = 0 = Q_{add} + W_{on}$
 $Q_{add} = 0$ because no heat enters or leaves system. So $W = 0$.

But there's an increase in entropy. Next can't use

$\Delta S = Q/T$ because the eq describes quasistatic isothermal

Entropy of mixing

Consider



know $S_{tot} = S_A + S_B$

Now, remove partition - let gases mix - how does S change?

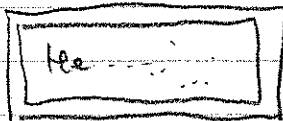
Back to S-T eqn: $S = Nk \left[\ln \left(\frac{V}{N} \left(\frac{4\pi m u}{3Nh^2} \right)^{3/2} \right) + \frac{5}{2} \right]$

- He: N const, u const, $V' = 2V$
- Ar: same thing.

$\Delta S = Nk \ln(2) |_{He} + Nk \ln(2) |_{Ar}$

$\Delta S = 2Nk \ln(2)$ \sim entropy of mixing (different gases)

Consider (same gas)



Adding Ar to cylinder... with same N, u as He
 \rightarrow expect ΔS by a factor of 2

If we add He instead (at same energy) \rightarrow same temperature

$S = Nk \left[\ln \left(\frac{V}{N} \left(\frac{4\pi m u}{3Nh^2} \right)^{3/2} \right) + \frac{5}{2} \right]$

V const $N' = 2N$

$U = \frac{3}{2} NkT \rightarrow u' = 2u$

$$S' = 2S_{He} + 2Nk \ln \left(\frac{1}{2} \right)$$

$$= 2S_{He} + \underbrace{(-2Nk \ln 2)}$$

$$S' = 2S_{He} - \Delta S_{mixing} \rightarrow \text{don't confuse set } S' = 2S$$

GIBBS' PARADOX \rightarrow why does distinguishability matter?

solution:
 particles have
 a distinguishable

Real

$$\Omega_N \approx \frac{1}{N!} \frac{V^N}{h^{3N}} \frac{u^{3N/2}}{(3N/2)!} (\sqrt{2\pi m})^{3N}$$

$$\ln \Omega_N \sim \ln \left(\frac{1}{N!} \right) \rightarrow -(N \ln N - N)$$

What if we're able to distinguish particles in gas \rightarrow $\frac{1}{N!}$
 because order matters

$$S = Nk \ln \left[V \left(\frac{4\pi m U}{3N h^2} \right)^{3/2} + \frac{3}{2} \right] \rightarrow \text{distinguishable}$$

Consider

•	•
•	•

 container with indistinguishable particles. Add a partition,

$$N \downarrow \times 2, V \downarrow \times 2, U \downarrow \times 2$$

$$\frac{1}{2} S^{new} = \frac{1}{2} S_{original} + \frac{1}{2} Nk \ln(1/2)$$

$$\frac{1}{2} S^{new} = \frac{1}{2} S_{original} - \frac{1}{2} Nk \ln 2 \rightarrow \text{decrease in entropy}$$

\rightarrow get decrease in entropy

Reversible vs Irreversible processes

- A process is irreversible if $\Delta S > 0$
- A process is reversible if $\Delta S = 0$

→ need to be quasistatic process.

↳ can be reversible, but don't have to be.

All reversible processes are quasistatic. But not all quasistatic processes are reversible

[Reversible $\not\subseteq$ Quasistatic]

Spontaneous heat flow is always irreversible

"Reversible heat flow" $\Delta T \rightarrow \Delta T$

System in $\Omega_{max} \Rightarrow$ thermal equilibrium

→ Infinitesimal change in temperature.

Mar 4, 2019

CHAPTER 3: RELATIONSHIP BETWEEN ENTROPY, TEMPERATURE

Simple interacting system of 2 Einstein solids

$N_A = 3$ oscillators
 $N_B = 2$
 $q = 6$

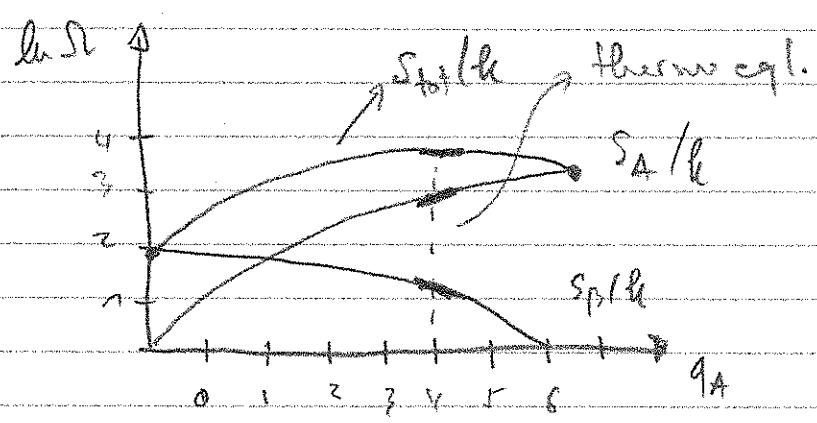
$$\Omega = \binom{q+N-1}{q} = \frac{(q+N+1)!}{q!(N+1)!}$$

$S = k_B \ln \Omega$

$\ln \Omega = \frac{S}{k}$

r	$N_A = 3$			$N_B = 2$			Ω_{tot}	S_{tot}/k
	q_A	Ω_A	S_A/k	q_B	Ω_B	S_B/k		
0	1	1	0	6	1	1.9	7	1.9
1	3	3	1.1	5	1	1.8	18	2.1
2	6	6	1.8	4	1	1.6	30	2.4
3	10	10	2.3	3	1	1.4	40	2.7
4	15	15	2.7	2	1	1.1	45	2.9
5	21	21	3.0	1	1	0.7	42	2.7
6	28	28	3.3	0	1	0	28	2.3

Plot of $\ln \Omega$ versus ϵ .



$\frac{\partial S_{tot}}{\partial q_A} = 0$, then we set maximum entropy

→ condition for thermodynamic equilibrium

Recall $U_A = q_A$ (constant)

$\frac{\partial S_{tot}}{\partial q_A} = 0 \Rightarrow \frac{\partial S_{tot}}{\partial U_A} = 0$ at eq.

Now, $S_{tot} = S_A + S_B \Rightarrow \partial S_{tot} = \partial S_A + \partial S_B$

$\frac{\partial S_{tot}}{\partial U_A} = \frac{\partial S_A}{\partial U_A} + \frac{\partial S_B}{\partial U_A} = 0 \Rightarrow \frac{\partial S_A}{\partial U_A} = -\frac{\partial S_B}{\partial U_A}$ at eq.

Note $U_{tot} = u_A + u_B$ - U_{tot} is conserved

$\rightarrow \partial U_{tot} = 0 = \partial u_A + \partial u_B \rightarrow \partial u_A = - \partial u_B$

So, we get $\frac{\partial S_A}{\partial u_A} = \frac{\partial S_B}{\partial u_B}$

Note when q_A is small $\Rightarrow \frac{\partial S_A}{\partial u_A}$ steep \rightarrow entropy of system A is increasing faster than entropy of B is decreasing

\rightarrow Spontaneous heat flow, energy

Energy flows to object with steeper S vs U slope

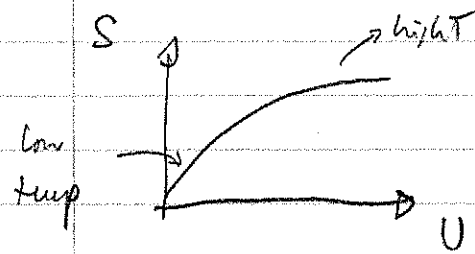
The steeper the slope the lower the temperature.

Units of S \rightarrow J/K } $T = \frac{\Delta U}{\Delta S} \equiv \frac{\partial U}{\partial S}$
Units of U \rightarrow J

Definition of temperature

$T^{-1} = \frac{\partial S}{\partial U}$ \rightarrow N, V constant

Patterns in S vs U graphs.



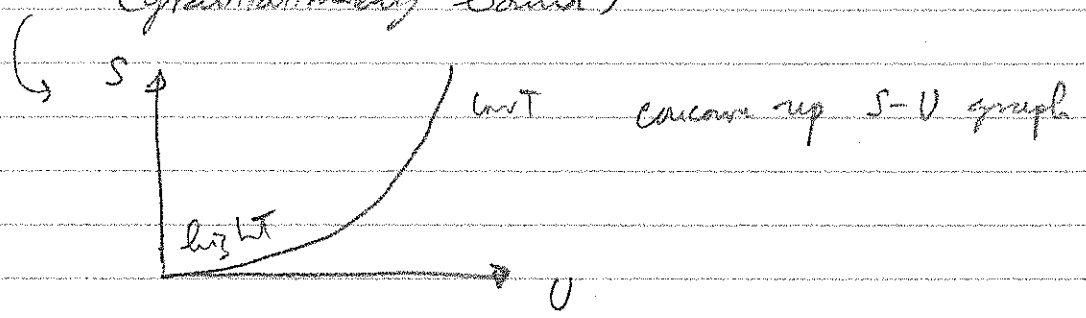
concave down \rightarrow In unit system, as $U \uparrow, T \uparrow$ which means \therefore slope of $(\frac{\partial S}{\partial u})_{N,V}$ decreases

Result $\Delta U = Q_{add} + W_{on}$ (assume V constant)

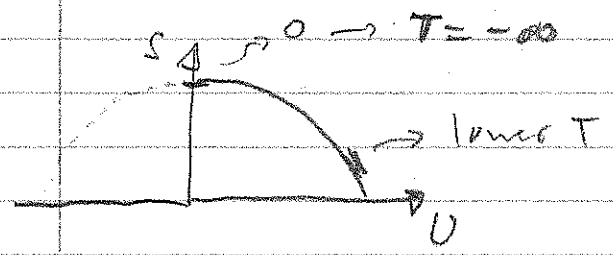
$Q_{add} = CST$

$\therefore \Delta U = CST \rightarrow$ makes sense

However, there are systems with negative heat capacity (gravitationally bound)



EX Concave down with negative slope...



EX Paramagnet. $U = \mu B (N_{\downarrow} - N_{\uparrow})$

$\left(\frac{\partial S}{\partial U}\right)_{N,V} = \text{negative} \rightarrow$ negative temperature

Example Relationship between S, U, T

① ^{large} Einstein solid at high temp limit $\rightarrow q \gg N \gg 1$

$\Omega = \left(\frac{q+1}{N}\right)^N$

SA $S = k_B \ln \Omega = N k_B \ln \left(\frac{q+1}{N}\right) = N k_B + N k_B \ln \left(\frac{q}{N}\right)$

def $u = \epsilon \cdot q$

$$\begin{aligned}
 \oint S &= Nk \left[\ln \left(\frac{u}{N\epsilon} \right) + 1 \right] \\
 &= Nk \ln \left(\frac{u}{N\epsilon} \right) + Nk \\
 &= Nk \ln u - Nk \ln (N\epsilon) + Nk
 \end{aligned}$$

$$\rightarrow \frac{1}{T} = \left(\frac{\partial S}{\partial u} \right)_{N,V} = \frac{Nk}{u} - 0 + 0$$

$$\oint T = \frac{u}{Nk}$$

Recall $u = \frac{f}{2} NkT$

or

$$\boxed{u = NkT}$$

$f = 2$ because SHD has 2 dots.

② Ideal gas (monatomic)

$$S = Nk \left(\ln \left[\frac{V}{N} \left(\frac{4\pi m u}{3Nh^2} \right)^{3/2} \right] + \frac{5}{2} \right)$$

constant kills by ln()

$$T = \left(\frac{\partial S}{\partial u} \right)_{N,V}^{-1} = \left[Nk \cdot \frac{V}{N} \left(\frac{4\pi m}{3Nh^2} \right)^{3/2} \cdot \frac{3}{2} \cdot \frac{1}{u} \right]^{-1}$$

$$T = \left(\frac{7}{2} Nk \frac{1}{u} \right)^{-1} \rightarrow \boxed{u = \frac{7}{2} NkT}$$

Entropy - Heat Capacity

Mar 5, 2019

Recall: C_v = (du/dT)_v,N

1st law du = Q_add + W_on } -> du = Q_add if V constant -> W_on = 0

Now T = (du/dS)^-1 -> dS = du/T with constant volume = Q/T & dS = dQ/T

But recall dQ = C_v dT

integrate dS = C_v dT/T -> integral dS = integral C_v dT/T if temp range is small -> C_v constant -> Delta S = C_v ln(T_f/T_i)

Examp 6 Heat a cup of H2O from 20C to 100C. Calculate (200g) how much entropy increases? C_v = 1 cal/gK = 4.186 J/gK

Delta S = 4.186 J/gK * (200g) ln(373/293) approx 200 J/K

In terms of Omega -> Delta S = ln(Omega_2/Omega_1) -> Omega_2 = e^(S/k) Omega_1

Omega_2 = e^(1.5 x 10^25) Omega_1

☒ Total entropy of the system

$$\Delta S = S_f - S_{(T=0)} = \int_0^{T_f} \frac{C_v}{T} dT$$

But we need C_v at $T=0$. Guess that $S(0) \rightarrow 0$

Third Law of Thermodynamic

↳ Planck's Formalism As $T \rightarrow 0$, entropy goes to its minimum value

↳ Note this is only true for crystalline solids

Another way to state 3rd law $\boxed{\text{As } T \rightarrow 0, C_v \rightarrow 0}$

Ex ideal gas $C_v = \frac{3}{2} nR \rightarrow 0$ as $T \rightarrow 0$

☒ Macroscopic view of Entropy $\Rightarrow \boxed{dS = \frac{dQ}{T}}$

★ Example The sun heating the surface of the Earth
 $\sim 1000 \text{ W/m}^2$ $T_0 = 6000 \text{ K}$
 $T_E = 300 \text{ K}$

Estimating - energy created in 1 year by the flow of heat to the Earth's surface.

$$\Delta S_{\odot} = \frac{Q}{T} = \frac{(-1000 \text{ J/s}) (60^2) (24) (365)}{6000 \text{ K} \cdot 1 \text{ m}^2} = -1.75 \times 10^6 \text{ J/K}$$

$$\Delta S_{\oplus} = \frac{Q}{T} = \frac{(-1000 \text{ J/s}) (60^2) (24) (365)}{300 \text{ K} \cdot 1 \text{ m}^2} = +3.5 \times 10^7 \text{ J/K}$$

$$\Delta S_{tot} = \Delta S_o + \Delta S_{\oplus} = 3.3 \times 10^7 \text{ J/Km}^2$$

Suppose we plant grass on this 1 m^2 area. Does the decrease in entropy violate the 2nd law?

On $1 \text{ m}^2 \rightarrow$ maybe 10kg of grass. Let's say grass = C
 $\mu = 12 \text{ g/mol}$
 Say 1200g of grass

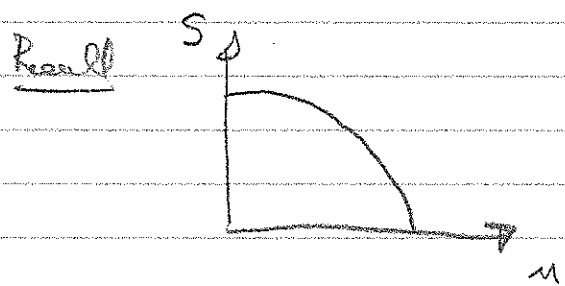
$$\rightarrow N = 1000 N_A \text{ C atoms/m}^2$$

To assemble grass out of smaller molecules.

$$S \sim Nk \sim nR = 1000R = (1000 \cdot 8.31 \text{ J/molK})$$

$$\rightarrow S \approx 10^4 \text{ J/K} \ll \Delta S_{\oplus}$$

Paramagnetism 1) Ω 2) S 3) T 4) $U(T)$ 5) C_v



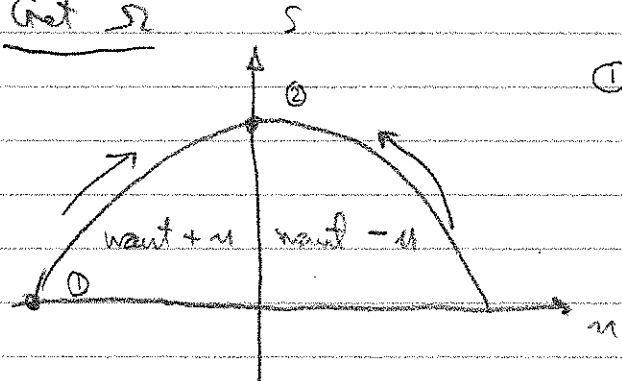
For paramagnets

$$u = \mu B (N_{\downarrow} - N_{\uparrow}) = \mu B (2N_{\downarrow} - N)$$

Question how do U, M depend on temperature

$$M = \mu (N_{\uparrow} - N_{\downarrow}) = -\frac{U}{B}$$

(*) (1) Get Ω



① all N are N_T } \rightarrow low T ,
 S vs $U \rightarrow$ steep } positive
 \rightarrow wants to absorb u

② $U_{\downarrow} = N_T = \frac{1}{2} N$. Max entropy
 $u = 0$. If it absorbs u
 $\rightarrow S$ vs U has (-) slope

Temp of paramagnet

① $u = \text{negative}$ but $\frac{\partial S}{\partial u} = \text{positive}$

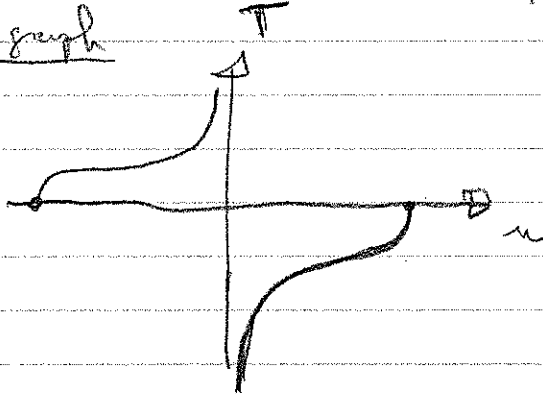
$T \uparrow \text{ as } u \uparrow$

② $u = \text{positive}$ but $\frac{\partial S}{\partial u} = \text{negative}$

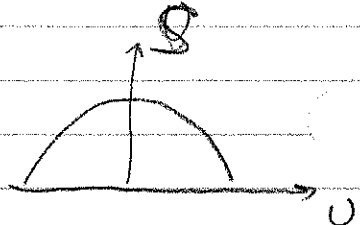
$T \downarrow \text{ as } u \uparrow$

\rightarrow system wants to give off energy

Temp graph



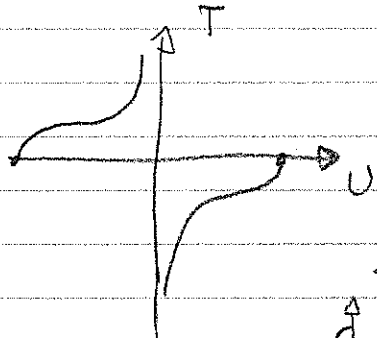
Recall $\left(\frac{\partial S}{\partial u}\right)_{N,V} = \frac{1}{T}$



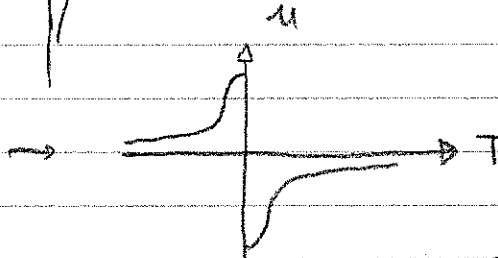
Mar 6, 2019

Recall paramagnet has a "mild" S-U graph:

So T vs U looks like



Flip the axes

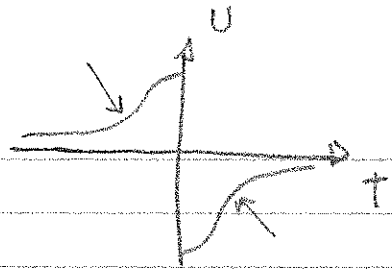


Recall

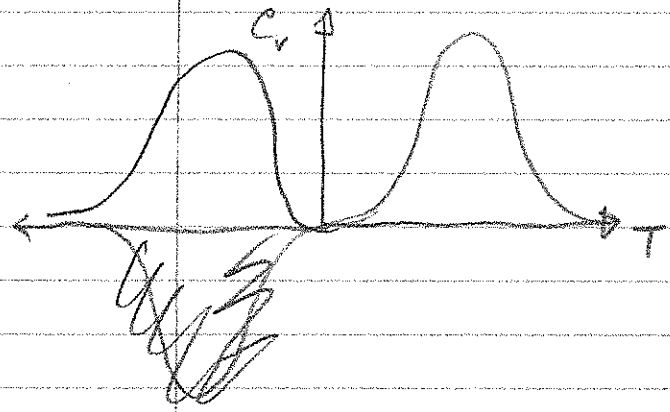
$C_V = \left(\frac{\partial U}{\partial T}\right)_{N,V}$

$\rightarrow C_V \begin{cases} C_V = \left(\frac{\partial U}{\partial T}\right)_{N,V} = 0 \text{ when } T=0 \\ C_V = 0 \text{ when } T = \pm \infty \end{cases}$

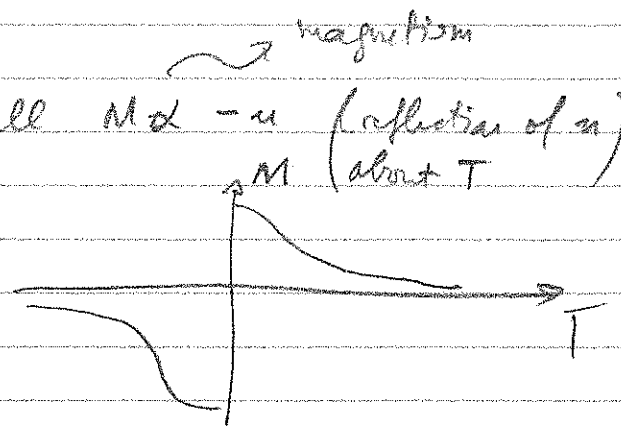
These are also an inflection points



Consider (positive) temperatures only



And recall $M \propto -u$ (reflection of u)
 (about T)



Analytic solution to paramagnet

Recall $\Omega = \binom{N}{N_T} = \frac{N!}{N_T! (N-N_T)!}$ assume $N \gg 1$

$S = k_B \ln \Omega = k_B [\ln(N!) - \ln(N_T!) - \ln((N-N_T)!)]$

Stirling's approx $\ln N! \sim N \ln N - N$

So $\frac{\partial S}{\partial N_T} = (N \ln N - N) - (N_T \ln N_T - N_T) - (N - N_T) \ln(N - N_T) + (N_T - N_T)$
 $= N \ln N - N_T \ln N_T - (N - N_T) \ln(N - N_T)$

$\frac{\partial S}{\partial N_T} = \left(\frac{\partial S}{\partial u}\right)_{N, B}$ and $u = \mu B (N - 2N_T)$

So $\left(\frac{\partial S}{\partial u}\right) = \left(\frac{\partial S}{\partial N_T}\right) \left(\frac{\partial N_T}{\partial u}\right) = (-2\mu B) \left(\frac{\partial S}{\partial N_T}\right) = \frac{-1}{2\mu B} \left(\frac{\partial S}{\partial N_T}\right)$

$\frac{\partial S}{\partial N_T} = k_B \left[-\ln N_T - 1 + \ln(N - N_T) + \frac{N - N_T}{N - N_T} \right]$

$$N_T = \frac{1}{2} \left(N - \frac{u}{\mu B} \right)$$

(60)

$$\frac{\partial S}{\partial N_T} = k \left[-\ln \left(\frac{1}{2} \left(N - \frac{u}{\mu B} \right) \right) + \ln \left(N - \frac{1}{2} N + \frac{u}{2\mu B} \right) \right]$$

= ...

$$\frac{\partial S}{\partial N_T} = k \ln \left(\frac{N + u/\mu B}{N - u/\mu B} \right)$$

$$\frac{\partial S}{\partial u} = \frac{\partial S}{\partial N_T} \frac{\partial N_T}{\partial u} = \frac{k \ln \left(\frac{N + u/\mu B}{N - u/\mu B} \right)}{-2\mu B} = \frac{1}{T}$$

$$\frac{1}{T} = \frac{k}{2\mu B} \ln \left(\frac{N - u/\mu B}{N + u/\mu B} \right) \quad T(u)$$

we can solve for $u(T)$

$$\frac{2\mu B}{kT} = \ln \left(\frac{N - u/\mu B}{N + u/\mu B} \right)$$

$$e^{2\mu B/kT} = \frac{N - u/\mu B}{N + u/\mu B} = \frac{1 - u/N\mu B}{1 + u/N\mu B}$$

$$e^{2\mu B/kT} + \frac{u}{N\mu B} e^{2\mu B/kT} = \frac{1 - u}{N\mu B}$$

$$\frac{u}{N\mu B} \left(e^{2\mu B/kT} + 1 \right) = 1 - e^{2\mu B/kT}$$

$$u(T) = N\mu B \frac{1 - e^{2\mu B/kT}}{1 + e^{2\mu B/kT}}$$

Now, simplify \rightarrow use $\sinh(x) = \frac{1}{2}(e^x - e^{-x})$, $\cosh(x) = \frac{1}{2}(e^x + e^{-x})$

$$\text{So } \tanh x = \frac{e^x - e^{-x}}{e^x + e^{-x}} = - \left(\frac{1 - e^{-2x}}{1 + e^{-2x}} \right)$$

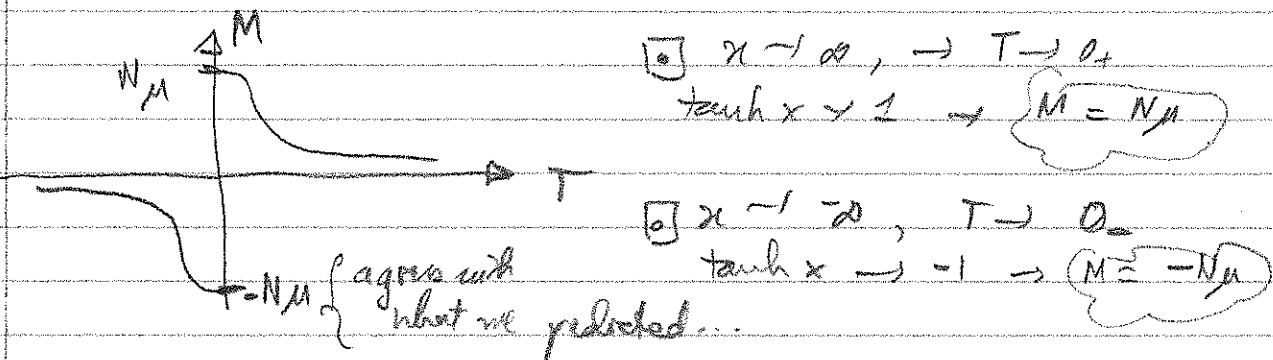
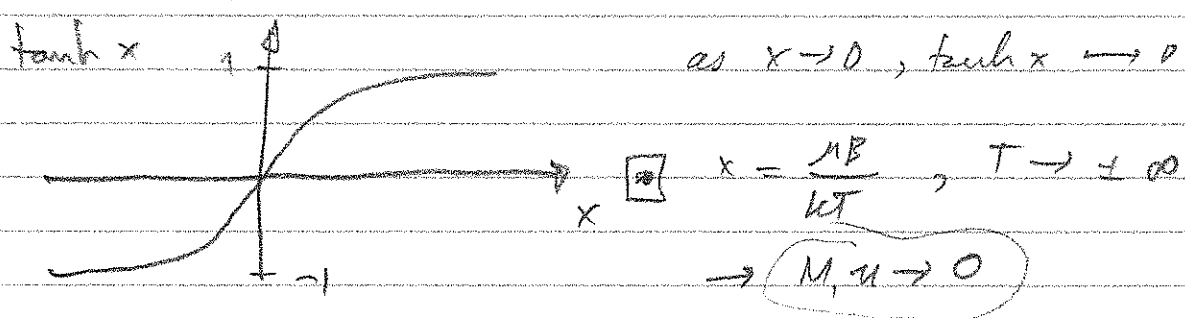
$$\text{So } \therefore \tanh x = \frac{1 - e^{-2x}}{1 + e^{-2x}}$$

Let $x = \left(\frac{\mu B}{kT} \right)$, then

$$u(T) = -\mu B N \tanh \left(\frac{\mu B}{kT} \right)$$

$$M(T) = +N\mu \tanh \left(\frac{\mu B}{kT} \right)$$

with $M = \frac{-u}{B}$



What about heat capacity of paramagnet?

$$C_B = \left(\frac{\partial U}{\partial T} \right)_{N, B}$$

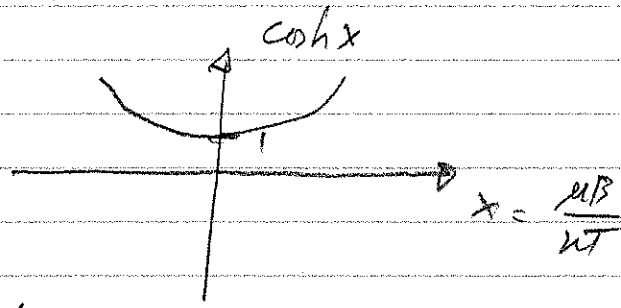
Now, $u = -N\mu B \tanh \left(\frac{\mu B}{kT} \right)$

Recall $\frac{d}{dx} \tanh(u) = \text{sech}^2(u) \cdot \frac{du}{dx} = \frac{1}{\cosh^2(u)} \frac{du}{dx}$

} \Rightarrow

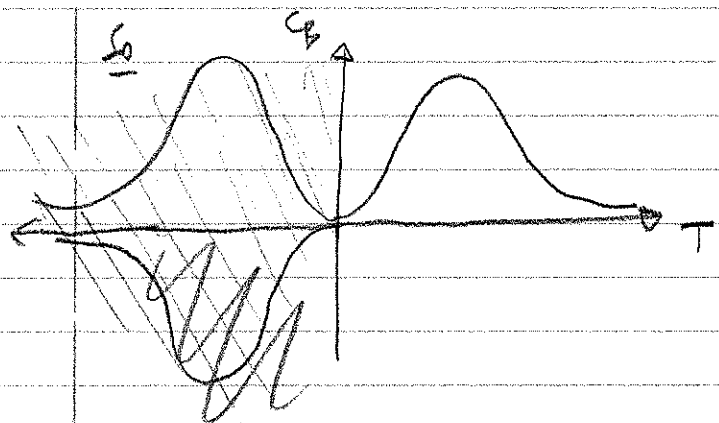
$$\left(\frac{\partial U}{\partial T}\right)_{N, B} = -N \mu_B \operatorname{sech}^2\left(\frac{\mu_B}{kT}\right) \left(\frac{-\mu_B}{kT^2}\right) = C_B$$

$$\text{So } C_B = \frac{N \mu_B^2 \left(\frac{\mu_B}{kT}\right)^2}{\cosh^2\left(\frac{\mu_B}{kT}\right)}$$



① as $x \rightarrow 0, T \rightarrow \pm \infty, \cosh(x) = 1$
 $\Rightarrow C_B \rightarrow 0$ as $T \rightarrow \pm \infty$

② as $x \rightarrow \infty, T \rightarrow 0_+, \cosh(x) \rightarrow +\infty$ (faster)
 $\text{So } C_B \rightarrow 0$ as $T \rightarrow 0$



Ex Consider two-state paramagnet.

Let $\mu = \mu_B$ Bohr magneton $\mu_B = \frac{eh}{4\pi m_e} = \frac{eh}{2m_e}$

Let $\vec{B} = 1 \text{ T}$ $\approx 5.788 \text{ eV/T}$
 $\approx 9.274 \times 10^{-24} \text{ J/T}$

then $M = ?$ $\left. \begin{aligned} \mu_B &= 5.8 \times 10^{-5} \text{ eV} \\ kT &= \frac{1}{40} \text{ eV} \end{aligned} \right\} \rightarrow \frac{\mu_B}{kT} \ll 1$

Now $\tanh(x) \approx x$ for small x

$M \approx (N \mu) \left(\frac{\mu_B}{kT}\right) = \frac{N \mu^2 B}{kT}$ \rightarrow true in "high-temperature" limit.

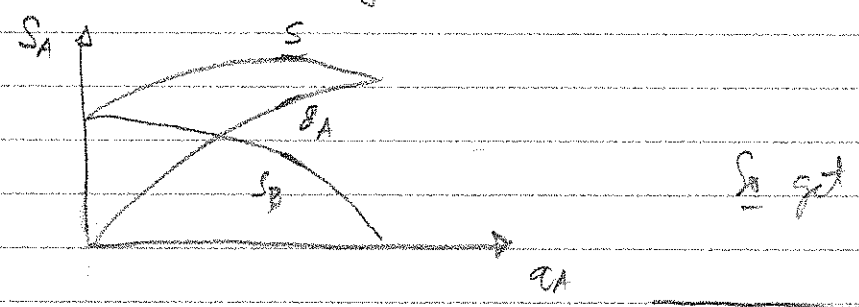
Get $M \propto \frac{1}{T}$ → Curie's Law (Pierre Curie)
(high temp limit)

Get $C_B \propto \frac{1}{T^2}$ → (high temp limit)

Mar 8, 2019

MECHANICAL EQUILIBRIUM

↳ we've been discussing dU and dS



at thermal eq $\frac{\partial S_{tot}}{\partial U} = 0 \Rightarrow \frac{\partial S_A}{\partial U_A} = \frac{\partial S_B}{\partial U_B}$ → conserved U

Consider some interacting systems that can exchange volume as well as energy



→ changes in V governed by changes in P

→ changes in U governed by change in T

as U^A, Ω^A, S^A
 U^B, Ω^B, S^B } Goal develop a relationship between $\frac{\partial S}{\partial V}$ and P

Just like dS_{tot}/dU gives thermal equilibrium

↳ $\frac{\partial S_{tot}}{\partial V} = 0 \rightarrow$ mechanical equilibrium

$$\delta \frac{\partial S_{tot}}{\partial V_A} = 0 \Rightarrow \boxed{\frac{\partial S_A}{\partial V_A} = \frac{\partial S_B}{\partial V_B}}$$

$$\frac{\partial S_{tot}}{\partial V_A} + \frac{\partial S_B}{\partial V_A} = 0, \text{ but } \partial V_A = -\partial V_B$$

Volume is conserved

Medi-equit.

What are being held constant \Rightarrow

$$\boxed{\left(\frac{\partial S_A}{\partial V_A}\right)_{U_A, N_A} = \left(\frac{\partial S_B}{\partial V_B}\right)_{U_B, N_B}}$$

Dimensional analysis.

$$\frac{[S]}{[V]} = \frac{J/k}{[m^3]} = \frac{N \cdot m/k}{m^3} = \frac{N}{m^2} \cdot \frac{1}{k} = \frac{[P]}{[T]}$$

Guess $\boxed{\left(\frac{\partial S}{\partial V}\right)_{U, N} = \frac{P}{T}}$

Look at ideal monatomic gas... $\Omega = f(N) V^N u^{3N/2}$

$$S = k \ln \Omega = k \left[\ln f(N) + \ln V^N + \ln u^{3N/2} \right]$$

$$= k \left[\ln f(N) + N \ln V + \frac{3N}{2} \ln u \right]$$

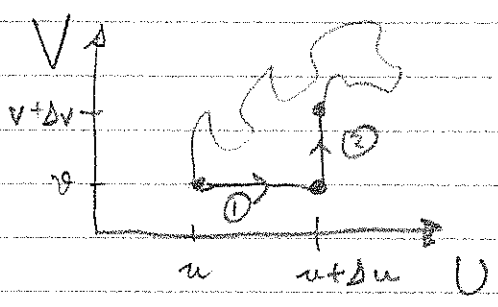
if $P \stackrel{?}{=} T \left(\frac{\partial S}{\partial V}\right)_{U, N}$, then

$$\stackrel{?}{=} T k \cdot N \cdot \frac{1}{V}$$

$\Rightarrow P \stackrel{?}{=} \frac{NkT}{V}$ works...

$$\boxed{PV = NkT} \quad \checkmark$$

We'd like to combine both of these relations for thermal and mechanical equilibrium.



Entropy is an exact differential

↳ path independent.

$$\Delta S_{tot} = \Delta S_1 + \Delta S_2$$

① Isochoric process → volume constant

② Isothermal process → temp constant or energy

$$\Delta S_{tot} = \left(\frac{\partial S}{\partial u}\right) du + \left(\frac{\partial S}{\partial v}\right) dv$$

↳ $S(u, v, N)$
 ↑ ↑ ↑
 T vol # part.

$$\partial S_{tot} = \left(\frac{\partial S}{\partial u}\right)_{v, N} du + \left(\frac{\partial S}{\partial v}\right)_{u, N} dv$$

$$= \frac{1}{T} du + \frac{P}{T} dv$$

↳

$$dU = TdS - PdV \rightarrow \text{thermodynamic identity}$$

↑ as long as N is constant.

Note this is just the first law of thermo.

$$dU = dW_{on} + dq$$

↳ For quasi-static processes → $W_{on} = -PdV$

↳ For quasi-static isothermal process → $q_{in} = \Delta S = \frac{Q}{T} \rightarrow dq = TdS$

↳ $Q = TdS$ → for any quasi-static process.
Not just isothermal

$dU = TdS - PdV$ ← more fundamental.

Now, if $u = u(S, V)$ and dU exact, then

$\frac{\partial^2 u}{\partial S \partial V} = \frac{\partial^2 u}{\partial V \partial S}$ order of diff. doesn't matter.

Then $du = \left(\frac{\partial U}{\partial S}\right)_V dS + \left(\frac{\partial U}{\partial V}\right)_S dV$

$du = TdS - PdV$

Then $\left(\frac{\partial}{\partial V}\right)_S \left(\frac{\partial U}{\partial S}\right)_V = \left(\frac{\partial}{\partial S}\right)_V \left(\frac{\partial U}{\partial V}\right)_S$
T -P

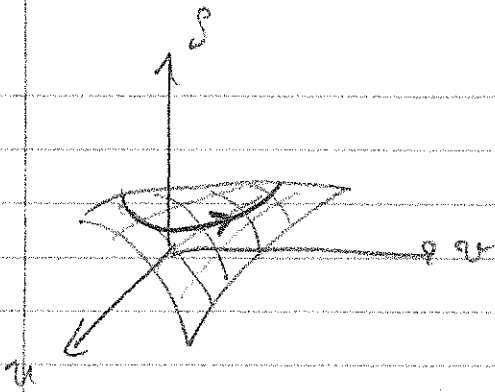
↳ $\left(\frac{\partial}{\partial V}\right)_S T = -\left(\frac{\partial}{\partial S}\right)_V P$ ← Maxwell's relation

Constant Entropy process?

If we have quasi-static process & adiabatic process (no heat leave system)
(P-equilibrates)

→ no change in Entropy

$Q = TdS = 0$ } → Isentropic { quasi static
adiabatic



$$dU = TdS - PdV$$

$$TdS = 0 = dU + PdV$$

$$dS_{tot} = 0 \text{ but } \frac{\partial S}{\partial U} \neq 0 \neq \frac{\partial S}{\partial V}$$

Recall $C_v \equiv \left(\frac{\partial U}{\partial T} \right)_{V,N}$

$$Q = C_v dT = TdS$$

$\int \Delta S = \int \frac{C_v}{T} dT$ But we want to look at constant pressure processes

$$\left(\Delta S \right)_p = \int \frac{C_p}{T} dT \rightarrow \text{more useful in many cases...}$$

Example 1L of air (N_2 & O_2) at 1 atm. Heat air until it doubles in volume - what is ΔS ?

Diatomic gas $C_v = \frac{f}{2} Nk$

$$C_p = C_v + Nk$$

For diatomic gas at room temp, $f = 5$

$$\underline{C_p} = \frac{7}{2} Nk$$

Ideal gas law $\rightarrow PV = NkT \rightarrow Nk = \frac{PV}{T} = \frac{(10^5 \text{ Pa})(1 \times 10^{-3} \text{ m}^3)}{300 \text{ K}} = \frac{1}{3} \text{ J/K}$

$\underline{C_p} = \frac{7}{2} T = 2T$

$$\oint (\Delta S)_P = \int \frac{C_P}{T} dT = C_P \ln \frac{T_f}{T_i} = C_P \ln(2)$$

$$\oint (\Delta S)_P = C_P \ln(2) = \left(\frac{7}{2} Nk\right) \ln(2) \approx 0.11 \text{ J/K}$$

Another way to do this

$$\hookrightarrow dU = TdS - PdV$$

$$\downarrow$$

$$\frac{5}{2} kN dT = TdS - \frac{NkT}{V} dV$$

~~$$\frac{5}{2} kN = T \frac{dS}{dT} - NkT$$~~

$$\frac{5}{2} kN \frac{dT}{T} = dS - \frac{Nk}{V} dV$$

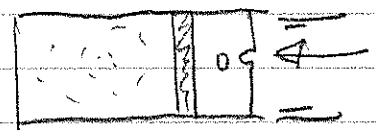
$$\oint \Delta S = \frac{5}{2} kN \ln \frac{T_f}{T_i} + Nk \ln \left(\frac{V_f}{V_i}\right)$$

$$\boxed{(\Delta S)_P = \frac{7}{2} kN \ln(2)}$$

Nov 11, 2019

Recall $dU = TdS - PdV$ \rightarrow can be used for non-quasi-static processes

① Fast compression



$dU \neq 0$. We have done work but work is greater than $-PdV$

$$dU = TdS - PdV = Q + W$$

$$\oint Q < TdS \rightarrow \boxed{dS > \frac{Q}{T}} \rightarrow \text{added entropy}$$

② Free-expansion



vacuum \rightarrow allows gas expand into vacuum

$$W=0, \quad d=0 \quad \text{to} \quad dD=0 \quad \begin{array}{l} \text{was quasi} \\ \text{static} \\ \downarrow \end{array}$$

$$\int dU = TdS - PdV = 0 \Rightarrow TdS = PdV > 0 \quad (W \neq PdV)$$

\hookrightarrow we added entropy

Example

Fast compression of air at $P = 1 \text{ atm}$, $T = 300 \text{ K}$
 $= 10^5 \text{ Pa}$



$$F = 2000 \text{ N}$$

$$A = 0.01 \text{ m}^2 \quad V = 1 \text{ L}$$

$$n = \frac{1}{25} \text{ mol}$$

Say piston moves 1 mm before it stops...

$$\bullet \text{ If this is quasi-static } W = \int PdV = \int -\frac{nRT}{V} dV = nRT \ln \frac{V_i}{V_f}$$

$$W = nR \ln \frac{V_i}{V_f}$$

$$V_i = \frac{1.00 \text{ L}}{1000}, \quad V_f = \frac{1.00 - (0.001)(0.01)}{1000}$$

Work actually done

$$W = F \cdot d = (2000 \text{ N})(0.001 \text{ m}) = 2 \text{ J}$$

$> -PdV$

Fast compression Adiabatic $\rightarrow Q=0$

$$\Rightarrow \Delta U = Q + W = 0 + W = 2 \text{ J}$$

How does S change?

$$dU = TdS - PdV$$

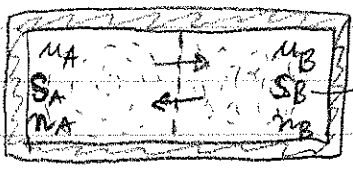
$$\Delta S = dS = \frac{\Delta U + PdV}{T} = \frac{2 \text{ J} + (10^5 \text{ Pa})(-0.01 \text{ m}^2)(0.001 \text{ m})}{300 \text{ K}} \approx \frac{1}{300} \frac{\text{J}}{\text{K}}$$

Diffusive Equilibrium

Thermal equil $\rightarrow T$ same

Mech equil $\rightarrow P$ same

Diffusive equil $\rightarrow N$ same (μ)



assume same gas

Assume V constant, Assume that gases can exchange energy and particles, Assume same gas on both sides...

$$U_{tot} = N_{tot} = P_{tot}$$

$$S_{tot} = S(u_A, N_A)$$

Before $\bullet \left(\frac{\partial S_{tot}}{\partial P_A} \right)_{N,V} = \left(\frac{\partial S_{tot}}{\partial P_B} \right)_{N,V} = 0$ at equilibrium. thermal

$\bullet \left(\frac{\partial S_{tot}}{\partial N_A} \right)_{U,V} = \left(\frac{\partial S_{tot}}{\partial N_B} \right)_{U,V} = 0$ at diffusive eq.

$\bullet \left(\frac{\partial S_A}{\partial N_A} \right)_{U,V} = \left(\frac{\partial S_B}{\partial N_B} \right)_{U,V} = 0$ at equilibrium.

Butler not N , but μ

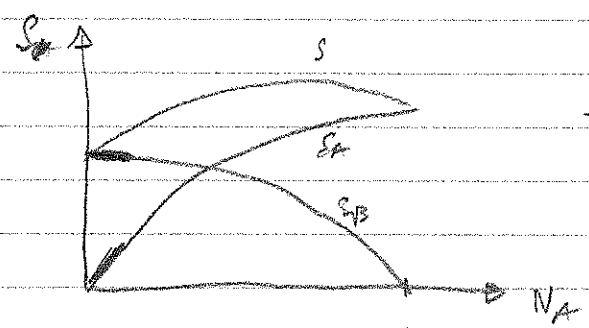
μ : Chemical potential (μ) has units of energy [J]

Relating $\frac{\partial S}{\partial N}$ to μ $\bullet \left(\frac{\partial S}{\partial N} \right)$ multiply by temperature to get μ

\uparrow \uparrow
 $\frac{J/K}{\#}$ J

$$\mu = -T \left(\frac{\partial S}{\partial N} \right)_{U,V}$$

At equilibrium $\mu_A = \mu_B$. Consider S vs. N



→ particles will flow from system with lower $\frac{\partial S}{\partial N}$ to higher $\frac{\partial S}{\partial N}$

Since, larger $\left(\frac{\partial S}{\partial N}\right) \rightarrow$ smaller μ .

→ particles flow from system with high to low μ

$\mu \rightarrow$ concentration / density of gas...

Generalized Thermodynamic identity

$S = S(U, N, V)$

$$dS = \left(\frac{\partial S}{\partial U}\right)_{N,V} dU + \left(\frac{\partial S}{\partial N}\right)_{U,V} dN + \left(\frac{\partial S}{\partial V}\right)_{U,N} dV$$

$$= \frac{1}{T} dU + \frac{\mu}{T} dN + \frac{P}{T} dV$$

$$\oint TdS = dU - \mu dN + PdV$$

$$\oint dU = TdS + \mu dN - PdV$$

if quasi-static... \rightarrow "heat" "chem work" "mech work"

When U, V constant $\rightarrow \mu = -T \left(\frac{\partial S}{\partial N}\right)$
 when, S, V constant $\rightarrow \mu = \left(\frac{\partial U}{\partial N}\right)_{S,V}$ } ΔE due to change in N

Normally, to keep $\Delta S = 0$, if we $\uparrow N$, need to $\downarrow \epsilon$

e.g. Einstein solid w. $N=3, q=3$

$$\Omega = \binom{3+2 \cdot 1}{3} = 10$$

Then

$S = k \ln \Omega$. If we $\uparrow N$ by 1, $N=4$

$$\text{Then } \Omega' = \binom{4+3-1}{3} = 20 \quad S' = k \ln 20 > S.$$

To keep S constant \rightarrow need to decrease $q \rightarrow q=2$

$$\Omega'' = \binom{4+2-1}{2} = 10 \text{ so that } S'' = S$$

$$\left. \begin{aligned} \Delta U &= q_i \epsilon - q_f \epsilon = 2\epsilon_i - 3\epsilon_i = -\epsilon \\ \Delta N &= 1 \end{aligned} \right\} \frac{\partial U}{\partial N} = -\epsilon$$

$$\frac{\partial \mu}{\partial \epsilon} = - \left(\frac{\partial U}{\partial N} \right)_{\epsilon, V} = \frac{-\epsilon}{1} = -\epsilon$$

Nov 12, 2019

Chemical potential of ideal gas (monatomic)

$$\mu = -T \left(\frac{\partial S}{\partial N} \right)_{U, V} \quad S = Nk \left[\ln \left(V \left(\frac{4\pi m U}{3h^2} \right)^{3/2} \right) - \ln N^{5/2} \frac{5}{2} \right]$$

$$\mu = -T \left\{ k \left[\ln \left(V \left(\frac{4\pi m U}{3h^2} \right)^{3/2} \right) - \ln N^{5/2} \frac{5}{2} \right] + Nk \left[0 - \frac{5}{2} \frac{1}{N} \right] \right\}$$

$$\mu = -T k \ln \left[\frac{V}{N} \left(\frac{4\pi m U}{3N h^2} \right)^{3/2} \right]$$

$$\text{But } u = \frac{3NkT}{2}$$

$$\mu = -T k \ln \left[\frac{V}{N} \left(\frac{2\pi m k T}{h^2} \right)^{3/2} \right]$$

$\frac{d\mu}{P}$

Ex for He at room temp - 1 atm. $\rightarrow \mu = -0.32 \text{ eV}$

higher $\mu \rightarrow$ higher concentration \rightarrow more likely to give off particles

What about for a mixture of gases?

$$\mu_1 = -T \left(\frac{\partial S}{\partial N_1} \right)_{U, V, N_2} \rightarrow \text{total}$$

$$\mu_2 = -T \left(\frac{\partial S}{\partial N_2} \right)_{U, V, N_1}$$

Thermo identity $\rightarrow dD = T dS - P dV + \sum_i \mu_i dN_i$

In diffusive equilibrium $\rightarrow \mu_A = \mu_B, \mu_{CA} = \mu_{CB}, \dots$
 where $\begin{cases} A, B \rightarrow \text{systems} \\ 1, 2, \dots \rightarrow \text{species of atoms/molecules} \end{cases}$

Notes Characterise $\mu = -T \left(\frac{\partial S}{\partial N} \right)_{U, V} \rightarrow \# \text{ molecules}$ $n = \frac{N}{N_A}$

In a mixture of ideal gases, each μ_i behaves as if the other species weren't present. At constant partial pressure

$$P_i = x_i P$$

De Rive court Practica $\rightarrow x_i = \frac{N_i}{N_{\text{tot}}}$

Now $P_i = x_i P = \frac{N_i}{N_{tot}} \frac{N_{tot} RT}{V} = \frac{N_i}{N_{tot}} \frac{N_{tot} RT}{V} = \boxed{N_i \frac{RT}{V} = P_i}$

Now, consider 2 gases A & B → mixture occupying the same volume V

$$S_{tot} = S_A + S_B = S(U_A, V, N_A) + S(U_B, V, N_B)$$

if we hold u constant at equilibrium, then this is the same as holding u_A & u_B constant.

$$\mu_A = -T \left(\frac{\partial S_{tot}}{\partial N_A} \right)_{U, V, N_B} = -T \left(\frac{\partial S_A}{\partial N_A} \right)_{U, V} \quad (\text{since } \partial S_B = 0)$$

same as if B not present

Chemical Potential of A Large Einstein Solid

$$\Omega = \binom{q+N-1}{q} = \frac{(q+N-1)!}{q!(N-1)!} = \frac{(q+N)! N}{(q+N) N! q!}$$

note $(N-1)! = \frac{N!}{N}$

Stirling's approximation → $N! \approx N^N e^{-N} \sqrt{2\pi N}$

$$\Omega \approx \frac{(q+N)^{q+N} e^{-q-N} \sqrt{2\pi(q+N)}}{(q+N)} \cdot \frac{N}{q^q e^{-q} \sqrt{2\pi q} N^N e^{-N} \sqrt{2\pi N}}$$

$$= \frac{(q+N)^{q+N}}{q^q N^N} \sqrt{\frac{N}{2\pi q(q+N)}} \approx 1$$

$$\approx \left(\frac{q+N}{q} \right)^q \left(\frac{q+N}{N} \right)^N \approx \boxed{\left(\frac{q+N}{q} \right)^q \left(\frac{q+N}{N} \right)^N}$$

$$S = k \ln \Omega = q k \ln \left(\frac{q+N}{q} \right) + N k \ln \left(\frac{q+N}{N} \right)$$

$$S = k q \ln \left(1 + \frac{N}{q} \right) + N k \ln \left(\frac{q}{N} + 1 \right)$$

$$\frac{\partial S}{\partial N} = k q \frac{1}{1 + N/q} \cdot \frac{1}{q} + k \ln \left(\frac{q}{N} + 1 \right) + N k \frac{1}{1 + \frac{q}{N}} \cdot \left(-\frac{q}{N^2} \right)$$

$$\frac{\partial S}{\partial N} = k \ln \left(1 + \frac{q}{N} \right)$$

chemical potential of = $\mu = kT \ln \left(1 + \frac{q}{N} \right)$
Einstein solid

$$\mu = -T \left(\frac{\partial S}{\partial N} \right)_{U,V} = -kT \ln \left(1 + \frac{q}{N} \right)$$

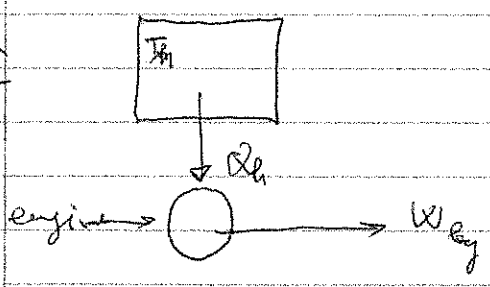
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ur 15, 2019

Ch. 4 ASAT ENGINE & REFRIGERATOR

Concept → absorb Q. Convert to mechanical W

Consider



Design considerations

- ① Want to start & end at the same macrostate (energy) → cyclic on PV diagram

$$\Delta u = 0$$

- ② Must obey 1st law of thermodynamics

$$\Delta U = Q_{\text{absorb}} - W_{\text{eng}}$$

- ③ Must obey 2nd law of thermodynamics $\Delta S \geq 0$

• If turns out that it is impossible to convert 100% of absolute Q into usable work because we have heat flow.

→ Look at entropy of system.

$$\left\{ \begin{array}{l} \text{For reversible engine, want } \Delta S_{\text{engine}} = 0 \\ \Delta S_{\text{reservoir}} = \frac{-Q_h}{T_h} \geq 0 \end{array} \right.$$

1st law

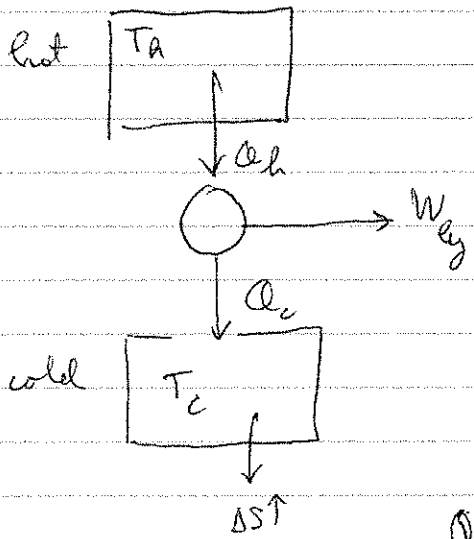
$$\Delta U = Q_{\text{abs}} - W_{\text{by}} \Rightarrow Q_{\text{abs}} = W_{\text{by}}$$

$$\Delta S_{\text{system}} = \Delta S_{\text{engine}} + \Delta S_{\text{reservoir}} = \frac{-Q_h}{T_h} = \frac{-W_{\text{by}}}{T_h} \geq 0$$

But then W_{by} has to be negative...

Result: cannot build an engine with a single reservoir that converts heat into work

To fix this



• Assume cyclic engine $\Delta u = 0$

$$\Delta u_h - \Delta u_c = 0$$

$$Q_h - Q_c - W_{\text{by}} = 0$$

$$W_{\text{by}} = Q_h - Q_c$$

work done by the engine.

$Q_h = Q$ absorbed by the ~~total~~ engine

$W_{\text{by}} = W$ done by engine.

$Q_c = Q$ expelled by the engine

Efficiency

$$e = \frac{W_{net}}{Q_{in}} = \frac{W_{net}}{Q_h}$$

Req

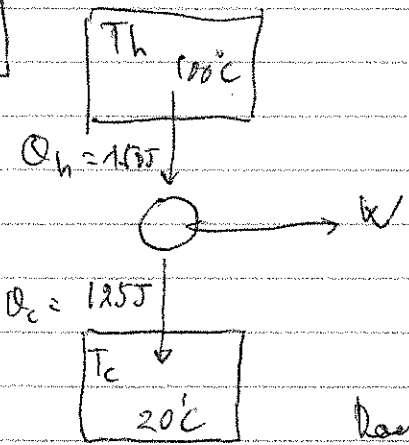
$$e = \frac{Q_h - Q_c}{Q_h} = 1 - \frac{Q_c}{Q_h}$$

$$\Delta S_{hot\ res} = -\frac{Q_h}{T_h}, \quad \Delta S_{cold\ res} = \frac{Q_c}{T_c}$$

$$\Delta S \geq 0 \Rightarrow \frac{Q_c}{T_c} \geq \frac{Q_h}{T_h}$$

$$e \leq 1 - \frac{T_c}{T_h}$$

Example



Assume $\Delta u = 0$
 $W = 150J - 125J = 25J$

$$Q_{abs} = Q_h - Q_c$$

$$e = \frac{W_{net}}{Q_h} = \frac{25}{150} = \frac{1}{6}$$

Does this engine reach maximum eff?

$$\text{Max } e = 1 - \frac{T_c}{T_h} = 1 - \frac{20+273}{100+273} = 21.4\%$$

B

No, doesn't reach maximum efficiency.

Carnot Cycle → towards a more efficient engine.

• To avoid creating excess entropy in an engine.

$T_{engine} = T_h$ → not possible.

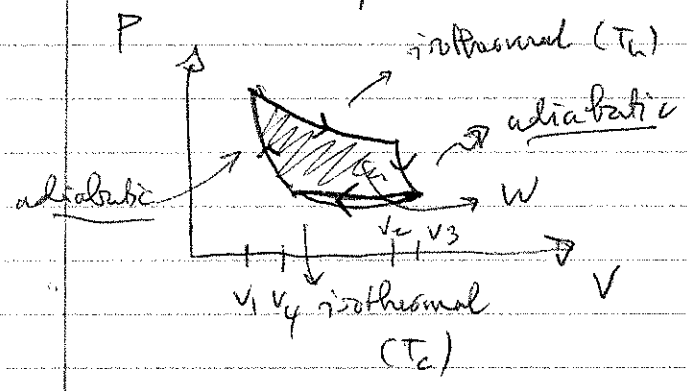
Instead, we want T_{engine} just slightly below T_h

⇒ let it expand isothermally to keep $T_{engine} \sim$ constant

• after isothermal expansion → bring temp of engine down to T_c ($T_{engine} > T_c$ slightly)

→ Want [adiabatic expansion] (to avoid additional heat flow)

↳ repel waste heat during an isothermal compression.



Carnot Cycle

- (1) Isothermal ^{expansion} @ T_h
- (2) Adiabatic expansion to get T_c
- (3) Isothermal compression @ T_c (waste heat dump)
- (4) Adiabatic compression to bring engine back to T_h .

$$(1) Q_h = W_{eng} = \int_{V_1}^{V_2} PdV = \int_{V_1}^{V_2} \frac{NRT_h}{V} dV = NRT_h \ln \frac{V_2}{V_1}$$

$$(C_{V_3} > C_{V_4}) Q_c = - \int_{V_3}^{V_4} PdV = -NRT_c \ln \left(\frac{V_4}{V_3} \right) = NRT_c \ln \left(\frac{V_3}{V_4} \right)$$

$$\eta = 1 - \frac{Q_c}{Q_h} = 1 - \frac{\ln(V_3/V_4) \cdot T_c}{\ln(V_2/V_1) \cdot T_h}$$

Now, for adiabatic processes

$$\hookrightarrow VT^{\gamma} = \text{constant}$$

$$\circ V_3 T_c^{\gamma} = V_2 T_h^{\gamma} \quad \& \quad V_4 T_c^{\gamma} = V_1 T_h^{\gamma}$$

$$\circ \frac{V_3 T_c^{\gamma}}{V_4 T_c^{\gamma}} = \frac{V_2 T_h^{\gamma}}{V_1 T_h^{\gamma}} \Rightarrow \frac{V_3}{V_4} = \frac{V_2}{V_1} \Rightarrow \frac{\ln(V_3/V_4)}{\ln(V_2/V_1)}$$

$$\eta = 1 - \frac{T_c}{T_h}$$

→ assuming adiabatic

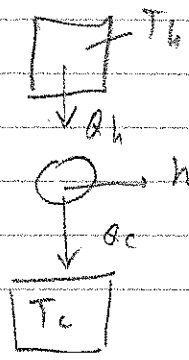
→ Carnot cycle produces max efficiency

or

Nov 18, 2019

Heat Engines

Recall



Cyclic process → Δu = 0


$$W_{eng} = Q_{in} - Q_{out}$$

$$\eta = \frac{Q_{in} - Q_{out}}{Q_{in}} = \frac{W_{eng}}{Q_{in}} = 1 - \frac{Q_{out}}{Q_{in}}$$

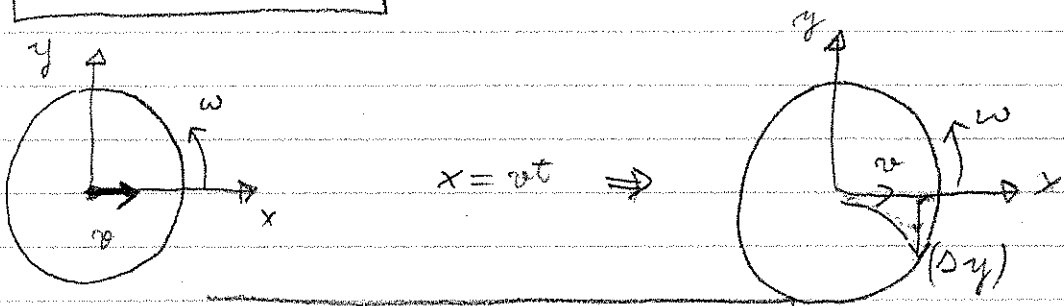
Since $\Delta S \geq 0$, $\eta \leq 1 - \frac{T_c}{T_h}$ equality holds when Carnot engine

Hurricanes as Heat Engines

Hot reservoir \rightarrow ocean surface
 Cold reservoir \rightarrow atmosphere.

 \rightarrow Low pressure system with circulation due to Coriolis effect

$F_c = 2m\mathbf{v} \times \boldsymbol{\omega}$



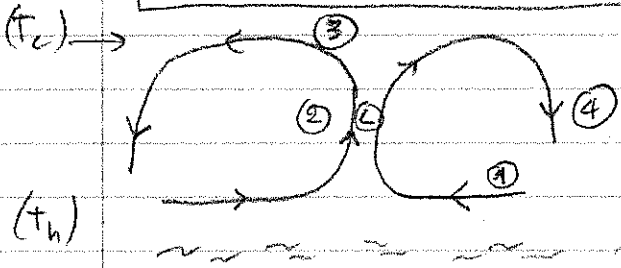
$\Delta y = (\omega t) x$

Coriolis acceleration \uparrow

But since $x = vt \rightarrow \Delta y = \omega vt^2 = \frac{1}{2} (2\omega v) t^2 = \frac{1}{2} a_c t^2$

Steps of Hurricane engine

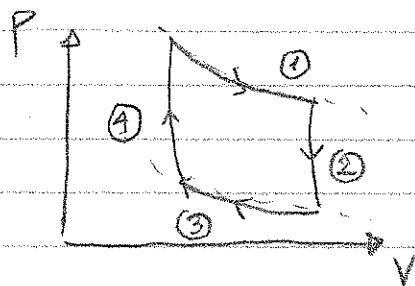
\rightarrow same as Carnot's...



- (1) Isothermal expansion of air over hot ocean ($T \approx 300K$)
- (2) Adiabatic expansion \rightarrow air moves rapidly up eyewall up to tropopause

- (3) Isothermal compression in tropopause ($T \approx 200K$)
- (4) Adiabatic compression of dry air

On PV diagram



Work produced by thermians dissipated by friction

$$W = F_{\text{drag}} \cdot x$$

$\propto v^2$ (turbulent flow)

$$\frac{dW}{dt} = (av^2)v \approx av^3$$

Heat transfer from the ocean by forced convection. $Q_h \propto v$

$$\text{Total: } Q_h = av^3 + bv \rightarrow Q_{\text{ocean}}$$

\downarrow
Q due to friction

$$e = \frac{W_{\text{net}}}{Q_{\text{in}}} = \frac{av^3}{av^3 + bv} = 1 - \frac{T_c}{T_h} \rightarrow \text{Carnot engine}$$

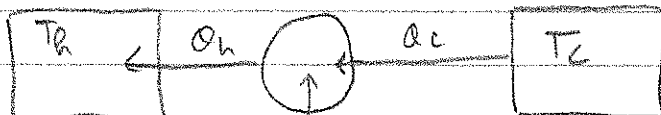
⇒ Can solve for v.

$$\frac{av^3}{av^3 + bv} = 1 - \frac{T_c}{T_h} \Rightarrow av^3 = (av^3 + b) \left(1 - \frac{T_c}{T_h}\right) = av^3 \left(1 - \frac{T_c}{T_h}\right) + b \left(1 - \frac{T_c}{T_h}\right)$$

$$av^3 \left(\frac{T_c}{T_h}\right) = b \left(1 - \frac{T_c}{T_h}\right)$$

$$v = \sqrt{\frac{b}{a} \left(\frac{T_h}{T_c} - 1\right)}$$

Refrigerator



Work done on substance, to pull heat out cold reservoir

⇒ expel waste heat to heat reservoir.

Now, $\Delta u = 0 \Rightarrow Q_c + W_{in} = Q_h$
 ↓ compression work.

Coefficient of Performance

$COP = \frac{Q_c}{W_{in}}$ replace $W_{in} = Q_h - Q_c$

$COP = \frac{Q_c}{Q_h - Q_c} = \frac{1}{Q_h/Q_c - 1} \geq 1$

2nd law, $\Delta S \geq 0 \Rightarrow \frac{Q_h}{T_h} - \frac{Q_c}{T_c} \geq 0 \Rightarrow \frac{Q_h}{Q_c} \geq \frac{T_h}{T_c}$

$COP = \frac{1}{Q_h/Q_c - 1} \leq \frac{1}{T_h/T_c - 1}$

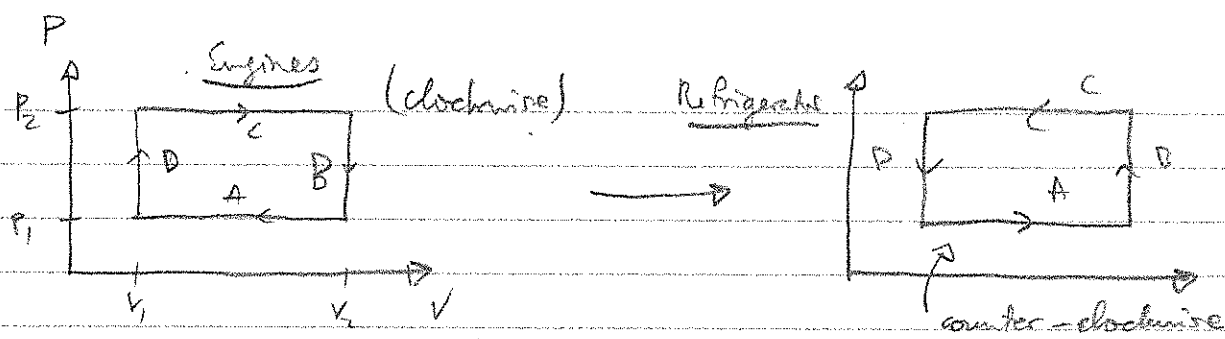
Carnot cycle once again creates the most efficient refrigerator

Need $\left\{ \begin{array}{l} T \geq T_h \text{ during heat expulsion} \\ T \leq T_c \text{ during heat absorption} \end{array} \right.$

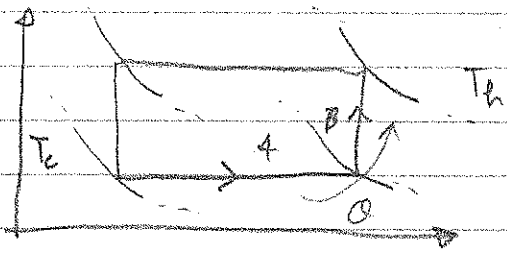
Example what is the max possible COP for a standard AC unit?

Let $T_{in} = 22^\circ C$ then $COP_{max} = \frac{1}{\frac{30+273}{22+273} - 1} \approx \underline{\underline{36.9}}$
 $T_{out} = 30^\circ C$

PV diagram



But



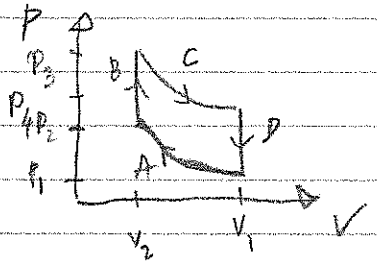
Need $T_c > T_h$ for heat flow A, B } not going to work
 and $T_h < T_c$ for heat flow C, D }

→ Need adiabatic processes

lec 19, 2019

Real Heat Engines

Example Internal Combustion Engine (Otto cycle)



A, C → adiabats.

- A: adiabatic compression of air + fuel
- B: spark plug ignites the mixture, increasing T, P, holding V constant
- C: adiabatic expansion inside cylinder due to high pressure
- D: hot exhaust is expelled and replaced by new mixture at lower temperature

Efficiency of this engine?

$$e = 1 - \frac{Q_c}{Q_h}$$

Steps A₂C are adiabatic $\rightarrow Q = 0$
 B $\rightarrow Q_h$
 D $\rightarrow Q_c$

Step B $\Delta U_B = Q + W \rightarrow Q = \frac{f}{2} NkT = \frac{f}{2} PV = \frac{f}{2} V_2 (P_3 - P_2)$

Step D $\Delta U_D = Q_c + W = -\frac{f}{2} NkT \rightarrow Q_c = \frac{f}{2} V_2 (P_4 - P_1)$

So,
$$e = 1 - \frac{Q_c}{Q_h} = 1 - \frac{V_1 (P_4 - P_1)}{V_2 (P_3 - P_2)}$$

But more convenient with temperatures...

Adiabatic $\Rightarrow P_4 V_1^\gamma = P_3 V_2^\gamma \text{ \& } P_1 V_1^\gamma = P_2 V_2^\gamma$

So $(P_4 - P_1) V_1^\gamma = (P_3 - P_2) V_2^\gamma$

A $\frac{P_4 - P_1}{P_3 - P_2} = \frac{V_2^\gamma}{V_1^\gamma} = \left(\frac{V_2}{V_1}\right)^\gamma$

B
$$e = 1 - \frac{V_1 V_2^\gamma}{V_2 V_1^\gamma} = 1 - \left(\frac{V_2}{V_1}\right)^{\gamma-1}$$

So
$$e = 1 - \left(\frac{V_2}{V_1}\right)^{\gamma-1}$$

Compared to Carnot engine:
$$e = 1 - \frac{T_c}{T_h} = e = 1 - \frac{T_1}{T_3}$$

Remember that $TV^{\gamma-1} = \text{constant}$ for an adiabat $\Rightarrow \frac{T_1}{T_2} = \left(\frac{V_2}{V_1}\right)^{\gamma-1}$

$$\rightarrow e = 1 - \frac{T_1}{T_2}$$

or, another adiabatic $\rightarrow T_3 V_2^{\gamma-1} = T_4 V_1^{\gamma-1}$

$$\frac{T_4}{T_3} = \left(\frac{V_2}{V_1}\right)^{\gamma-1} \quad \underline{\Delta} \quad \boxed{e = 1 - \frac{T_4}{T_3}}$$

Note $\frac{T_4}{T_3} < \frac{T_1}{T_2}$ and $\frac{T_1}{T_3} < \frac{T_2}{T_3}$

$$\underline{\Delta} \quad \boxed{e_{Otto} < e_{Carnot}}$$

So { Otto cycle will always be less efficient than Carnot engine }
with the same T

Revisiting 3rd Law

↳ Planck's statement = "as $T \rightarrow 0$, $S \rightarrow S_{min}$, $S_{min} = 0$ for pure crystalline solids."

Einstein statement

↳ "As $T \rightarrow 0$, S remains finite"

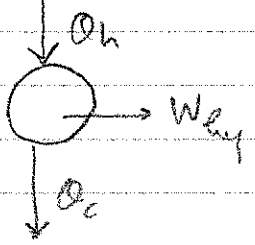
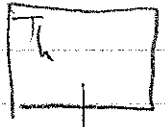
$$\underline{\Delta} \quad S = \int_0^T \frac{C_V}{T} dT \quad \text{if } C_V \rightarrow 0 \text{ then } S \rightarrow S_{min} = -\infty$$

Nernst unattainability principle

↳ "Any thermodynamic process cannot reach absolute zero in a finite number of steps in a finite amount of time"

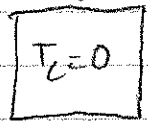
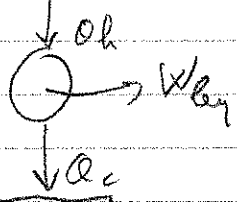
- 1st Law tells us we can't get work for free
- 2nd Law tells us we can't build a monothermal heat engine
- 3rd Law tells us we can't get 100% conversion of heat to work even if $\Delta S = 0$

Einstein



$Q_h = W_{piston}$ Einstein's statement
S finite at $T=0$

Nernst



If you want $\Delta S = 0$, Nernst says can't get engine to $T=0$ in finite time

4

ch 5 → FREE ENERGY

Enthalpy → useful at constant P

$H \equiv U + PV \Rightarrow dH = dU + PdV$

or $\Delta H = \Delta U + P\Delta V$

$Q + W_{on}$
 \downarrow
 $-P\Delta V + W_{other}$

$\Delta H = Q + W_{other}$

Helmholtz free energy (F)

used for constant T processes.

$$F \equiv U - TS$$

create system out of nothing

Q = TΔS, quasistatic

$$S_{final} = 0$$

Gibbs free energy (G)

used for constant T, P

$$G \equiv U - TS + PV = H - TS$$

Nov 30, 2019

Recall Thermodynamic Potential U, H, F, G

Look at changes in these: $F \equiv U - TS \Rightarrow dF = dU - SdT - TdS$

For F, T constant $\Rightarrow \Delta F = \Delta U - T\Delta S$ can write...

$$\Delta F = Q_{in} + W_{on} - T\Delta S \quad \text{Now } Q_{in} \leq T\Delta S \text{ (in general)}$$

$$\Delta F \leq W_{on} \quad (\text{constant T, equality when quasistatic})$$

can be expansion/compression work = $\int PdV + \text{others}$

Gibbs free energy $\Rightarrow G \equiv U - TS + PV \Rightarrow dG = dU - TdS - SdT + PdV + VdP$

$$\text{constant T, P} \Rightarrow dG = dU - TdS + PdV$$

$$Q_{in} + W_{on}, Q_{in} \leq T\Delta S, W_{on} = -PdV + W_{other}$$

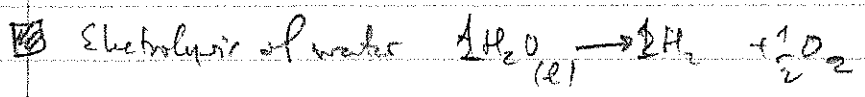
So

$$\Delta G \leq W_{other}$$

$$\Delta H = \Delta U + PdV = Q_{in} + W_{other} = Q_{in} + W_{on}$$

$$\Delta G = \Delta H - T\Delta S$$

Ex of using ΔG



$\Delta H_p = -286 \text{ kJ/mol}$

How much work do we need to supply to get reaction to proceed?

Change in S: $S_{\text{H}_2\text{O}(l)} = 70 \text{ J/K}$
 $S_{\text{H}_2(g)} = 131 \text{ J/K}$
 $S_{\frac{1}{2}\text{O}_2(g)} = 205 \text{ J/K}$

$\Delta S = (131 \text{ J/K} + \frac{1}{2} \cdot 205 \text{ J/K}) - 70 \text{ J/K} = 163 \text{ J/K}$

Max amount of heat that can enter system = $T\Delta S = 49 \text{ kJ}$

$\Delta G = \Delta H - T\Delta S = 286 \text{ kJ} - 49 \text{ kJ} = \boxed{\Delta G = 237 \text{ kJ}}$

Thermodynamic identities

$dU = TdS - PdV + \mu dN \Rightarrow u(S, V)$

$dU = \left(\frac{\partial U}{\partial S}\right)_{V, N} dS + \left(\frac{\partial U}{\partial V}\right)_{S, N} dV$

$\frac{\partial^2 u}{\partial S \partial V} = \frac{\partial^2 u}{\partial V \partial S} \Rightarrow \frac{\partial}{\partial V} \left[\left(\frac{\partial U}{\partial S}\right)_{V, N} \right]_{S, N} = \frac{\partial}{\partial S} \left[\left(\frac{\partial U}{\partial V}\right)_{S, N} \right]_{V, N}$

① $\boxed{\left(\frac{\partial T}{\partial V}\right)_{S, N} = -\left(\frac{\partial P}{\partial S}\right)_{V, N}}$ \rightarrow independent variables S, V
Maxwell's relation # 1

② $dU = TdS - PdV = TdS - d(PV) + VdP \rightarrow d(U+PV) = TdS + VdP$

$dH = TdS + VdP$ \rightarrow how to get ΔH at non-standard P, T, \dots
 $+ \mu dN$

H = H(S, P)

dH = (dH/dS)_{P,N} dS + (dH/dP)_{S,N} dP

T = (dH/dS)_{P,N} ; V = (dH/dP)_{S,N}

d/dP (dH/dS)_{P,N} = d/dS (dH/dP)_{S,N}

(dT/dP)_{S,N} = (dV/dS)_{P,N} -> Maxwell's relation #2

3 Independent variables T, V

dU = TdS - PdV = d(TS) - SdT - PdV

d(U - TS) = -SdT - PdV

dF = -SdT - PdV

Here F(T, V)

dF = (dF/dT)_{V,N} dT + (dF/dV)_{T,N} dV

S = -(dF/dT)_{V,N} , P = -(dF/dV)_{T,N}

$$\frac{\partial}{\partial V} \left(\frac{\partial F}{\partial T} \right) = \frac{\partial}{\partial T} \left(\frac{\partial F}{\partial V} \right)$$

$$-\left(\frac{\partial S}{\partial V} \right)_{T,N} = - \left(\frac{\partial P}{\partial T} \right)_{V,N}$$

$$\left(\frac{\partial S}{\partial V} \right)_{T,N} = \left(\frac{\partial P}{\partial T} \right)_{V,N}$$

4) Independent variables : T & P

$$dU = TdS - PdV = d(TS) - SdT - d(PV) + VdP$$

$$d(U - TS + PV) = -SdT + VdP$$

$$dG = -SdT + VdP$$

$$V = \left(\frac{\partial G}{\partial P} \right)_{T,N}, \quad S = - \left(\frac{\partial G}{\partial T} \right)_{P,N}$$

and

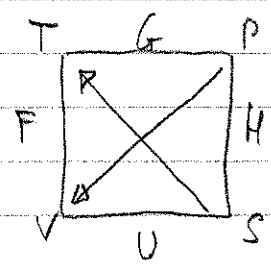
$$\left(\frac{\partial V}{\partial T} \right)_{P,N} = \left(\frac{\partial S}{\partial P} \right)_{T,N}$$

Mar 23, 2019

Thermodynamics Potentials U, H, F, G

"good physicists have studied under very fine teachers"

Use square



$$dH = VdP + TdS + mdN$$

$$dU = TdS - PdV + mdN$$

Write potentials as fn of vars on that side of square

cells diagonal
signs + across
pt to (-) diffe

Maxwell's Relations

$$L = -L \rightarrow \left(\frac{\partial T}{\partial V}\right)_S = -\left(\frac{\partial P}{\partial S}\right)_V$$

arrow point to minus sign for the constant variable.

Definition of Enthalpy From squares

$$H = U + PV \quad \curvearrowright, \text{ against arrow } \rightarrow (+)$$
$$G = H - TS$$
$$= U + PV - TS$$

Usefulness of Maxwell's Relations

Can derive a relationship between C_p & C_v for any substance

Reminder $C_v = \left(\frac{\partial U}{\partial T}\right)_V$

$$C_p = \left(\frac{\partial H}{\partial T}\right)_P$$

① Start by writing S in terms of T, V

$$dS = \left(\frac{\partial S}{\partial T}\right)_V dT + \left(\frac{\partial S}{\partial V}\right)_T dV$$
$$= \left(\frac{C_v}{T}\right) dT + \left(\frac{\partial S}{\partial V}\right)_T dV$$

Express $V = V(T, P)$ @ consider constant pressure

$$\left(\frac{dV}{P}\right) = \left(\frac{\partial V}{\partial T}\right)_P dT + \left(\frac{\partial V}{\partial P}\right)_T dP = \left(\frac{\partial V}{\partial T}\right)_P (dT)_P$$

$$\oint \left(\frac{dS}{P}\right) = \left(\frac{C_v}{T}\right) (dT)_P + \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_P (dT)_P$$

13

$$\left(\frac{\partial S}{\partial T}\right)_p = \frac{C_v}{T} + \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

For C_p , we identity for enthalpy - $dH = TdS + VdP$

At constant pressure $\Rightarrow (dH)_p = (TdS)_p$

$$C_p = \left(\frac{\partial H}{\partial T}\right)_p \stackrel{\text{so}}{=} \left(\frac{\partial H}{\partial T}\right)_p = T \left(\frac{\partial S}{\partial T}\right)_p$$

13

$$T \left(\frac{\partial S}{\partial T}\right)_p = C_v + T \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

13

$$C_p = C_v + T \left(\frac{\partial S}{\partial V}\right)_T \left(\frac{\partial V}{\partial T}\right)_p$$

Use Maxwell's relation $\left(\frac{\partial S}{\partial V}\right)_T = \left(\frac{\partial P}{\partial T}\right)_V$

13

$$C_p = C_v + T \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_p$$

• Let $\beta \equiv \left(\frac{1}{V}\right) \left(\frac{\partial V}{\partial T}\right)_p \rightarrow$ "thermal volume coefficient of expansion"

• Let $\kappa_T \equiv \left(-\frac{1}{V}\right) \left(\frac{\partial V}{\partial P}\right)_T \rightarrow$ "isothermal compressibility"

To write $C_p - C_v$ in terms of β & κ_T , more partial derivatives manipulation is required.

$$z = z(x, y), \text{ then } \left(\frac{\partial x}{\partial y}\right)_z = \frac{-(\partial z / \partial y)_x}{(\partial z / \partial x)_y}$$

Proof $dz = \left(\frac{\partial z}{\partial y}\right) dy + \left(\frac{\partial z}{\partial x}\right) dx$

when z constant $\rightarrow dz = 0$

So $\left(\frac{\partial z}{\partial x}\right) dx = -\left(\frac{\partial z}{\partial y}\right) dy$ ($dz = 0$)

So $\left(\frac{dx}{dy}\right)_z = \frac{-\left(\frac{\partial z}{\partial y}\right)_z}{\left(\frac{\partial z}{\partial x}\right)_z}$

So $\left(\frac{dx}{dy}\right)_z = \frac{-\left(\frac{\partial z}{\partial y}\right)_x}{\left(\frac{\partial z}{\partial x}\right)_y}$

So back to derivs...

$\left(\frac{\partial P}{\partial T}\right)_V = \frac{-\left(\frac{\partial V}{\partial T}\right)_P}{\left(\frac{\partial V}{\partial P}\right)_T}$

\downarrow $(C_p - C_v) = T \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial V}{\partial T}\right)_P = -T \left(\frac{\partial V}{\partial T}\right)_P \left(\frac{\partial P}{\partial T}\right)_V \left(\frac{\partial V}{\partial P}\right)_T^{-1}$
 $= -T (VP)^2 \frac{-1}{K_T V}$

So $C_p - C_v = \frac{TP^2V}{K_T} \rightarrow$ true for any substance

Ex For ideal gas $\rightarrow C_p - C_v = nR = NR$

$\beta = \frac{1}{V} \left(\frac{\partial V}{\partial T}\right)_P$, $K_T = -\frac{1}{V} \left(\frac{\partial V}{\partial P}\right)_T$
 $= \frac{1}{V} \left(\frac{NR}{P}\right)$, $= -\frac{1}{V} \left(\frac{-NR}{P^2}\right) = \frac{NR}{PV} = \frac{1}{P}$

So $C_p - C_v = \frac{T(T)^{-2}V}{P^{-1}} = \frac{PV}{T} = NR = nR$ ✓

April 2, 2019

Extensive vs. Intensive parameters

	1	2
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Let us have a homogeneous system

- ① if $y_1 + y_2 = y$ then y is an extensive parameter.
- ② if $y_1 = y_2 = y$ then y is an intensive parameter.

- Extensive { volume, mass, # particles, internal energy, Entropy
(V) (m) (N) (U) (S)
(Enthalpy (H)), (F), (G)
- Intensive { Temp, Pressure, density, chemical potential
(T) (P) (ρ) (μ)

Rules of multiplication & addition:

- ① (Ext) * (Int) = (Ext) $\frac{EX}{V \times \rho} = m$
- ② $\frac{[Ext]}{[Ext]} = [Int]$ $\frac{EX}{\frac{m}{V}} = \rho$
or $\frac{C_p}{mass} = C_v$

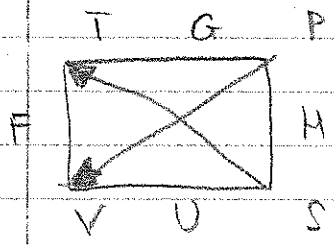
③ (Ext, Ext) \Rightarrow neither (extensive) nor (intensive)

④ $[Ext] + [Ext] = [Ext]$

⑤ Not allowed ~~$[Ext] + [Int]$~~

EX G has units of J But $G + \mu$ does not make sense
 μ has units of J

Gibbs free energy & chemical potential



$$dG = VdP - SdT + \mu dN$$

$$\left(\frac{\partial G}{\partial P}\right)_{T,N} = V, \quad \left(\frac{\partial G}{\partial T}\right)_{P,N} = -S, \quad \left(\frac{\partial G}{\partial N}\right)_{P,T} = \mu$$

Now, $\mu = \left(\frac{\partial G}{\partial N}\right)_{P,T}$ ext intensive

↑ ↑ ↑

int ext ext

↳ @ constant P,T → $G = \mu N$ ∝ N¹, G¹ proportionally

for a system with only 1 type of particles. $\mu = G/N$

Helmholtz free energy & chemical potential

$$dF = ~~dE~~ - SdT - PdV + \mu dN$$

$\mu = \left(\frac{\partial F}{\partial N}\right)_{T,V}$ → $F = N\mu(V)$

↑ ↑ ↑

int ext ext

Derivation of chemical potential of ideal gas

Before, $\mu = -T \left(\frac{\partial S}{\partial N}\right)_{U,V}$

Now, $G = \mu N$ or $\mu = \frac{G}{N}$

Consider a fixed amount of gas (N) at const (T) and allow P to vary.

$$\left(\frac{\partial \mu}{\partial P}\right)_{T,N} = \frac{\partial}{\partial P} \left(\frac{\partial G}{\partial N}\right)_{T,N} = \frac{1}{N} \left(\frac{\partial G}{\partial P}\right)_{T,N} = \frac{V}{N}$$

$$\int_{P_i}^{P_f} d\mu = \int_{P_i}^{P_f} \left(\frac{V}{N}\right) dP \Rightarrow \Delta \mu = \int_{P_i}^{P_f} \frac{kT}{P} dP = kT \ln \left(\frac{P_f}{P_i}\right)$$

$$\mu(T, P_f) - \mu(T, P_i) = kT \ln \left(\frac{P_f}{P_i}\right)$$

write $\mu(T, P_i) = \mu^{\circ}(T) \uparrow$ 1 atm

$$\mu(T, P) = \mu^{\circ}(T) + kT \ln \left(\frac{P}{P_0}\right)$$

↑ typically, 1 atm

• P is the partial pressure

Ex He, H $\mu_{He}(T, P) = \mu_{He}^{\circ}(T) + kT \ln \left(\frac{P_{He}}{P_0}\right)$

Test vs μ derived for a monatomic ideal gas

$$\begin{aligned} \mu &= -T \left(\frac{\partial S}{\partial N}\right)_{U,V} \\ \mu &= -kT \ln \left[\frac{V}{N} \left(\frac{2\pi m kT}{h^2}\right)^{3/2} \right] \\ &= -kT \ln \left[\frac{P^{\circ} kT}{P^{\circ} P} \left(\frac{2\pi m kT}{h^2}\right)^{3/2} \right] \\ &= -kT \ln \left[\frac{kT}{P^{\circ}} \left(\frac{2\pi m kT}{h^2}\right)^{3/2} \right] + kT \ln \left(\frac{P}{P^{\circ}}\right) \end{aligned}$$

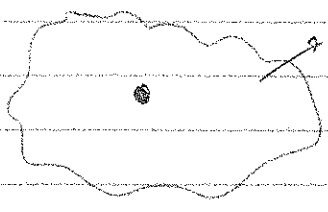
$$\mu = -kT \ln \left[\frac{kT}{P^{\circ}} \left(\frac{2\pi m kT}{h^2}\right)^{3/2} \right] + kT \ln \left(\frac{P}{P^{\circ}}\right)$$

$\mu^{\circ}(T)$

Free Energy as a Force Towards Equilibrium

- For isolated system $\rightarrow S \uparrow$
- For interacting system $\rightarrow S_{tot} \uparrow$

Assume environment is a reservoir of constant T, V, N



reservoir

$$S_{tot} = S_{system} + S_{reservoir}$$

$$dS_{tot} = dS_{sys} + dS_{res}$$

For reservoir, $TdS = dU + PdV - \mu dN$

$$dS = \frac{1}{T} dU + \frac{P}{T} dV - \frac{\mu}{T} dN$$

if T, N, V constant, then $dS_{res} = \frac{1}{T_{res}} dU_{res}$

$$dS_{tot} = dS_{sys} + \frac{1}{T_{res}} dU_{res}$$

In eq, $T_{sys} = T_{res}$, $dU_{sys} = -dU_{res}$

$$dS_{tot} = dS_{sys} - \frac{1}{T_{sys}} dU_{sys}$$

$dS_{tot} = -\frac{1}{T} (dU - TdS)$ \rightarrow dropping sys. subscript

dF

$$dS_{tot} = -\frac{dF}{T}$$

if $dF < 0 \rightarrow$ spontaneous flow towards equilibrium

Now, let V vary, holding $P, T, (\& N)$ constant

$$dS_{tot} = dS_{sys} + \frac{1}{T_{res}} dU_{res} + \frac{P_{res}}{T_{res}} dV_{res} - \frac{\mu_{res}}{T_{res}} dN_{res}$$

At equilibrium, $P_{res} = P_{sys}$, $T_{res} = T_{sys}$, $dU_{res} = -dU_{sys}$
 $dV_{res} = -dV_{sys}$

↳

$$dS_{tot} = dS - \frac{1}{T}dU - \frac{P}{T}dV$$

$$\text{↳ } dS_{tot} = \frac{-1}{T} \underbrace{(dU - TdS + PdV)}_{dG}$$

↳

$$\boxed{dS_{tot} = \frac{-dG}{T}}$$

$dG = dG_{sys}$, $T = \text{equilibrium } T$

↳

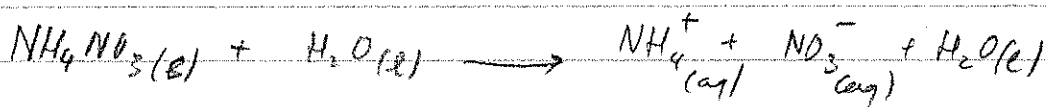
For fixed $P, T, N \Rightarrow \boxed{G \text{ tends to decrease}}$

if $\Delta G < 0 \rightarrow \text{spontaneous process}$

Example

use of free energy to calculate whether a reaction is spontaneous or not

Crystallized ammonium nitrate NH_4NO_3



look up $\Delta_f H$, $\Delta_f S$

	$\Delta_f H$	$\Delta_f S$	@ eq, $\Delta G = 0$
$NH_4NO_3(s)$	-365.56	151.08	
$NH_4^+(aq)$	-132.51	113.4	
$NO_3^-(aq)$	-205.0	146.4	

$$\Delta G = \Delta R - T\Delta S = -4.4 \text{ kJ} < 0 \rightarrow \text{spontaneous}$$

@ constant T

In general, $H = U + PV$ for constant P process, $\Delta H = \Delta U + P\Delta V$

$$\Delta H = \Delta U + P\Delta V = Q_{\text{calc}}$$

$\Delta H < 0 \Rightarrow$ exothermic rxn
$\Delta H > 0 \Rightarrow$ endothermic rxn

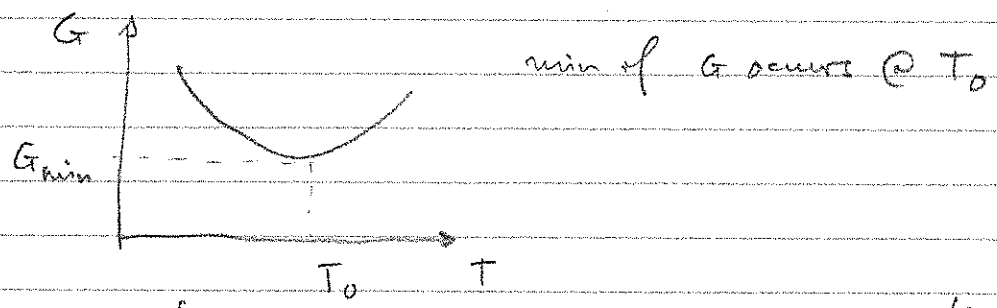
if $\Delta H < 0, \Delta S > 0 \Rightarrow \Delta G < 0$ spontaneous
 $\Delta H > 0, \Delta S < 0 \Rightarrow \Delta G > 0$ not spontaneous process.

Summary	Reservoir	System
	• At constant U, V	$S \uparrow$
	• At const T, V	$F \downarrow$
	• At const T, P	$G \downarrow$

Stability against temperature fluctuations

Consider a system. Let T, V be independent parameters that describe system

1st, hold V fixed & allow T to vary
 Interacting with respect to constant T, P, N



• Expand G around eq. value $\Delta G = G - G_{\text{min}} = \left(\frac{\partial G}{\partial T}\right)_V \Delta T + \frac{1}{2} \left(\frac{\partial^2 G}{\partial T^2}\right)_V (\Delta T)^2$

where $\Delta T = T - T_0$

• Evaluate derivs at $T = T_0$

$$\left(\frac{\partial G}{\partial T}\right)_V \Big|_{T_0} = 0, \quad \left(\frac{\partial^2 G}{\partial T^2}\right)_V \Big|_{T_0} > 0$$

$$G = U - TS + PV \quad G_0 @ T_0, P_0$$

$$G_0 = U_0 - T_0 S + P_0 V$$

$$\left(\frac{\partial G_0}{\partial T}\right)_V = \left(\frac{\partial U}{\partial T}\right)_V - T_0 \left(\frac{\partial S}{\partial T}\right)_V = 0 @ T = T_0$$

$$dU = T ds - P dV \quad \left(\frac{dU}{dT}\right)_V = T \left(\frac{\partial S}{\partial T}\right)_V$$

$$\left(\frac{\partial G}{\partial T}\right)_V = \left(\frac{\partial U}{\partial T}\right)_V - T_0 \left[\frac{1}{T} \left(\frac{\partial U}{\partial T}\right)_V \right]$$

$$\left(\frac{\partial G_0}{\partial T}\right)_V = \left(\frac{\partial U}{\partial T}\right)_V \left[1 - \frac{T_0}{T} \right]$$

• Evaluate $\left(\frac{\partial^2 G_0}{\partial T^2}\right)_V = \left(\frac{\partial}{\partial T}\right) \left(\frac{\partial G_0}{\partial T}\right) = \frac{T_0}{T^2} \left(\frac{\partial U}{\partial T}\right)_V + \left(1 - \frac{T_0}{T}\right) \left(\frac{\partial^2 U}{\partial T^2}\right)_V > 0$
at $T = T_0$

$$\frac{T_0}{T^2} \left(\frac{\partial U}{\partial T}\right)_V > 0$$

$$\left(\frac{\partial U}{\partial T}\right)_V > 0$$

$$C_V > 0$$

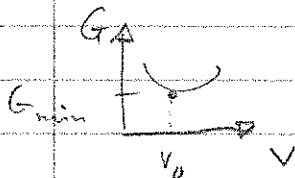
if heat cap > 0 , then stable around δT

Le Châtelier's Principle

April 3, 2019

When a system in eq. is disturbed, it will respond in a (stable) way to restore itself back to equilibrium.

Result for V Disturbances



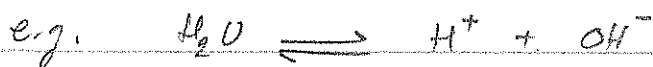
$$\left. \left(\frac{\partial^2 G}{\partial V^2} \right) \right|_{T=T_0} = - \left(\frac{\partial P}{\partial V} \right)_T > 0$$

$$K_T = - \frac{1}{V} \left(\frac{\partial V}{\partial T} \right)_T$$

$$\frac{1}{K_T} > 0 \quad \text{or simply} \quad \boxed{K_T > 0}$$

Chemical Equilibrium

Can we Gibbs to determine equilibrium conditions...

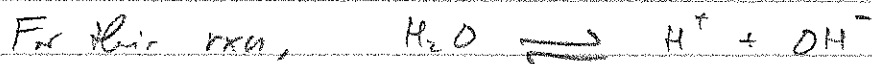


Mixture of H_2O ions is most stable state (lower G)

$$G = U - TS$$

@ Eq... $\Delta G = 0$. Ions have a higher entropy. But additional entropy of mixing makes the mixture more stable.

$$\text{@ Eq, } dG = 0 = dH - TdS = \mu dN \dots = \sum_i \mu_i dN_i = \sum_i \mu_i dN_i$$



$$dN_{\text{H}_2\text{O}} = -1, \quad dN_{\text{H}^+} = +1, \quad dN_{\text{OH}^-} = +1 \quad \text{@ Eq, } dG = 0 = \sum_i \mu_i dN_i$$

$\sum -\mu_{H_2O} + \mu_{OH^-} + \mu_{H^+} = 0$

$\sum \mu_{OH^-} + \mu_{H^+} = \mu_{H_2O}$

More generally, $\nu_1 X_1 + \nu_2 X_2 + \dots \rightleftharpoons \nu_3 X_3 + \nu_4 X_4 + \dots$

$\nu_i \rightarrow$ stoichiometric coefficient of species i

In eq, $\nu_1 \mu_1 + \nu_2 \mu_2 + \dots = \nu_3 \mu_3 + \nu_4 \mu_4 + \dots$

The rxn $H_2O \rightleftharpoons H^+ + OH^-$ produces a solution, which is a mixture of a solvent (primary component) + solute (secondary comp)

Dilute solution { # of solute molecules \ll # of solvent molecules
and solute molecules don't interact with each other
 \rightarrow can treat them as an ideal gas!

Need to calculate μ for solvent & solute in order to predict eq.

Suppose we have pure water... 100% H_2O ... solvent, A \rightarrow "pure"

$G = N_A \mu_A = N_A \mu_A^\circ(T, P)$ μ_A° : chem. pot. of pure solvent

Add a single B molecule (solute), holding T, P fixed

$dG = dU + PdV - TdS$
 \downarrow
indep of N_A
only dep on N_B \rightarrow dep on N_A ($R \sim N_A$)

$dS = k_B \ln N_A$ - additional terms indep of N_A ...
 $dG = -kT \ln N_A + f(T, P)$ for adding 1 molecule
indep of N_A

Adding 2 B molecules...

Gross $\rightarrow dG' = 2dG = 2 \left[f(T,P) - kT \ln N_A \right] \otimes$

But B molecules indistinguishable.

\hookrightarrow I need to be divided by 2! \rightarrow indistinguishable

So...

$$dG' = 2f(T,P) - T \left[2k \ln N_A - k \ln 2 \right]$$
$$= 2f(T,P) - 2kT \ln N_A + kT \ln 2$$

Generalizing... (for N_B molecules...)

$$kT N_A \ln N_B - kT N_B$$

$dG = N_B f(T,P) - N_B kT \ln N_A + kT \ln(N_B!)$

Pure Solvent

$$G = N_A \mu^0(T,P)$$

Dilute Solution $G + dG$

Solution

$G = N_A \mu^0(T,P) + N_B f(T,P) - N_B kT \ln N_A + N_B kT \ln N_B - N_B kT$

\uparrow valid if $N_B \ll N_A$ (dilute solution...)

Since, $\mu = \left(\frac{\partial G}{\partial N} \right)_{T,P}$ we can solve for μ_A & μ_B

$\mu_A = \left(\frac{\partial G}{\partial N_A} \right)_{T,P,N_B} = \mu^0(T,P) - N_B kT / N_A$

\rightarrow chem pot of solvent

$\mu_B = \left(\frac{\partial G}{\partial N_B} \right)_{T,P,N_A} = f(T,P) - kT \ln N_A - kT + kT + kT \ln N_B$
$$= f(T,P) + kT \ln \frac{N_B}{N_A}$$

\rightarrow chem pot of solute

April 5, 2019

Recall

① Started with G for pure solvent (A)

$$G = \mu^\circ(T, P) N_A$$

② Add solute particles (B) to this

$$dG = \underbrace{dU + PdV - TdS}_{f(T, P) \text{ independent of } N_A} \rightarrow \begin{matrix} \text{Some terms dep. on } N_A \\ \text{some indep of } N_A \end{matrix}$$

$$\Omega = \frac{N_A!}{N_B! (N_A - N_B)!}, \text{ and since } N_A \gg N_B \Rightarrow \Omega \approx \frac{N_A^{N_B}}{N_B!}$$

$$\begin{aligned} \underline{S} \quad S &= k_B \ln \Omega = k_B \ln \left[\frac{N_A^{N_B}}{N_B!} \right] = k_B \ln(N_A^{N_B}) - k_B \ln(N_B!) \\ &\approx N_B k_B \ln(N_A) - N_B k_B \ln N_B + N_B k_B \end{aligned}$$

Now, $G = G_A + dG$

$$\hookrightarrow dG = N_B f(T, P) - N_B k_B T \ln N_A + k_B T \ln N_B - N_B k_B$$

$$\underline{G} \quad \boxed{G = \mu^\circ(T, P) N_A + N_B f(T, P) + N_B k_B T \ln \left(\frac{N_B}{N_A} \right) - N_B k_B T}$$

Now,

$$\mu = \left(\frac{\partial G}{\partial N} \right)_{T, P} \Rightarrow \left. \begin{aligned} \mu_A &= \left(\frac{\partial G}{\partial N_A} \right)_{T, P} = \mu^\circ(T, P) - \frac{N_B k_B T}{N_A} \\ &\quad \text{(solvent)} \\ \mu_B &= \left(\frac{\partial G}{\partial N_B} \right)_{T, P} = f(T, P) + k_B T \ln \frac{N_B}{N_A} \\ &\quad \text{(solute)} \end{aligned} \right\}$$

Definition

"Molality" \rightarrow # moles of solute per kg of solvent.

$$\boxed{m = \frac{\text{moles solute}}{\text{kg solvent}} \propto \frac{N_B}{N_A}}$$

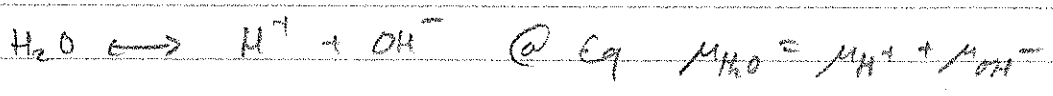
Re-writing μ_B in terms of m : \rightarrow absorbed ... extra term ...

* $\mu_B = f(T, P) + kT \ln(m_B)$ (1)

* $\mu_B^0(T, P) \xrightarrow{\Delta}$ standard condition for molality = 1 = m_B

So when $m_B = 1 \rightarrow \mu_B = \mu_B^0(T, P) + kT \ln(m_B)$

Example Dissociation of water



Treat as dilute solution: solvent H_2O

$$\mu_{H_2O} = \mu_{H_2O}^0(T, P) - \frac{N_{H^+} kT}{N_{H_2O}} - \frac{N_{OH^-} kT}{N_{H_2O}}$$

$$\mu_{H^+} = \mu_{H^+}^0(T, P) + kT \ln m_{H^+}$$

$$\mu_{OH^-} = \mu_{OH^-}^0(T, P) + kT \ln m_{OH^-}$$

at room temp, $kT \sim 4 \times 10^{-21} J$

$\mu_{H_2O} = \mu_{H^+} + \mu_{OH^-} \Rightarrow \mu_{H_2O} - \mu_{H^+} - \mu_{OH^-} = 0$

$\Rightarrow \mu_{H_2O}^0 - \mu_{H^+}^0 - \mu_{OH^-}^0 = kT \ln(m_{H^+}) + kT \ln(m_{OH^-})$
 $= kT \ln(m_{H^+} \cdot m_{OH^-})$

$-\Delta G^0 = RT \ln(m_{H^+} \cdot m_{OH^-})$

$-\Delta G^0 = RT \ln(m_{H^+} \cdot m_{OH^-})$

Ex ΔG° dissociation of water = 79.9 kJ/mol

Now $\Rightarrow m_{H^+} \cdot m_{OH^-} = e^{-\Delta G^\circ/RT}$
 K equilibrium constant

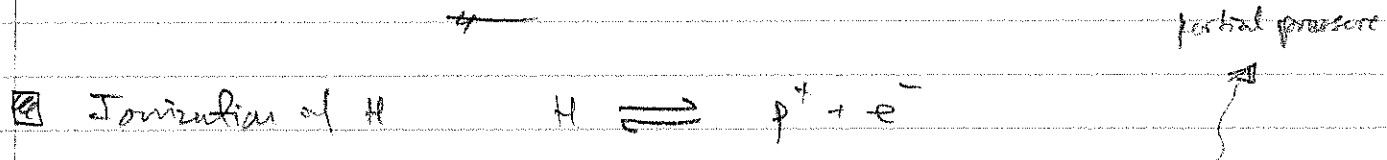
For some temp & standard P, $K_{H_2O} = 10^{-14}$

$\therefore m_{H^+} \cdot m_{OH^-} = 10^{-14} = (m_{OH^-})^2 = (m_{H^+})^2$

$\therefore m_{H^+} = m_{OH^-} = 10^{-7}$ → moles/kg H₂O

$pH \equiv -\log_{10}(m_{H^+}) \Rightarrow pH = 7$ for "pure" H₂O

if lower H⁺ conc. then Basic, pH ↑
if more H⁺ conc. then Acidic, pH ↓



treat as ideal gas: $\mu(T, P) = \mu^\circ(T) + kT \ln(P/p_0)$
↑ std. atm. pressure

$(\mu_{p^+}^\circ + \mu_{e^-}^\circ - \mu_H^\circ) = kT \ln\left(\frac{P_H}{p_0}\right) - kT \ln\left(\frac{p_{p^+}}{p_0}\right) - kT \ln\left(\frac{p_{e^-}}{p_0}\right)$

$\Rightarrow -\Delta G^\circ = N_A kT \ln \left[\frac{P_H p_0}{p_{p^+} p_{e^-}} \right]$ ↑ kT/p_0

\therefore recall, for ideal gas $\mu^\circ = -kT \ln \left[\frac{V}{N} \left(\frac{2\pi m kT}{h^2} \right)^{3/2} \right]$

Part, μ for H should be less than -13.6eV when at rest ($\mu E = 0$)

$$\mu_{H^0} = -kT \ln \left[\frac{kT}{p^0} \left(\frac{2\pi m_p kT}{h^2} \right)^{3/2} \right] - 13.6\text{eV}$$

Part Part p^+, e^- combined \rightarrow

$$\mu_{p^+}^0 = -kT \ln \left[\frac{kT}{p^0} \left(\frac{2\pi m_p kT}{h^2} \right)^{3/2} \right]$$

$$\mu_{e^-}^0 = -kT \ln \left[\frac{kT}{p^0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \right]$$

Now, $m_H \approx m_e$

$$\mu_{p^+}^0 + \mu_{e^-}^0 - \mu_{H^0}^0 = -kT \ln \left(\frac{kT}{p^0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \right) + 13.6\text{eV}$$

Therefore,

$$-\ln \left(\frac{p_H p^0}{p_{p^+} p_{e^-}} \right) = \ln \left(\frac{kT}{p^0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \right) - \frac{13.6\text{eV}}{kT}$$

$$\left(\frac{p_H p^0}{p_{p^+} p_{e^-}} \right)^{-1} = \frac{kT}{p^0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \cdot e^{-13.6\text{eV}/kT}$$

$$\frac{p_{p^+} p_{e^-}}{p_H} = \frac{kT}{p^0} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \cdot e^{-13.6\text{eV}/kT}$$

$$\frac{p_{p^+}}{p_H} = \frac{kT}{p_{e^-}} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} \cdot e^{-13.6\text{eV}/kT} \quad \text{Saha Eqn}$$

$\rightarrow N_{p^+}/N_H$

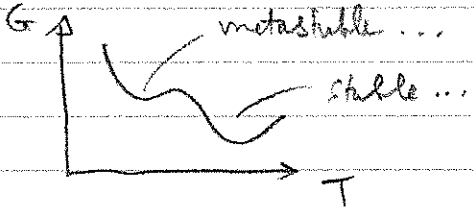
PHASE TRANSFORMATION

def { A continuous change in property of matter as its environment changes infinitesimally. }

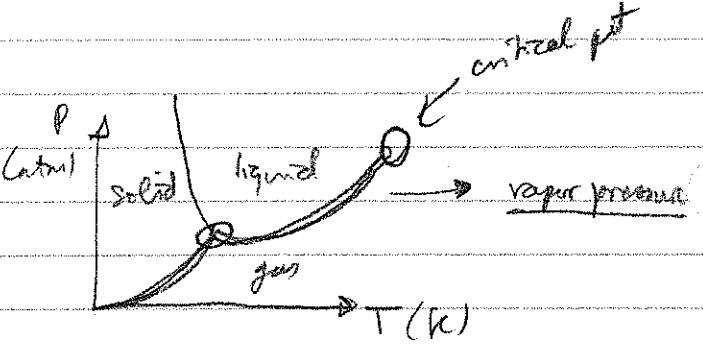
Phases { different states of matter - or unique structural arrangement of atoms within matter. }

Can depend on many variables : eg: P, T, B, ...

↳ Gibbs free energy is key to understanding these...

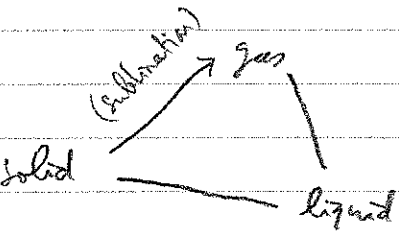
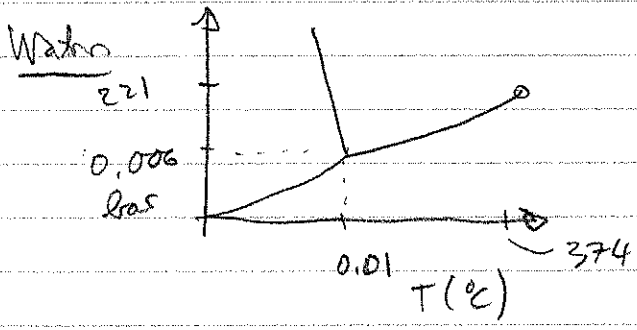


Phase diagram for water



Vapor pressure → pressure at which liquid or solid phase can coexist with gas

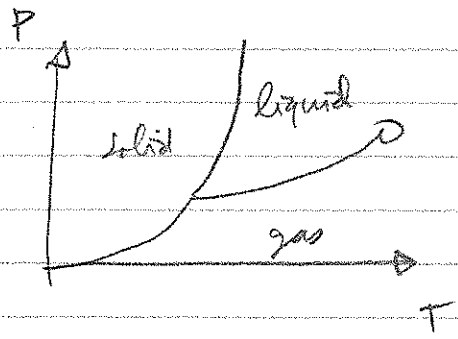
Triple point → precise T, P at which all 3 phases (liquid, gas, solid) can coexist...



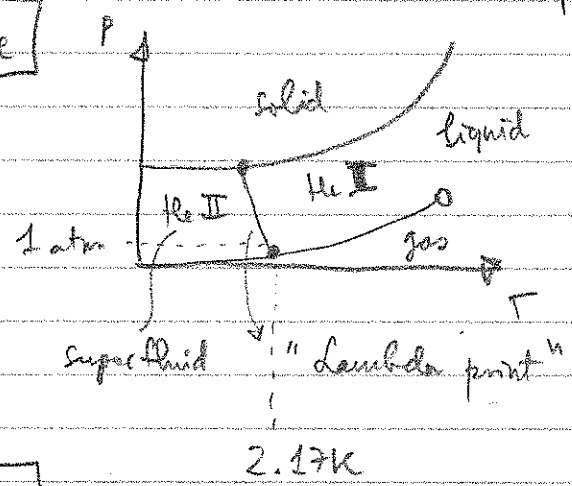
Critical point As P or T increases, we reach a point where liquid & gaseous phases are indistinguishable.

Ex Plasma...

CO₂



⁴He

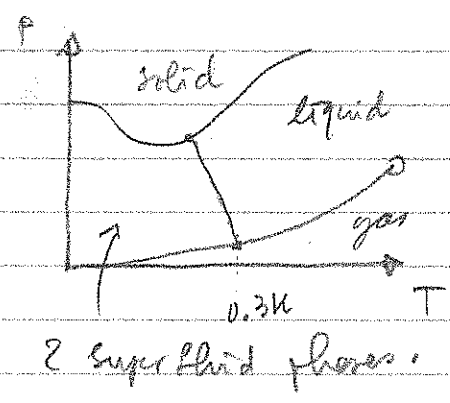


"He is a superfluid below the Lambda point (@ 1 atm, 2.17K)"

Superfluid

- zero viscosity
- zero entropy
- high conductivity

³He

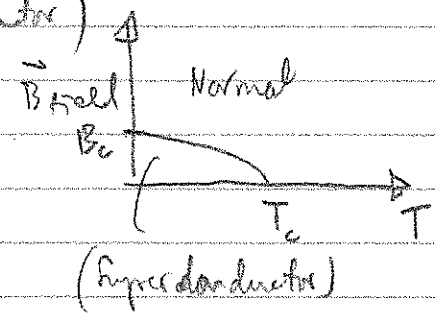


Other variables that can cause phase change:

- Chemical composition:
- external \vec{B} field strength → (Type I superconductor) (0 resistivity)

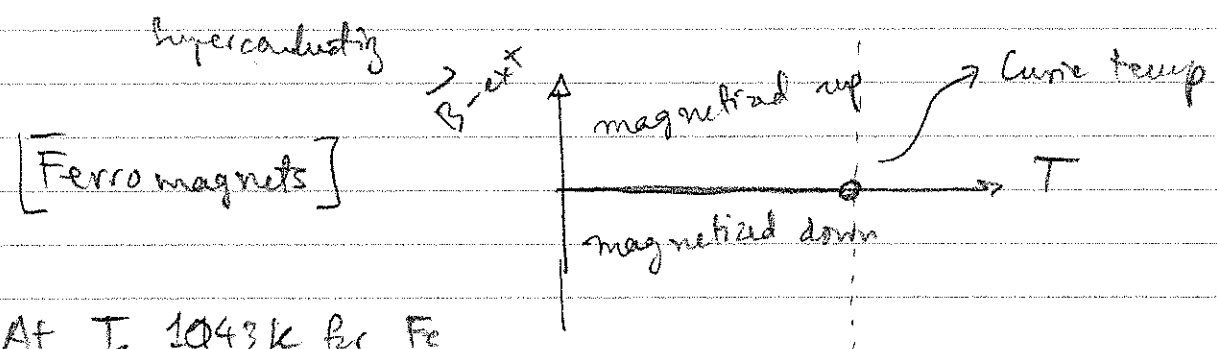
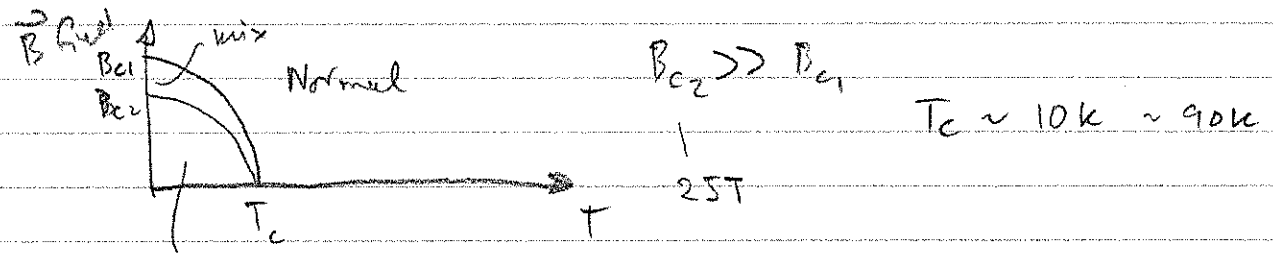
(Type I superconductor)

Typical $B_c \sim 0.01 - 0.1 T$
 $T_c \sim 10 K$



(superconductor)

Aside Type II - Superconductor



At T_c 1043K for Fe
 → magnetization disappears
 → behaves like paramagnet

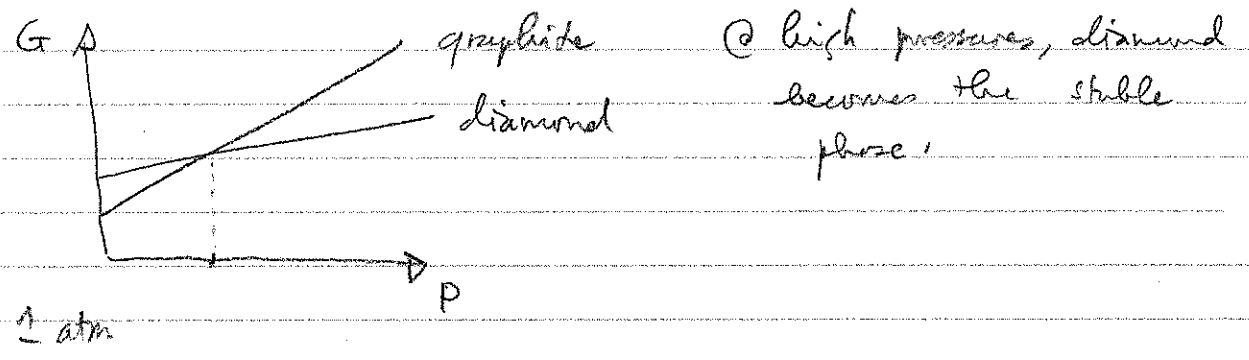
Using Gibbs free energy to evaluate stable phase for substances

$$dG = -SdT + VdP + \mu dN$$

$$\left(\frac{\partial G}{\partial T} \right)_{P,N} = -S \quad ; \quad \left(\frac{\partial G}{\partial P} \right)_{T,N} = V$$

Ex Diamond vs Graphite, look up $\Delta_f G$ for both room T & 1 atm

$\Delta_f G_{\text{graphite}}$ is 2900J less than $\Delta_f G_{\text{diamond}}$ @ 298K, 1 atm

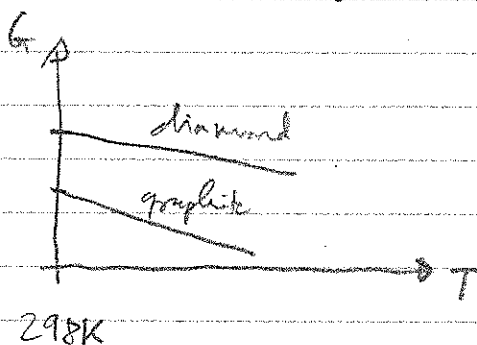


Now look at T dependence

$$\left(\frac{\partial G}{\partial T}\right) = -S \text{ as } T \uparrow, G \downarrow$$

Entropy of diamond vs graphite.

↑ lower S ↑ higher S



Graphite is always more stable.

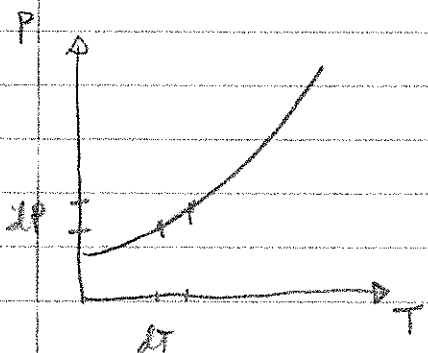
Clausius - Clapeyron relation

Since $\left(\frac{\partial G}{\partial T}\right)_{P,N} = -S$, $\left(\frac{\partial G}{\partial P}\right)_{T,N} = +V$ then slope of the phase boundary line on P vs T diagram is related to S & V of the two phases...

Phase boundary between liquid & gas

→ assume 1 mole of Helium

On the boundary $G_l = G_g$



increase P & T w/ 2 phases remain in eq.

$$dG = -SdT + VdP + \mu dN$$

$$\int_{S_0} SdT = \int_{V_0} VdP \dots$$

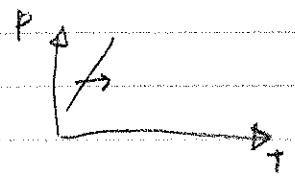
$$dG_l = -S_l dT + V_l dP$$

$$dG_g = -S_g dT + V_g dP \quad \updownarrow \text{ equal}$$

$$\oint (V_g - V_l) dP = (S_g - S_l) dT$$

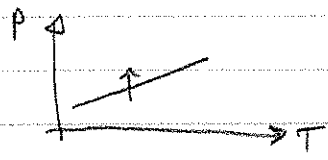
$$\frac{dP}{dT} = \frac{S_g - S_l}{V_g - V_l}$$

• if we have a large entropy difference between phases
→ steep slope...



dP/dT steep: Small T changes will change the phase...

• if large volume difference



dP/dT → shallow. Small P change will change phase.

Reminder $\Delta G = \frac{Q}{T} = \frac{L}{T}$

$$\frac{dP}{dT} = \frac{L}{T \Delta V}$$
 L: total latent heat of vaporization
 $\Delta V = V_g - V_l$

↖ Clausius - Clapeyron Eqn.

L: l.m → extensive } ratio $\frac{L}{\Delta V}$ = intensive.
 $\Delta V =$ extensive

Example Use Clausius - Clapeyron to explain why H₂O has negative $\frac{dP}{dT}$ between solid - liquid phases.

$$\frac{dP}{dT} = \frac{L}{T \Delta V} = \frac{\Delta S}{\Delta V}$$

$\rho_{ice} = 917 \text{ kg/m}^3$, $\rho_{liq} = 1000 \text{ kg/m}^3$ → use 1 vol of H₂O

$$V_l = m/\rho = \frac{1000\text{kg}}{1000\text{kg/m}^3} = 1\text{m}^3 \quad V_{ice} = \frac{1000\text{kg}}{917\text{kg/m}^3} = 1.09\text{m}^3$$

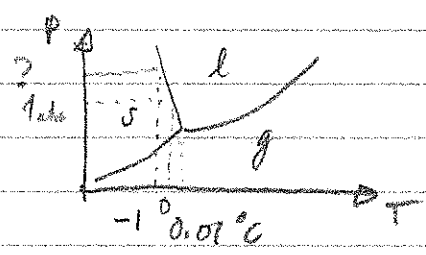
$$(V_l - V_g) = -0.09\text{m}^3$$

As we go from ice to water, $V \downarrow$, ΔT

So $\frac{dP}{dT}$ is negative

Assume L is constant with T , T : $\frac{dP}{dT} = \frac{3335\text{J/g} \times 10^6\text{g}}{(273\text{K})(-0.09\text{m}^3)} = -1.35 \times 10^9 \text{ Pa/K}$

How much pressure is required to melt ice at -1°C ?

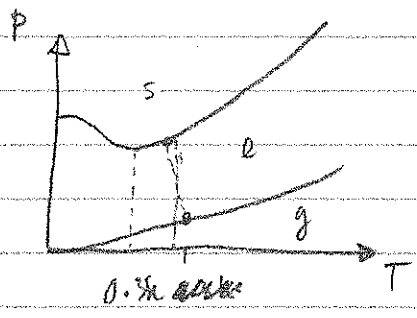


$$\frac{dP}{dT} = -1.35 \times 10^9 \text{ Pa/K}$$

$$dP = (-1.35 \times 10^9 \text{ Pa/K})(-1\text{K})$$

$$dP = 1.35 \times 10^9 \text{ Pa} \approx 135 \text{ atm} = 135 \text{ bar}$$

Ex ^3He



At $T < 0.3\text{K}$, slope between solid & liquid is negative

which phase is more dense? Remember that $(\frac{\partial G}{\partial T})_{P,N} = V$

solid ^3He is stable phase at high P , so it must have smaller V . Whatever $dG/dP \rightarrow$ solid is more dense.

Which phase has more entropy?

$$\frac{dP}{dT} = \frac{\Delta S}{\Delta V} < 0 \quad @ \quad T < 0.3K$$

if $V \downarrow$ as we go $l \rightarrow s$, $S \uparrow$ as we go from $l \rightarrow s$

to solid H_2O has more entropy.

Q: what is the slope of the phase boundary at $T=0$?

3rd law: As $T \rightarrow 0K$, $S \rightarrow$ minimum value.

$\Delta S = 0$ between the phases @ $T=0$

$$\frac{dP}{dT} = \frac{\Delta S}{\Delta V} \Rightarrow \frac{dP}{dT} = 0 \Rightarrow \text{slope of phase boundary goes away.}$$

April 10, 2019

The van der Waals Model

Ideal gas: $PV = nRT = NkT \rightarrow$ want to correct for finite volumes of molecules & attractive forces between particles

$$\left(P + \frac{aN^2}{V^2} \right) (V - Nb) = NkT \quad \text{van der Waals equation.}$$

Two modifications: ① $V \rightarrow V - V_0 \rightarrow$ can't compress gas to $V=0$
"b" represents volume per particle
min volume = Nb @ $P = \infty$

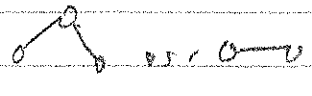
② $P \rightarrow P + \frac{aN^2}{V^2}$ accounts for short range attractive forces between molecules

$$P = \frac{NkT}{V - Nb} - \frac{aN^2}{V^2}$$

Imagine being at $T=0$, frozen thermal motion. \Rightarrow no KE, but still has potential energy

PE single particle $\propto N/V \Rightarrow PE_{\Sigma} \propto \frac{N}{V} \cdot N$

$\Rightarrow PE_{\Sigma} = -\frac{aN^2}{V}$, negative since it works against KE

"a" constant depending on type of molecules 

To calculate P, $dU = TdS - PdV \Rightarrow P = -\left(\frac{\partial U}{\partial V}\right)_{S,N}$ ($T=0$)

Contribution to P from PE

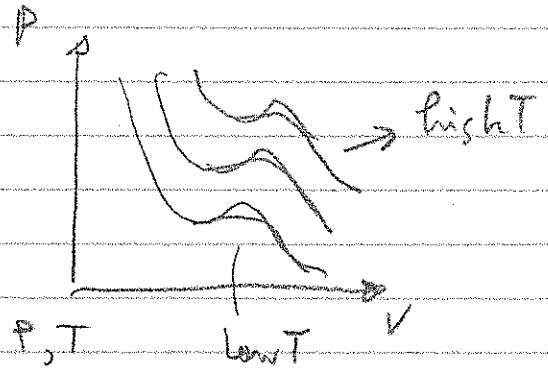
$P = -\frac{\partial}{\partial V} \left(-\frac{aN^2}{V} \right)_{S,N} \Rightarrow P = \frac{NkT}{V-Nb} - \frac{aN^2}{V^2}$

Ex Molecular Interaction $H_2O: b \approx 6 \times 10^{-24} m^3 \sim (4\text{\AA})^3$
 N_2 similar

"a" varies between molecules ... $N_2: a \sim 2.5 eV \text{\AA}^3$
 $H_2O \sim a_{N_2}$ due to dipole interaction
 $He: a_{He} < a_{N_2}$ (atomistic)

Consequences of vdW models

For a given T, plot P vs V.



\Rightarrow Multiple possible V 's for a given P, T

Use G to find which volume is stable

$dG = -SdT + VdP + \mu dN$, for $T, N \Rightarrow \left(\frac{\partial G}{\partial V}\right)_{T,N} = V\left(\frac{\partial P}{\partial V}\right)_{T,N}$

$P = \frac{NkT}{V-Nb} - \frac{aN^2}{V^2}$ so,

$$V \left(\frac{\partial P}{\partial V} \right)_{T,N} = V \frac{\partial}{\partial V} \left[\frac{NkT}{V-Nb} - \frac{aN^2}{V^2} \right]$$

$$= V \left[\frac{-NkT}{(V-Nb)^2} + \frac{2aN^2}{V^3} \right]$$

$$\rightarrow \left(\frac{\partial G}{\partial V} \right)_{T,N} = \frac{-NkTV}{(V-Nb)^2} + \frac{2aN^2}{V^2}$$

$$\int dG = \int \left[\frac{-NkT(V-Nb)}{(V-Nb)^2} + \frac{2aN^2}{V^2} \right] dV$$

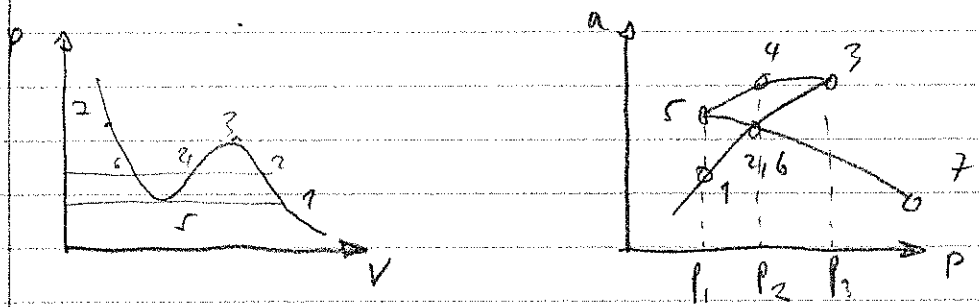
$$= \int \frac{-NkT(V-Nb)}{(V-Nb)^2} + \frac{2aN^2}{V^2} dV$$

$$= \int \frac{-NkT(V-Nb)}{(V-Nb)^2} - \frac{NkT}{(V-Nb)^2} + \frac{2aN^2}{V^2} dV$$

constant
of int

$$\rightarrow G = -NkT \ln(V-Nb) + \frac{NkT(Nb)}{(V-Nb)} - \frac{2aN^2}{V} + c(T)$$

Wants to know G vs. P



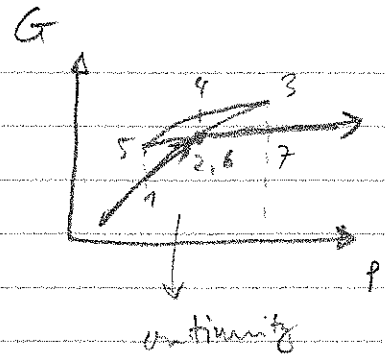
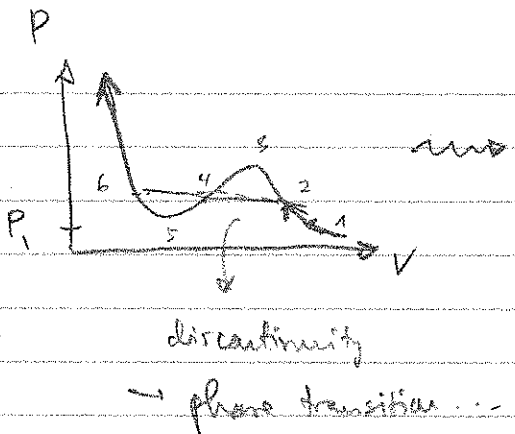
- 2 & 3 are unstable.
- substance will go directly from vol @ 2 → vol @ 6 as it's compressed
- Discontinuity = phase change

$$\Delta G \text{ around loop} = 0 \quad \int_{\text{loop}} dG = 0, \quad \left(\frac{\partial G}{\partial P} \right)_T = V \Rightarrow \left(\frac{\partial G}{\partial P} \right)_T dP = 0$$

$$\int_{\text{loop}} 0 = \int_{\text{loop}} V dP$$

April 12, 2019

Reull, vdW

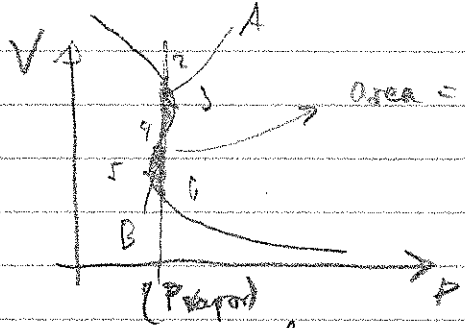


$\int_{loop\ 2-6} dG = 0 = \int_{loop\ 2-6} dG = 0$ where $dG = -SdT + PdV$

$\hookrightarrow \left(\frac{\partial G}{\partial P}\right)_{T,N} = V$

$\int_{loop\ 2-6} VdP_T = 0$

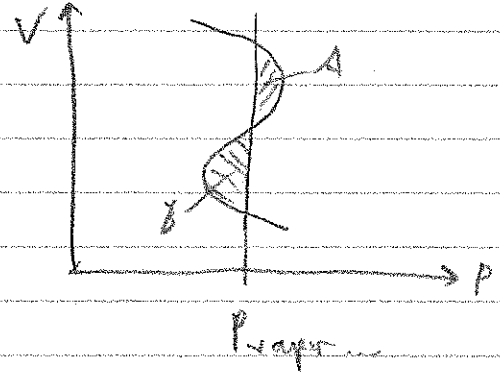
flip around ...



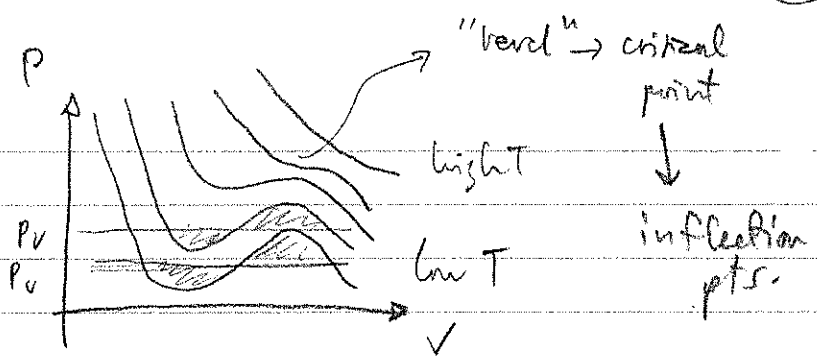
$\rightarrow \text{area (A)} = \text{area (B)}$ for $\int VdP_T = 0$

\hookrightarrow "Maxwell's construction"

\Rightarrow P of phase transformation occurs where vertical P divides the area in equal halves



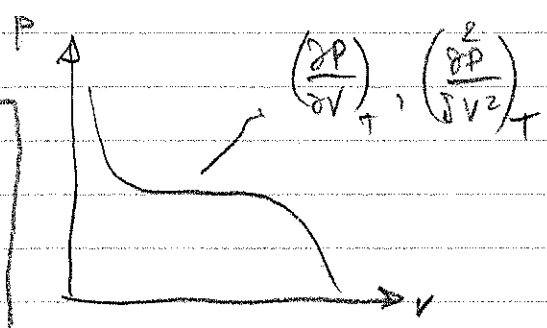
Isotherms @ different T



↳ by finding P_{max} based on Isotherms...

↳ P_{max} or critical point.

(Critical point) \rightarrow $\left\{ \begin{array}{l} \left(\frac{\partial P}{\partial V}\right)_T = 0 \\ \left(\frac{\partial^2 P}{\partial V^2}\right)_T = 0 \end{array} \right\}$

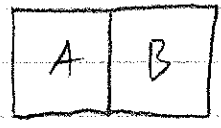


$\left. \begin{array}{l} T_c = \text{critical temp is where first \& 2^{nd} \text{ derivs of } P \text{ wrt } V \\ \text{are zero.} \end{array} \right\}$

PHASE TRANSFORMATION OF MIXTURES (§ 5.4)

Start with G $G = U - TS + PV$

Consider a mixture of 2 substances A & B



in thermal-mech. equilibrium
 $\rightarrow T_A = T_B = T \quad P_A = P_B = P$

Then $G_{tot} = G_A + G_B$. Let $x = \frac{\#B}{\Sigma} \rightarrow 1-x = \frac{\#A}{\Sigma}$

Can write $G_A^0 =$ Gibbs free energy of pure A ($x=0$)
 $G_B^0 =$ Gibbs free energy of pure B ($x=1$)

Remove partition & let A & B mix

$$G = U - TS + PV, \text{ Assume these changes are small } \left. \begin{array}{l} \text{in } U, V \end{array} \right\}$$

$$\Delta G = \Delta U - T\Delta S + P\Delta V$$

Initially, $G_{tot}^0 = (1-x)G_A^0 + xG_B^0$

Recall, $\Delta S_{mixing} = -Nk [x \ln x + (1-x) \ln(1-x)]$

Assuming $\Delta U = 0, \Delta V = 0$, then,

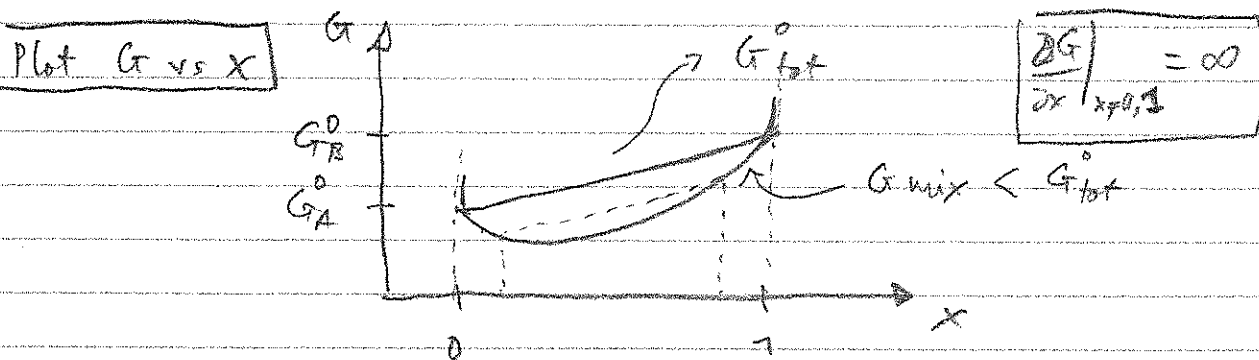
$$G_{mixed} = G_{tot}^0 - T\Delta S$$

$$= G_{tot}^0 + NkT [x \ln x + (1-x) \ln(1-x)]$$

$$G_{mixed} = (1-x)G_A^0 + xG_B^0 + nRT [x \ln x + (1-x) \ln(1-x)]$$

< 0

We call this an ideal mixture \Rightarrow derived from ideal gas...



slope of G vs. x @ 0, 1 is ∞

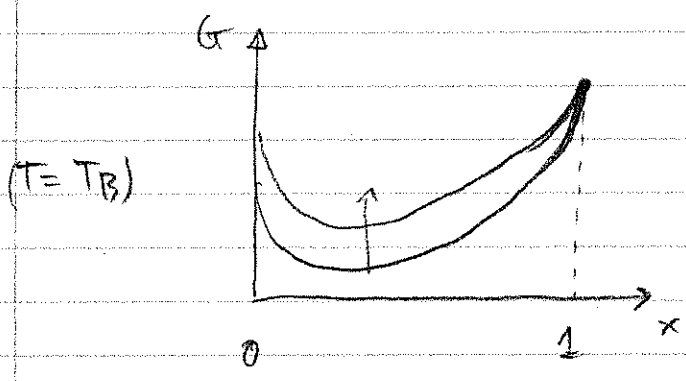
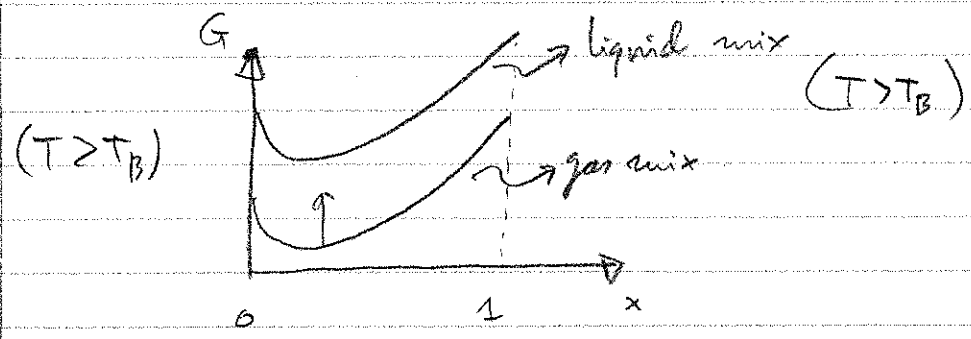
impure (mixed) is always more stable b/c of entropy of mixing...

Phase changes of mixtures

e.g. $N_2 + O_2$

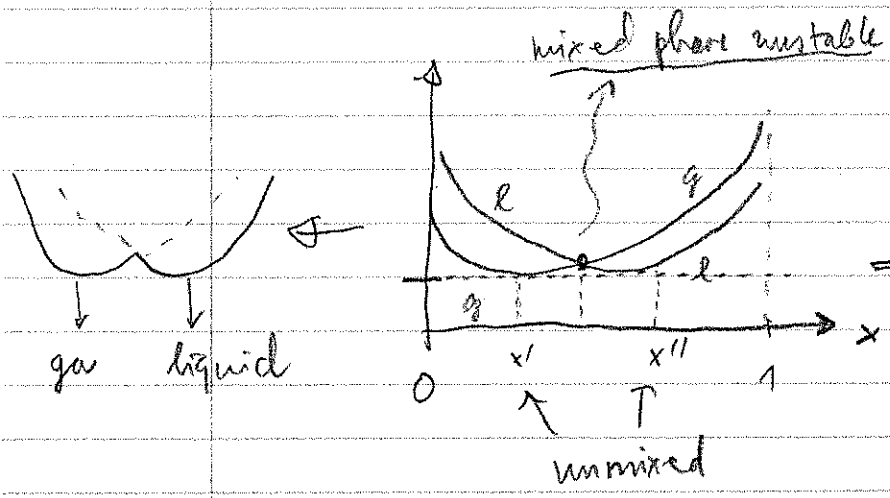
let T_A = boiling point of pure substance A
 T_B = boiling point of pure substance B

let $T_D > T_A$. then at high temp. $T > T_D > T_A$
 \rightarrow stable phase is a gas regardless of composition...



As we decrease T, G changes.
 $\leftarrow \left\{ \begin{array}{l} \text{known } \left(\frac{\partial G}{\partial T} \right) = -S \end{array} \right.$

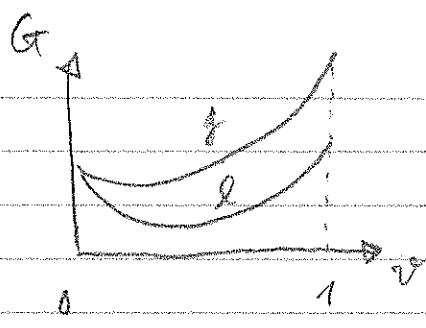
gas = liquid of pure B are in equilibrium.



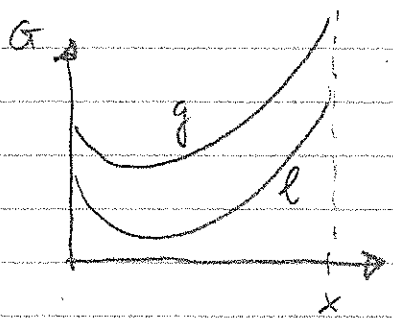
$T_A < T < T_B$

\Rightarrow Unmixed combination of liquid & gas is more stable than mixed

Decrease T further...

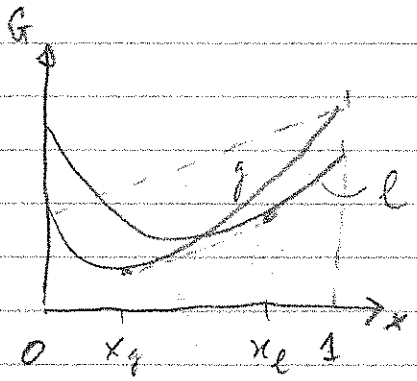


~~(unstable)~~
 $T \approx T_A \Rightarrow$ liquid stable for pure A

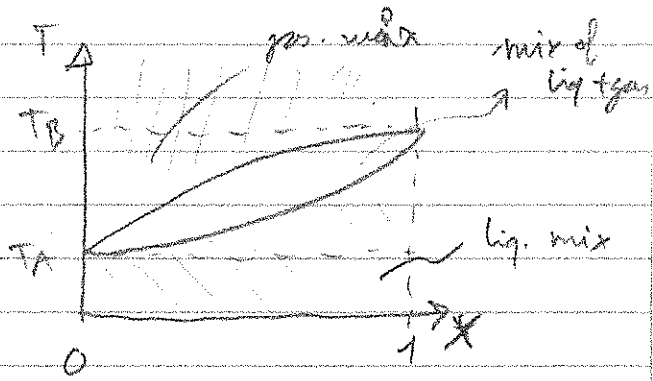


$T < T_A \Rightarrow$ liquid mixed is stable

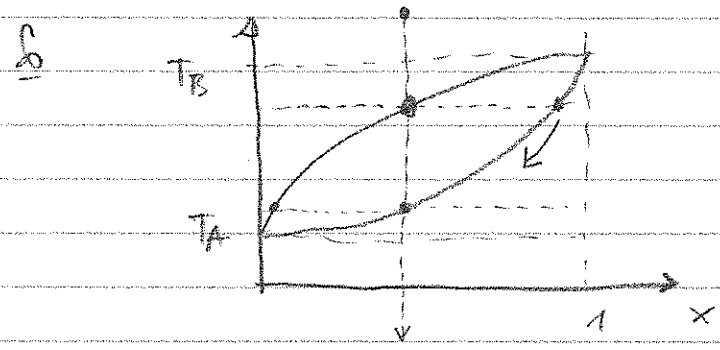
part 13, 2579



\Rightarrow



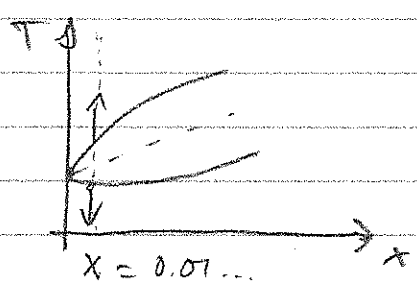
gas mix



as we go down in temp

For dilute solutions

x is small. From side don't evaporate \rightarrow gas is pure solvent



\Rightarrow only need equilibrium condition for solvent.

A = solvent, B = solute

$\mu_{A, liq}(T, P) = \mu_{A, gas}(T, P) \rightarrow A \text{ in equili.}$

Solvent, $\mu_{A, liq}(T, P) = \mu_0(T, P) - \frac{N_B kT}{N_A}$

Also,

$\mu_0(T, P) - \frac{N_B kT}{N_A} = \mu_{A, gas}(T, P)$

Let T_0 be boiling point of pure solvent (A). Hold pressure steady, vary temperature around T_0 to see how μ changes...

$\mu_0(T_0, P) + (T - T_0) \left(\frac{\partial \mu_0}{\partial T} \right) = \frac{N_B kT}{N_A} = \mu_{gas}(T_0, P) + (T - T_0) \left(\frac{\partial \mu_{gas}}{\partial T} \right)$

at $T = T_0$, by assumption $\mu_{A, gas}(T_0, P) = \mu_{A, liq}(T_0, P)$ @ eq. (assuming gas is pure solvent)

\int

$(T - T_0) \left(\frac{\partial \mu_0}{\partial T} \right) - \frac{N_B kT}{N_A} = (T - T_0) \left(\frac{\partial \mu_{gas}}{\partial T} \right)$

Also,

$\mu = \frac{G}{N} \rightarrow \frac{\partial \mu}{\partial T} = \frac{1}{N} \left(\frac{\partial G}{\partial T} \right)_{P, N} = \frac{-S}{N}$

\int

$(T - T_0) \left(\frac{-S_{liq}}{N_A} \right) - \frac{N_B kT}{N_A} = (T - T_0) \left(\frac{-S_{gas}}{N_A} \right)$

\int

$(T - T_0) \left[\frac{S_{gas}}{N_A} - \frac{S_{liq}}{N_A} \right] = \frac{N_B kT}{N_A}$

\int

$(T - T_0) = \frac{N_B kT}{S_{gas} - S_{liq}} = \frac{N_B kT}{\Delta S} = \frac{N_B kT}{Q/T_0} = \frac{N_B kT T_0}{L}$

$Q = L = \text{Latent heat}$

Assuming $T_0 \approx T$

$T - T_0 = \frac{N_B k T_0^2}{L}$

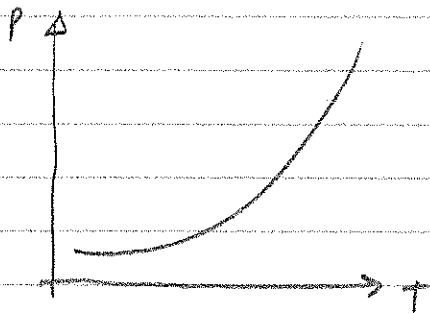
\int

$T - T_0 = \frac{n_B R T_0^2}{L}$

shift in boiling point of solvent due to n_B solute

Shift in vapor pressure

... (derivation in book)



Result's law

$$\frac{P}{P_0} = 1 - \frac{N_B}{N_A}$$

only for dilute solutions...

Ch 6 Boltzmann Statistics

Goal: Get multiplicity for more complicated systems

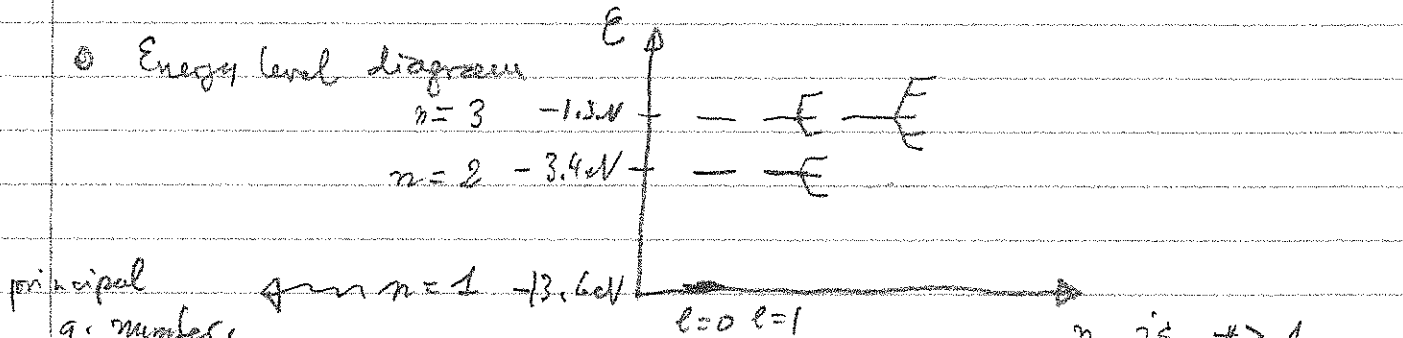
April 16, 2019

Goal: "System" of a single atom in a reservoir of other atoms at same temperature T

Macrostate = energy level. These energy levels are degenerate. \rightarrow multiple microstates.

Ex Hydrogen atom, n, l, m_l, m_s .

Energy level diagram



l : orbital angular momentum. l is $0, 1, \dots, (n-1)$

m_l : z-component of orbital angular momentum $-l \leq m_l \leq l$

m_s : z-component of spin angular momentum

$$m_s = \pm \frac{1}{2}$$

In general, for H, degeneracy is $2n^2$ for H

- Single atom exchanges energy with reservoir at temp T .
Assumption \rightarrow all microstates with in a given macrostate are equally probable.

• Macrostate of the atom + reservoir system with highest multiplicity should be most probable.

• Remember : $P(A) = \frac{\#A}{\# \Omega} \rightarrow \xi$

- Use ratios instead to avoid $\# \Omega$. Take 2 possible states of atom s_1, s_2 .

- $E(s_1)$ = Energy of atom in s_1
- $E(s_2)$ = Energy of atom in s_2
- $P(s_1)$ = prob. in s_1
- $P(s_2)$ = prob. in s_2

Want state with highest multiplicity in combined atom + reservoir system \rightarrow most probable.

$\Omega_R(s_i)$ \rightarrow multiplicity of reservoir when atom is in state s_i

$P_R(s_i) \propto \Omega_R(s_i) \Rightarrow \frac{P(s_2)}{P(s_1)} = \frac{\Omega_R(s_2)}{\Omega_R(s_1)} \quad S = k \ln \Omega$

$S = k \ln \Omega \rightarrow \frac{P(s_2)}{P(s_1)} = \frac{e^{S_R(s_2)/k}}{e^{S_R(s_1)/k}} = e^{\underbrace{(S_R(s_2) - S_R(s_1))}_{\downarrow}}/k$

infinitesimal change in entropy of reservoir

$dS_R = \frac{1}{T_R} [dW_R + PdV_R - \mu dN_R]$
 equal & opposite to the atoms ...

$\rightarrow PdV_R \sim (\Delta A)^3$ at Δ atom $\rightarrow (10^5 \text{ Pa})(10^{-10})^3 \approx 10^{-25} \text{ J}$
 $dV_R \sim \text{few eV} \sim 10^{-19} \text{ J}$

$\oint PdV_R \ll dU_R \rightarrow \text{ignore} \rightarrow dV_R = 0$
 $A_{\text{res}}, dN_R \approx 0$

$\oint, [S_R(s_2) - S_R(s_1)] = \frac{1}{T_R} [U_R(s_2) - U_R(s_1)]$

$[S_R(s_2) - S_R(s_1)] = \frac{-1}{T_R} [E(s_2) - E(s_1)]$

And so,

$$\frac{P(s_2)}{P(s_1)} = \frac{e^{-[E(s_2) - E(s_1)]/kT}}{e^{-E(s_1)/kT}} = \frac{e^{-E(s_2)/kT}}{e^{-E(s_1)/kT}}$$

\approx Boltzmann factor...

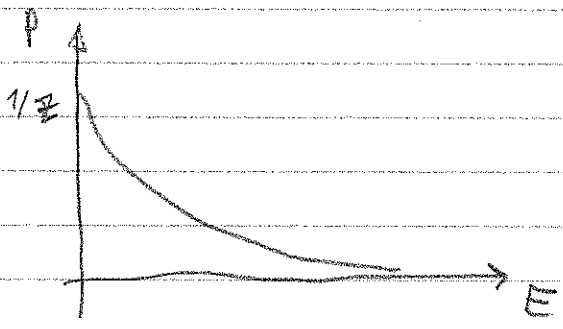
$$e^{-E(s)/kT}$$

$\oint P(s_2) e^{E(s_2)/kT} = P(s_1) e^{E(s_1)/kT} \Rightarrow$ must be constant.
 \uparrow indep. of s_1 , \uparrow indep. of s_2

$$\frac{P(s_2)}{e^{-E(s_2)/kT}} = \frac{P(s_1)}{e^{-E(s_1)/kT}} = \text{constant} = \frac{1}{Z}$$

$$P(s) = \frac{1}{Z} e^{-E(s)/kT}$$

\Rightarrow Boltzmann distribution (canonical distribution)



Z: The Partition Function

Total probability of finding an atom in some state or another = 1

$$1 = \sum_s P(s) = \sum_s \frac{1}{Z} e^{-E(s)/kT} = \frac{1}{Z} \sum_s e^{-E(s)/kT}$$

\oint $Z = \sum_s e^{-E(s)/kT}$ \rightarrow partition function...
constant

April 17, 2019

$Z \rightarrow$ normalization factor that converts Boltzmann factor into a prob

Temp. dependence of Z

- ① Low T, @ room T, $kT \approx 0.0257 \text{ eV}$
 ground state energy = 0 eV
 \rightarrow dominates partition function.

Ex Excited state $e^{-10.2 \text{ eV}/kT}$ while $e^{-0} = 1$

\rightarrow @ low T, $Z \approx 1$ \rightarrow 1 possible state available...

- ② At high T $E < kT$

$$Z = e^{-0/kT} + e^{-E_2/kT} + \dots$$

$$= 1 + (\text{order of unity}) + \dots$$

$\oint Z \gg 1$

- ① At high temp, there are many states available...

greetings

Applications of Boltzmann factors

Thermal excitations of atoms in stellar atmospheres...

Consider H atom in atm of sun ($T \sim 5800\text{K}$).
What is the prob. of finding e^- in one of the first excited states compared to probability of finding e^- in ground state.

$$\frac{P(s_2)}{P(s_1)} = \frac{e^{-E_2/kT}}{e^{-E_1/kT}} = e^{-(E_2-E_1)/kT} \quad \&$$

For H, $E_2 - E_1 = \Delta E = -3.4\text{eV} - (-13.6\text{eV}) = 10.2\text{eV}$

And $kT = (8.62 \times 10^{-5}\text{eV/K})(5800\text{K}) = 0.50\text{eV}$

$$\frac{P(s_2)}{P(s_1)} = e^{-10.2\text{eV}/0.5\text{eV}} = 1.4 \times 10^{-9}$$

But we need to add "statistical weights" to account for degeneracy of energy levels...

$$\begin{aligned} g_2 &= 8 & (2n^2) & \quad \& \quad P(E_2)/P(E_1) = \frac{g_2}{g_1} e^{-\Delta E/kT} \\ g_1 &= 2 & & & & = 4 [1.4 \times 10^{-9}] \\ & & & & & = 5.6 \times 10^{-9} \end{aligned}$$

Caveat At some temp T , we start ionizing atoms.

→ No more e^- for upwards transitions.

→ Boltzmann dist is only part of the story...

↑
Excitation → need to add Saha equation to account for

ionization. Saha eqn:

pressure \rightarrow

$$\frac{P_{H(\text{ionized})}}{P_{H(\text{neutral})}} = \frac{1}{n_e} \left(\frac{2\pi m_e kT}{h^2} \right)^{3/2} e^{-E_I/kT}$$

Average values

S.G.2.

$$P(s) = \frac{1}{Z} e^{-E(s)/kT} = \frac{1}{Z} e^{-\beta E(s)}$$

where $\beta = 1/kT$

And so $Z = \sum_s e^{-E(s)/kT} = \sum_s e^{-\beta E(s)}$

Imagine we have an atom with 3 discrete energy levels...

0eV, 4eV, 7eV ...

Sup we have 5 such atoms, 2 in ground, 2 in 1st state, 1, in 2nd state.

Average energy of all 5 atoms is:

$$\bar{E} = \frac{0 \cdot \text{eV} \cdot 2 + 4 \cdot \text{eV} \cdot 2 + 7 \cdot \text{eV} \cdot 1}{5} = \frac{17 \text{eV}}{5} = 3.4 \text{eV} \dots$$

or

$$\bar{E} = \left(\frac{2}{5} \cdot 0 \text{eV} \right) + \left(\frac{2}{5} \cdot 4 \text{eV} \right) + \left(\frac{1}{5} \cdot 7 \text{eV} \right)$$

$$= P(s_0) \cdot 0 \text{eV} + P(s_1) \dots$$

$\frac{1}{Z} e^{-\beta E(s)}$

\uparrow

Generalize

$$\bar{E} = \frac{\sum_s E(s) N(s)}{N} = \sum_s E(s) \frac{N(s)}{N} = \sum_s E(s) P(s)$$

$\bar{E} = \frac{1}{Z} \sum_s E(s) e^{-\beta E(s)}$

For any system in thermal equilibrium with reservoir at temp T, average value of the energy, \bar{E} :

$$\bar{E} = -\frac{1}{Z} \frac{\partial Z}{\partial \beta} \quad \text{where } \beta = \frac{1}{kT}$$

or equivalently

$$\bar{E} = -\frac{\partial \ln(Z)}{\partial \beta}$$

Proof

$$\frac{\partial Z}{\partial \beta} = \frac{\partial}{\partial \beta} \left[\sum_s e^{-\beta E(s)} \right] = \sum_s \frac{\partial}{\partial \beta} e^{-\beta E(s)} = \sum_s -E(s) e^{-\beta E(s)}$$

So

$$-\frac{1}{Z} \frac{\partial Z}{\partial \beta} = \frac{1}{Z} \sum_s +E(s) e^{-\beta E(s)} = \sum_s \left(\frac{1}{Z} E(s) e^{-\beta E(s)} \right) = \sum E(s) \cdot P(s)$$

$$\text{So } \boxed{-\frac{1}{Z} \frac{\partial Z}{\partial \beta} = \bar{E}}$$

Can also show that

$$\bar{E}^2 = \frac{1}{Z} \frac{\partial^2 Z}{\partial \beta^2}$$

How is work related to Z?

→ suppose we have a system characterized by a single param, x.

→ Quasi-static change in x, $x \rightarrow x + dx$

• Energy of state (s) changes by some small amount

$$\Delta E_s = \frac{\partial E_s}{\partial x} dx$$

• Work done on the system $\Rightarrow W = \int F dx \approx \sum F_i \Delta x$
where $F \rightarrow$ is change in Energy w.r.t x.

$$F = \frac{\partial E_s}{\partial x}$$

$$\text{• Work done on system } W = \frac{\sum_s \frac{\partial E_s}{\partial x} e^{-\beta E(s)} \Delta x}{\sum_s e^{-\beta E(s)}}$$

Re-writes numerator

$$\sum_s e^{-\beta E(s)} \frac{\partial E(s)}{\partial x} = -\frac{1}{\beta} \frac{\partial}{\partial x} \left(\sum_s e^{-\beta E(s)} \right)$$

$$\int_0 \sum_s e^{-\beta E(s)} \frac{\partial E(s)}{\partial x} = -\frac{1}{\beta} \frac{\partial}{\partial x} \left(\underbrace{\sum_s e^{-\beta E(s)}}_Z \right)$$

$$= -\frac{1}{\beta} \frac{\partial Z}{\partial x}$$

\int_0

$$W = -\frac{1}{\beta} \frac{\partial Z}{\partial x} dx / Z$$

\int_0

$$W = -\frac{1}{\beta} \frac{\frac{\partial Z}{\partial x} dx}{Z} = -\frac{1}{\beta Z} \frac{\partial Z}{\partial x} dx = -\frac{1}{\beta} \frac{\partial \ln Z}{\partial x} dx$$

\int_0

$$W_{on} = -\frac{1}{\beta} \frac{\partial \ln Z}{\partial x} dx$$

For example, $x = V$ (volume)

$$W_{on} = -\bar{P} dV = -\frac{1}{\beta} \frac{\partial \ln Z}{\partial V} dV$$

\int_0

$$\bar{P} = \frac{1}{\beta} \frac{\partial \ln Z}{\partial V}$$

How is Z related to S ?

$Z = Z(\beta, x)$. For small changes in Z ,

$$d \ln Z = \underbrace{\frac{\partial \ln Z}{\partial x} dx}_{\uparrow} + \underbrace{\frac{\partial \ln Z}{\partial \beta} d\beta}_{\uparrow}$$

$$\int_0 \boxed{d \ln(Z) = -\beta W_{on} + -\bar{E} d\beta}$$

\uparrow
 dW_{on}

Re-writing $d \ln Z = -\beta dW - d(\bar{E}\beta) + \beta d\bar{E}$

So $d(\ln Z + \bar{E}\beta) = \beta \underbrace{(d\bar{E} - dW)}_{dQ \text{ (first law)}} = \beta dQ = \frac{dQ}{kT} = \frac{1}{R} ds$

So $d(\ln Z + \bar{E}\beta) = \frac{ds}{R}$

Now, $S = k \ln \Omega$

So $S = k(\ln Z + \beta \bar{E})$

So $\ln Z + \beta \bar{E} = \ln \Omega$

So $\ln Z = \ln \Omega - \beta \bar{E}$

Example of paramagnetism

Before: (1) $\Omega(N_T) = \binom{N}{N_T} = \frac{N!}{N_T! N_D!}$

(2) $S = k \ln \Omega$ (use Stirling approximation)

(3) $\frac{1}{T} = \left(\frac{\partial S}{\partial U}\right)$

(4) $U = U(T) \rightarrow u = -N \mu_B \tanh\left(\frac{\mu_B}{kT}\right)$

(5) $M = \frac{-u}{B}$

(6) $C_B = \left(\frac{\partial U}{\partial T}\right)_B$

Now, we'll redo this with Boltzmann statistics... Two possible energy states...

"up" $\mu = -\mu_B$ } then $Z = \sum_s e^{-\beta E(s)} = e^{-\beta(-\mu_B)} + e^{-\beta(\mu_B)}$
"down" $\mu = \mu_B$ } $= e^{\mu_B \beta} + e^{-\mu_B \beta}$
So $Z = 2 \cosh(\mu_B \beta)$

Probability of finding in up/down direction,

$$P_{\uparrow} = \frac{e^{\beta\mu B}}{2 \cosh(\mu\beta B)}, \quad P_{\downarrow} = \frac{e^{-\beta\mu B}}{2 \cosh(\mu\beta B)}, \quad P_{\downarrow} + P_{\uparrow} = 1$$

Average energy of a dipole

$$\begin{aligned} \bar{E} &= \sum_s E(s) P(s) = (-\mu B) \frac{e^{\beta\mu B}}{2 \cosh(\mu\beta B)} + (\mu B) \frac{e^{-\beta\mu B}}{2 \cosh(\mu\beta B)} \\ &= (-\mu B) \frac{2 \sinh(\mu\beta B)}{2 \cosh(\mu\beta B)} \\ &= -\mu B \tanh(\mu\beta B) \end{aligned}$$

$$\bar{E} = -\mu B \tanh(\mu\beta B)$$

$$E_{\text{tot}} = -N\mu B \tanh(\mu\beta B) = -N\mu B \tanh\left(\frac{\mu B}{kT}\right)$$

Alternate approach

$$\begin{aligned} \bar{E} &= -\frac{1}{Z} \frac{\partial Z}{\partial \beta} \\ &= -\frac{1}{Z} \frac{\partial}{\partial \beta} \left[2 \cosh(\mu\beta B) \right] \\ &= -\frac{1}{Z} \cdot 2 \left(\mu B \sinh(\mu\beta B) \right) \\ &= \frac{2\mu B}{2 \cosh(\mu\beta B)} \cdot \sinh(\mu\beta B) \\ &= -\mu B \tanh(\mu\beta B) \end{aligned}$$

$$E_{\text{tot}} = -N\mu B \tanh(\mu\beta B)$$

Magnetisation $\Rightarrow M = N\bar{\mu}_z, \quad \bar{\mu}_z = \sum \mu_z P(s) \dots$

$$= +\mu P_{\uparrow} + (-\mu) P_{\downarrow}$$

April 22, 2019

The Equipartition Theorem

↳ applies to systems with quadratic degrees of freedom.

$E = p^2/2m$
 $E = cq^2$ where $q =$ position or momentum coordinates...

• $Z = \sum_q e^{-\beta cq^2}$, and assuming that the spacing Δq is constant and small...

$$\underline{\delta} \quad Z = \frac{1}{\Delta q} \sum_q e^{-\beta cq^2} \Delta q$$
$$= \frac{1}{\Delta q} \int_{-\infty}^{\infty} e^{-\beta cq^2} dq$$

Change of variable: let $x = \sqrt{\beta c} \cdot q \rightarrow x^2 = \beta c q^2$

$dq = \frac{dx}{\sqrt{\beta c}}$

$$\underline{\delta} \quad Z = \frac{1}{\Delta q} \int_{-\infty}^{\infty} e^{-x^2} dx \cdot \frac{1}{\sqrt{\beta c}} = \frac{1}{\Delta q} \frac{1}{\sqrt{\beta c}} \int_{-\infty}^{\infty} e^{-x^2} dx$$

assumption...

$Z = \frac{\sqrt{\pi}}{\Delta q \sqrt{\beta c}}$

(*) As long as $\Delta q \ll kT$, then equipartition holds (high temp)

$$\underline{\delta} \quad \boxed{Z = \frac{1}{\Delta q} \sqrt{\frac{\pi}{\beta c}}}$$

or, equivalently, $\boxed{Z = C \beta^{-1/2}}$ \rightarrow C is some constant...

• $\underline{\delta} \quad E = -\frac{1}{Z} \frac{\partial Z}{\partial \beta} = -\frac{1}{C \beta^{-1/2}} \left(\frac{-1}{2} C \beta^{-3/2} \right) \Rightarrow \bar{E} = \frac{1}{2} \beta^{-1}$

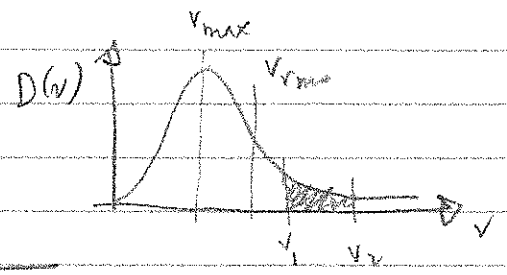
$$\underline{\delta} \quad \boxed{\bar{E} = \frac{1}{2} kT} \rightarrow \text{Eq. partition theorem for 1/2 kT df.}$$

Note Conditions

Equipartition doesn't hold for quantum mechanical systems, since it requires a continuum of states.

Equipartition holds if $\Delta \epsilon \ll kT$ (high temp)

The Maxwell's Speed Distribution



From equipartition, can imagine:

$$\frac{1}{2}mv^2 = \frac{3}{2}kT, \text{ then } v_{rms} = \sqrt{\frac{3kT}{m}}$$

$$P(v_1 \leq v \leq v_2) = \int_{v_1}^{v_2} D(v) dv, \text{ where } D(v) \text{ is the dist. function.}$$

↘ pdf,

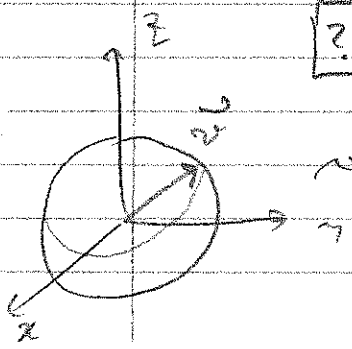
What is $D(v)$? → $D(v) \propto$ prob that a molecule will have velocity \vec{v} - a # of vectors, \vec{v} corresponding to speed v .

$$D(v) \propto \underbrace{\left(\text{prob. of molecule w/ velocity } \vec{v} \right)}_{\boxed{?}} \times \underbrace{\left(\# \text{ of vectors, } \vec{v} \text{ corresponding to speed } v \right)}_{\substack{\uparrow \\ \text{use } \boxed{??}}}$$

know, $\boxed{?} \propto$ Boltzmann factor... $E = \frac{1}{2}mv^2 \rightarrow = \boxed{e^{-mv^2/2kT}}$

$\boxed{??} \propto 4\pi v^2$

↳ larger v , more surface area, higher D for v .



$$D(v) = C (4\pi v^2) e^{-mv^2/2kT}$$

$$1 = \int_0^\infty D(v) dv = 4\pi C \int_0^\infty v^2 e^{-mv^2/2kT} dv$$

Change of vars, $x = v \sqrt{\frac{m}{2kT}}$, then...

$$1 = 4\pi C \int_0^\infty x^2 e^{-x^2} dx \left(\sqrt{\frac{2kT}{m}}\right)^3$$

$$= 4\pi C \cdot \left(\frac{2kT}{m}\right)^{3/2} \int_0^\infty x^2 e^{-x^2} dx$$

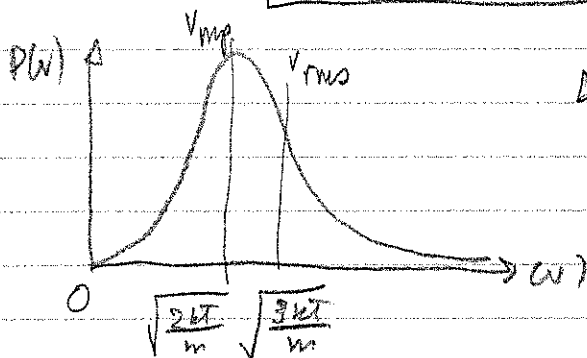
$\sqrt{\pi}/4$

Maxwell's speed distribution...

$$C = \left(\frac{m}{2\pi kT}\right)^{3/2}$$

Thus,

$$D(v) = 4\pi v^2 \left(\frac{m}{2\pi kT}\right)^{3/2} e^{-mv^2/2kT}$$



$$D(v) = 0 \text{ @ } v=0 \text{ - } v \rightarrow \infty$$

Calculate v_{mp} (most probable)

$$0 = \frac{d}{dv} D(v) = 0 \rightarrow 0 = \frac{d}{dv} \left[v^2 e^{-mv^2/2kT} \right]$$

$$0 = 2v e^{-mv^2/2kT} + v^2 \cdot \left(\frac{-mv}{kT}\right) e^{-mv^2/2kT}$$

$$= 2v + \frac{-mv^3}{kT} \Rightarrow 0 = 2 - \frac{mv^2}{kT} \Rightarrow$$

$$v_{mp} = \sqrt{\frac{2kT}{m}}$$

8 Calculate \bar{v}

$$\bar{v} = \langle v \rangle = \int_0^{\infty} v D(v) dv = \int_0^{\infty} 4\pi v^3 \left(\frac{m}{2\pi kT} \right)^{3/2} e^{-\frac{mv^2}{2kT}} dv$$

$$= 4\pi \left(\frac{m}{2\pi kT} \right)^{3/2} \int_0^{\infty} v^3 e^{-\frac{mv^2}{2kT}} dv$$

$$\bar{v} = \left(\frac{m}{2\pi kT} \right)^{3/2} (4\pi) \cdot \frac{1}{2} \left(\frac{2kT}{m} \right)^2$$

$$\bar{v} = \left(\frac{2kT}{m} \right)^{1/2} \cdot \frac{2}{\sqrt{\pi}}$$

$$\bar{v} = \left(\frac{8kT}{m\pi} \right)^{1/2}$$

Ex N_2 in air @ room temp... $T = 298K$, $M = 14g/mol$
 $m_N = 14g/mol$
 $m_{N_2} = 28g/mol$

$$v_{mp} = \sqrt{\frac{2kT}{m}} = \sqrt{\frac{2(1.38 \times 10^{-23})(298K)}{28 \times 10^{-3} kg/mol / 6.023 \times 10^{23}}} \approx 420.5 m/s$$

April 23, 2019

PARTITION FUNCTION ~ FREE ENERGY

$\Omega(u)$ @ const $u \Rightarrow S \text{ tends } -\ln T$, $S = k \ln \Omega$

$Z(T) \Leftrightarrow F$ @ constant T

Recall $F = U - TS \rightarrow \frac{F-U}{T} = -S$

$$dF = -PdV - SdT + \mu dN \rightarrow \left(\frac{\partial F}{\partial T} \right)_{V,N} = -S$$

$$\text{So, } \left(\frac{\partial F}{\partial T} \right)_{V,N} = \frac{F-U}{T} \quad (1)$$

Guess $\tilde{F} = -kT \ln Z \Rightarrow Z = e^{-\tilde{F}/kT}$

Check deriv w.r.t T: $\frac{\partial \tilde{F}}{\partial T} = \frac{\partial}{\partial T} (-kT \ln Z)$
 $= -k \ln Z - kT \frac{\partial}{\partial T} \ln Z$
 $= -k \ln Z - kT \frac{\partial \beta}{\partial T} \frac{\partial}{\partial \beta} \ln Z$

$\frac{\partial \tilde{F}}{\partial T} = -k \ln Z - \frac{U}{T}$

$\frac{\partial \tilde{F}}{\partial T} = \frac{\tilde{F}}{T} - \frac{U}{T} = \frac{\tilde{F} - U}{T}$, same as (1), so $-U$
we know guess was correct, except there might be a constant

Check initial condition (to determine constant)

$F = U - TS$ let's use $T=0$ then $F(T=0) = U_0$

$Z (@T=0) = \sum_{\epsilon_0} e^{-E(\epsilon)/kT}$ lowest possible energy.
 $= e^{-U_0/kT} + \text{high order terms, negligible because } U \gg kT$

$\tilde{F}(T=0) = -kT \ln Z = -kT (-U_0/kT) = -U_0$

$\tilde{F}(T=0) = U_0$ no constant!

$F = -kT \ln Z$

$dF = -PdV - SdT + \mu dN$

$\left(\frac{\partial F}{\partial V}\right)_{T,N} = -P, \left(\frac{\partial F}{\partial T}\right)_{V,N} = -S, \left(\frac{\partial F}{\partial N}\right)_{V,T} = \mu$

Example

$\left(\frac{\partial F}{\partial T}\right)_{V,N} = -S, F = -kT \ln Z, S = -\frac{\partial}{\partial T} (-kT \ln Z)$

$$S = \frac{-\partial}{\partial T} (-k_B T \ln Z) = k_B \ln Z + \frac{\partial P}{\partial T} \frac{\partial}{\partial P} \ln Z$$

$$= k_B \ln Z + \frac{\bar{E}}{T}$$

↳ $S = k_B (\ln Z + \beta \bar{E})$ ✓ same as before

or $\ln Z = \frac{S}{k_B} - \beta \bar{E}$

Partition Function for Composite System

Goal: write an expression for Z for an ideal gas

1st: Determine how Z_{tot} depends on Z for each individual particle...

Start w/ system of 2 particles. If they do not interact, total energy

$$E_{tot} = E_1 + E_2$$

$$Z_{tot} = \sum_c e^{-\beta [E_1(s) + E_2(s)]} = \sum_s e^{-\beta E_1(s)} e^{-\beta E_2(s)}$$

If we also assume that states of individual particles are independent of each other:

$$Z_{tot} = \underbrace{\sum_{s_1} e^{-\beta E_1(s_1)}}_{Z_1} \underbrace{\sum_{s_2} e^{-\beta E_2(s_2)}}_{Z_2} \Rightarrow \boxed{Z_{tot} = Z_1 Z_2}$$

(non-interacting distinguishable system particles)

If particles are indistinguishable, we have double counted states.

↳ $Z_{tot} \approx \frac{1}{2} Z_1 Z_2$ ↗ or $Z_{tot} = Z_1^N$

Generalize this to N particles → $Z_{tot} = Z_1 Z_2 \dots Z_N$ distinguishable

For distinguishable, $\boxed{Z_{tot} = \frac{1}{N!} Z_1^N}$

April 26, 2019

Working towards Z for ideal gas.

$$Z_{tot} = \frac{1}{N!} Z_n^N$$

$$E_{tot} = E_{tr} + E_{int}$$

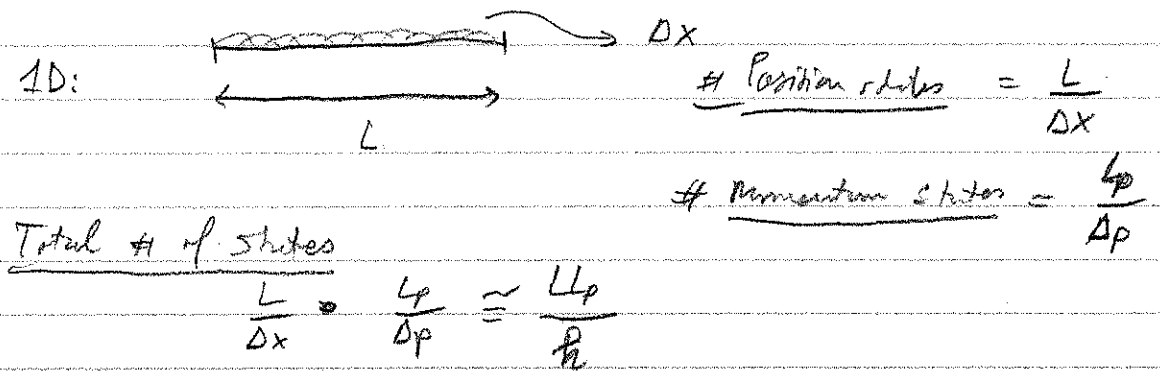
↓
 (translation) internal modes (rotation/vibration)
 (KE)
 or thermal energy

Boltzmann factor $\rightarrow e^{-E_{tr}(s)/kT} = e^{-(E_{tr})/kT} \cdot e^{-E_{int}(s)/kT}$

$\int Z_i = Z_{tr} Z_{int}$ ignore this one for now...

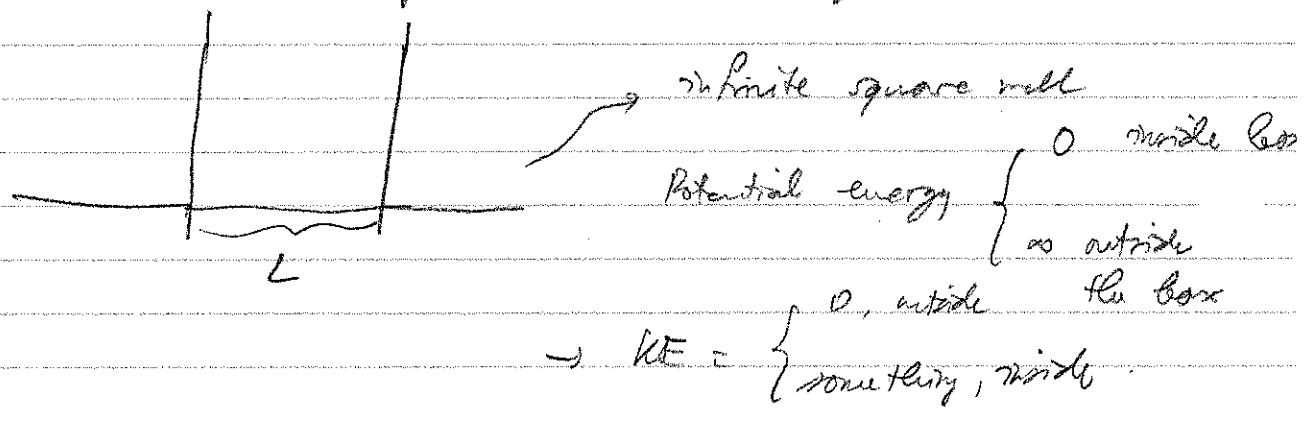
$$Z_{tr} = \sum_{tr} e^{-E_{tr}(s)/kT} \quad \& \quad Z_{int} = \sum_{int} e^{-E_{int}(s)/kT}$$

② when we counted states before:



③ More rigorously,

↳ count all independent, definite energy states or wavefunction



$$KE = \frac{1}{2}mv^2 = \frac{p^2}{2m} = \frac{h^2}{2m\lambda^2}$$

→ only certain wavelengths are allowed

$$\lambda = \frac{h}{p} = \frac{h}{2\pi}$$

allowed momenta

$$\lambda_n = \frac{2L}{n}, n=1,2,3, \dots$$

$$E_n = \frac{p^2}{2m} = \left(\frac{hn}{2L}\right)^2 \frac{1}{2m} = \frac{h^2 n^2}{8mL^2}$$

allowed independent energies..

$$Z_{(1-D)} = \sum e^{-E_n/kT}$$

$$= \sum_n \exp\left[-\frac{h^2 n^2}{8mL^2} \cdot \beta\right]$$

assume large $T, L \rightarrow \int_0^\infty \exp\left[-\frac{h^2 n^2}{8mL^2 kT}\right] dn$

$$\Delta n = 1$$

$$\text{let } x = \frac{hn}{\sqrt{8mL^2 kT}} \rightarrow \frac{dx}{dn} = \frac{h}{\sqrt{8mL^2 kT}}$$

$$Z_{1D} = \frac{\sqrt{8mL^2 kT}}{h} \int_0^\infty e^{-x^2} dx$$

$$= \sqrt{\frac{8mL^2 kT}{h^2}} \cdot \sqrt{\frac{\pi}{2}}$$

$$Z_{1D} = \frac{\sqrt{2\pi m kT}}{h} L = \frac{L}{l_q}$$

l_q = "quantum length" $l_q = \frac{h}{\sqrt{2\pi m kT}}$

The quantum length, l_q is roughly the de Broglie λ of a particle of mass m - energy kT ...

$$= \frac{h}{\sqrt{2\pi m kT}}$$

$$\lambda = \frac{h}{p}, E = kT = \frac{p^2}{2m} \rightarrow p = \sqrt{2m kT}, \text{ then}$$

$$\lambda = \frac{h}{\sqrt{2m kT}}$$

Δ $l_0 \sim$ roughly the size of a particle... For N_2 :

\square Δ For N_2 @ $T = 298K$, $l_0 \approx 1.0 \times 10^{-10}m$

$\Rightarrow \frac{L}{l_0}$ is large.

In three dimensions

$$E_{tr} = \frac{p_x^2}{2m} + \frac{p_y^2}{2m} + \frac{p_z^2}{2m}$$

independent

each $p_{i,n} = \frac{h n_i}{2L}$

$$E_{tr} = \sum_i e^{-E_i/kT} = \sum_{n_x, n_y, n_z} e^{-\frac{h^2 n_x^2}{8mL_x^2 kT}} e^{-\frac{h^2 n_y^2}{8mL_y^2 kT}} e^{-\frac{h^2 n_z^2}{8mL_z^2 kT}}$$

= ...

$$= \frac{L_x}{l_0} \cdot \frac{L_y}{l_0} \cdot \frac{L_z}{l_0}$$

for each atom.

$$Z_{tr} = \frac{V}{l_0^3} = \frac{V}{V_0}$$

"quantum volume"

$$V_0 = l_0^3 = \left(\frac{h}{\sqrt{2\pi m kT}} \right)^3$$

$$Z_{tot} = \frac{1}{N!} Z_1^N = \frac{1}{N!} (Z_{tr} \cdot Z_{int})^N$$

$$Z_{tot} = \frac{1}{N!} \left(\frac{V}{V_0} \cdot Z_{int} \right)^N$$

ignore this

Sometimes, \log of Z is more useful...

Stirling's approx

$$\ln Z_{\text{tot}} = \frac{N}{V_0} \left(\ln V + \ln Z_{\text{int}} - \ln V_0 \right) - N \ln N + N$$

So,
$$\ln Z_{\text{tot}} = N \left[\ln V + \ln Z_{\text{int}} - \ln V_0 - \ln N + 1 \right]$$

log of partition function for ideal gas...

Now we can predict the thermodynamic properties of ideal gas

Average energy of ideal gas \rightarrow expect $\bar{E} = \frac{3kTN}{2}$

$$\ln Z_{\text{tot}} = N \left[\ln V + \ln Z_{\text{int}} - \ln V_0 - \ln N + 1 \right]$$

$$\bar{E} = - \frac{1}{Z} \frac{\partial Z}{\partial \beta} = - \frac{\partial \ln Z}{\partial \beta}$$

Note: V is independent of T, β
 N is also independent of T, β
 Z_{int}, V_0 depend on β .

So,

$$\bar{E} = -N \left[\frac{\partial}{\partial \beta} (\ln Z_{\text{int}}) - \frac{1}{V_0} \frac{\partial V_0}{\partial \beta} \right]$$

$$= -N \left[-\bar{E}_{\text{int}} + \frac{1}{V_0} \frac{\partial}{\partial \beta} \left(\frac{h^2}{2\pi m k T} \right)^{3/2} \right]$$

$$= N \bar{E}_{\text{int}} + \frac{1}{V_0} \left(\frac{h^2}{2\pi m} \right)^{3/2} \frac{\partial}{\partial \beta} (\beta^{3/2})$$

$$= N \bar{E}_{\text{int}} + \frac{1}{V_0} \left(\frac{h}{\sqrt{2\pi m}} \right)^3 \frac{3}{2} \beta^{1/2}$$

$$= N \bar{E}_{\text{int}} + N \left(\frac{\sqrt{2\pi m k T}}{h} \right)^3 \left(\frac{h}{\sqrt{2\pi m}} \right)^3 \cdot \frac{3}{2} \sqrt{\beta}$$

$$= N \bar{E}_{\text{int}} + \frac{3}{2} N \rho^{-1}$$

$$\bar{E} = N \bar{E}_{\text{int}} + \frac{3}{2} N k T$$

→ if assume no internal energy, $E \rightarrow \frac{3}{2} NkT$
 → E_{int} depends on E_{eq} - Partition Function

Heat Cap $C_V = \left(\frac{\partial U}{\partial T} \right) = \left(\frac{\partial U_{int}}{\partial T} \right) + \frac{3}{2} Nk$

April 29, 2011

Ch 7: QUANTUM STATISTICS

↳ we'll use Gibbs factors instead of Boltzmann factor...

↳ think about system that can exchange energy or particles...

↳ look at ratio of probabilities $\frac{P(s_2)}{P(s_1)} = \frac{\Omega_R(s_2)}{\Omega_R(s_1)} = \frac{e^{S_R(s_2)/k}}{e^{S_R(s_1)/k}}$

$\frac{P(s_2)}{P(s_1)} = e^{(S_R(s_2) - S_R(s_1))/k}$

$dS_R = \frac{1}{T} [dU_R + PdV_R - \mu dN_R]$

• Assume that $dV_R = 0$

• keep μN terms their same dU_{sys} μdN_{sys}

$\frac{P(s_2)}{P(s_1)} = \frac{\Omega_R(s_2)}{\Omega_R(s_1)} = \frac{-1}{T} [(E(s_2) - E(s_1)) - (\mu N(s_2) - \mu N(s_1))]$
 $= -\Delta S_R$

$\frac{P(s_2)}{P(s_1)} = \frac{e^{-[(E(s_2) - \mu N(s_2))]/kT}}{e^{-[(E(s_1) - \mu N(s_1))]/kT}}$

↳ instead of Boltzmann factor, we set this factor → Gibbs
 $e^{-(E(s) - \mu N)/kT}$

To get absolute probability → need constant of norm

$$P(s) = \frac{1}{Z} e^{-\frac{(E(s) - \mu N(s))}{kT}}$$

$Z \Rightarrow$ "grand partition function" or "Gibbs sum"

So that $\sum_s P(s) = 1 \Rightarrow Z = \sum_s e^{-\frac{(E(s) - \mu N(s))}{kT}}$

Sum over all Gibbs factors...

If you have more than 1 type of particle, then sum over all species μ, dN_i

Ex 2 particles -- Gibbs factor: $e^{-\frac{(E(s) - \mu_1 N_1(s) - \mu_2 N_2(s))}{kT}}$

BOSONS - FERMIONS

Quantum statistics → important for high density + low temp systems...

In this case, derivation of

$$Z_{tot} = \frac{1}{N!} z_1^N$$

localised down @ high density, low temperature..

$\frac{1}{N!}$ is not quite correct here.

Ex 2 interacting particles, each with 5 available states in the ground state energy, $E = 0$.

□ □ □ □ □ E = 0

Boltzmann factor = e⁻⁰ = 1 ⇒ Z = 5 so Z = 5

But • If distinguishable ⇒ Ω = 5 × 5 = 25 = Z
 & Z_{dist} = Z₁^N

• If indistinguishable ⇒ Ω = $\binom{5}{2} = 10$
 so Z = 10

Previous assumption for indistinguishable particles

Z_{dist} = $\frac{1}{N!} Z_1^N = \frac{25}{2!} = 12.5 \rightarrow$ don't make sense...

(Fermions) # states for indistinguishable particles ⇒ 10, no² particles are occupying the same state.

(Bosons) But if we allow them to be in the same state ⇒ 15 for indistinguishable particles that can be in the same state.
 → boson.

⇒ And so 12.5 → average between bosons = Fermions

Z $\frac{1}{N!} Z_1^N$
 correctly cuts down 20 states for distinguishable particles to 10 for indistinguishable particles. But also cuts down 5 → 2.5 incorrectly.

Bosons → can share the same (quantum) states (Ex; photons, pions, He nuclei). integer spin: 0, 1, 2, ...

Fermions → cannot occupy the same (q) states (e^- , p^+ , n , ν , ...)
 ↳ half-integer spin ($\frac{1}{2}$, $\frac{3}{2}$, ...)

Pauli exclusion principle

↳ $Z_{tot} = \frac{1}{N!} z_i^N$ interpolates between correct value for indistinguishable bosons, fermions...

☑ Bosons → governed by Bose-Einstein statistics.

☑ Fermions → governed by Fermi-Dirac statistics.

?

When do we need to use B-E or F-D stats rather than Boltzmann stats?

↳ when # of single particle states \gg # of particles, then it doesn't matter if we have bosons or fermions, use Boltzmann statistics

→ if $Z_i \gg N$

☑ Think back to Ideal gas: $Z_i = \frac{V}{V_Q} z_{int}$, where

$$V_Q = \left(\frac{h}{\sqrt{2\pi m kT}} \right)^{3/2}, \text{ for } Z_i \gg N$$

$\frac{V}{V_Q} \gg N$. And so, $\frac{V}{N} \gg V_Q$ → average distance between particles is \gg de Broglie wavelengths.

☑ when $\frac{V}{N} \sim V_Q$, then it matters whether we have bosons or fermions. → use Quantum Statistics

either B-E or F-D.

At high temperature, $Z_i \gg N \rightarrow$ Boltzmann statistics.

Single-particle state of a system

- System \rightarrow particular state of particle.
- "Reservoir" \rightarrow all the possible states.

April 30, 2019

DISTRIBUTION FUNCTIONS

- System \Rightarrow single-particle quantum state
- Reservoir \Rightarrow all other possible states

\sim If state is occupied, it has energy E
If unoccupied, energy 0

If state can be occupied by N particles \rightarrow energy NE

Probability of being occupied by N particles

$$P(N) = \frac{1}{Z} e^{-(NE - N\mu)/kT}$$

$$P(N) = \frac{1}{Z} e^{-N(E - \mu)/kT}$$

For Fermions, $n = 0$ or 1

$$Z_F = e^{0(\dots)/kT} + e^{-1(E - \mu)/kT} = 1 + e^{-(E - \mu)/kT}$$

Fermions: $Z_F = 1 + e^{-(E - \mu)/kT}$

determine the average # of particles in a state, or the occupancy of the state

FERMIONS

$$\bar{n} = \sum_n n P(n) = 0 \cdot P(0) + 1 \cdot P(1)$$

$$= \frac{e^{-(E-\mu)/kT}}{1 + e^{-(E-\mu)/kT}}$$

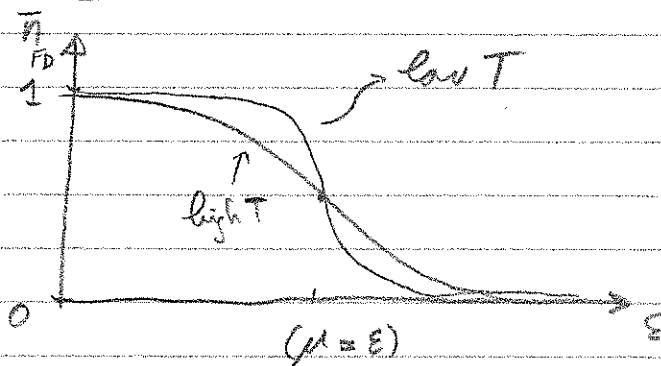
$$\bar{n}_{FD} = \frac{1}{e^{(E-\mu)/kT} + 1}$$

→ Fermi-Dirac distribution

■ If $E \gg \mu$ $\bar{n} \rightarrow 0$

■ If $E \ll \mu$ $\bar{n} \rightarrow 1$

■ If $E = \mu$ $\bar{n} \rightarrow 1/2$ → 50% chance of being occupied.



Bozons → $n \in \mathbb{N} \quad 0, 1, 2, \dots$

Then

$$\sum_{n=0}^{\infty} z^n = 1 + z + z^2 + z^3 + \dots$$

Use $\frac{1}{1-x} = 1 + x + x^2 + x^3 + \dots$ (geometric series)

$$\sum_{n=0}^{\infty} z^n = \frac{1}{1 - e^{-(E-\mu)/kT}}$$

Q. partition functions for bosons,

$$Z_B = \frac{1}{1 - e^{-(\epsilon - \mu)/kT}}$$

Q. Average occupancy: $\bar{n} = \sum_n n P(n)$, Let $x = \frac{\epsilon - \mu}{kT}$

$$\begin{aligned} \text{Then } \bar{n} &= \frac{\sum_n n e^{-nx}}{Z} = -\frac{1}{Z} \sum_n \frac{d}{dx} e^{-nx} \\ &= -\frac{1}{Z} \frac{d}{dx} \sum_n e^{-nx} \end{aligned}$$

$$\bar{n}_B = -\frac{1}{Z} \frac{d}{dx} Z$$

$$\begin{aligned} \frac{d}{dx} \bar{n}_B &= -(1 - e^{-x}) \cdot \frac{d}{dx} (1 - e^{-x})^{-1} \\ &= \frac{1 - e^{-x}}{(1 - e^{-x})^2} \cdot (e^{-x}) \\ &= \frac{e^{-x}}{1 - e^{-x}} \end{aligned}$$

$$\bar{n}_B = \frac{1}{e^x - 1}$$

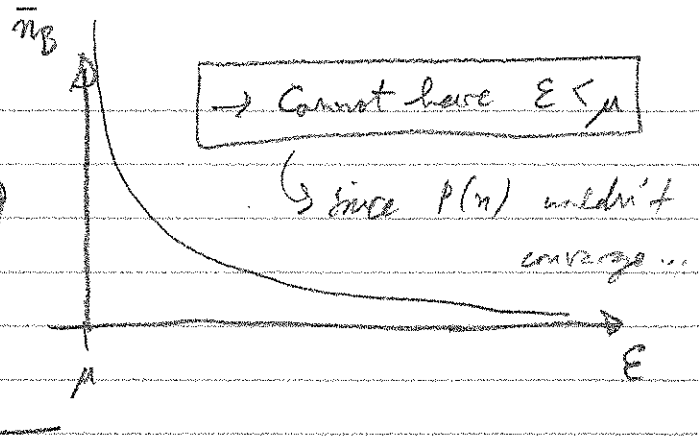
Fermi - Einstein dist.

$$\bar{n}_{BE} = \frac{1}{e^{+(\epsilon - \mu)/kT} - 1}$$

□ If $E \gg \mu \rightarrow \bar{n} \rightarrow 0$

□ If $E < \mu \rightarrow \bar{n} \rightarrow -1$ (X)

□ If $E \rightarrow \mu \rightarrow \bar{n} \rightarrow \infty$



□ Consider particles obeying Boltzmann statistics

$P(\epsilon) = \frac{1}{Z_1} e^{-E(\epsilon)/kT}$. If we have N particles, then

$\bar{n}_p = \frac{N}{Z_1} e^{-E(\epsilon)/kT} = \frac{N}{Z_1} e^{-E/kT}$

Boltzmann distribution.

$\mu = \left(\frac{\partial F}{\partial N} \right)_{T,V}$ & $F = -kT \ln Z$

□

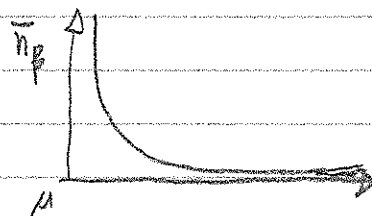
$\mu = -kT \ln \left(\frac{Z_1}{N} \right)$

□

$e^{-\mu/kT} = \frac{Z_1}{N}$ so $\bar{n}_{Boltz} = e^{\mu/kT} e^{-E/kT} = e^{-(E-\mu)/kT}$

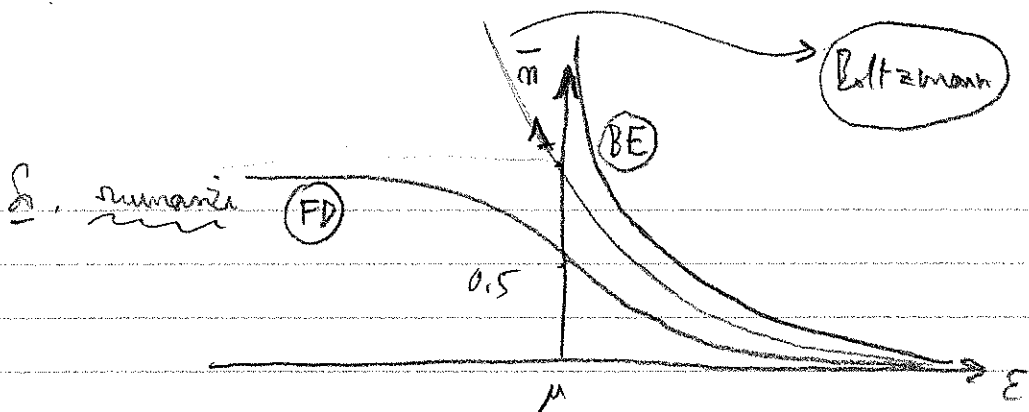
□

$\bar{n}_p = \frac{1}{e^{(E-\mu)/kT}}$



□

$\bar{n}_F = \frac{1}{e^x + 1}$, $\bar{n}_B = \frac{1}{e^x - 1}$, $\bar{n}_p = \frac{1}{e^x}$



NE
DEGENERATE FERMI GASES

Consider a gas of Fermions at low T, or $\frac{V}{N} \gg \lambda_Q^3$

Ex: for an electron at room temp:

$$\lambda_Q = \left(\frac{h}{\sqrt{2\pi m_e kT}} \right)^3 = (4.3 \text{ nm})^3$$

Typical conductor supplies 1 free e^- for every atom

↳ 1 e^- per atom $\rightarrow V \sim (\text{size of atom})^3 \sim (0.2 \text{ nm})^3$

May 2, 2018

Recall

$$\bar{n}_F = \frac{1}{e^{(\epsilon - \mu)/kT} + 1} \rightarrow$$

@ T=0 all $\epsilon < \mu$ will be occupied. All $\epsilon > \mu$ unoccupied

→ "degenerate Fermi gas"

At T=0 at $\mu(T=0) = \epsilon_F$ or Fermi Energy

Goal

Calculate \rightarrow total & average energy of Fermions

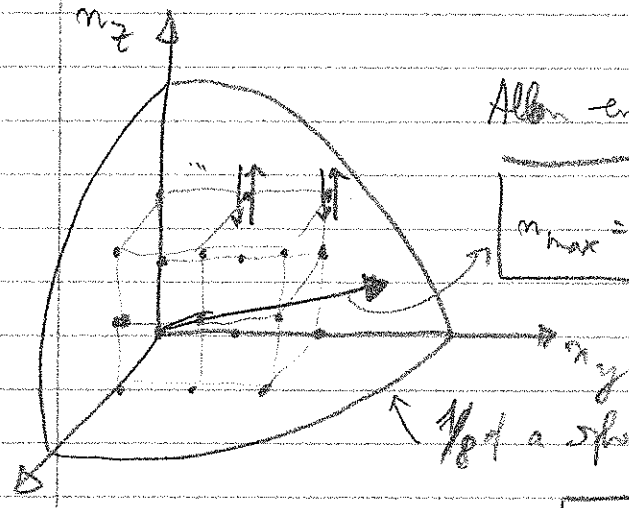
↳ degeneracy pressure. (where there's degenerate Fermi gas!!!)

Consider packing electrons into some 3D volume (infinite square well)

Allowed wavefunctions gives $\lambda_n = \frac{2L}{n}$ $\therefore p_n = \frac{h}{\lambda_n} = \frac{hn}{2L}$

$p_x = \frac{hn_x}{2L_x}$, $p_y = \frac{hn_y}{2L_y}$, $p_z = \frac{hn_z}{2L_z}$

n_x, n_y, n_z are integers, independent of each other...



Allowed energies: $E = \frac{|p|^2}{2m} = \frac{h^2}{2m} \left[\frac{n_x^2}{(2L)^2} + \frac{n_y^2}{(2L)^2} + \frac{n_z^2}{(2L)^2} \right]$

$n_{max} = \sqrt{n_x^2 + n_y^2 + n_z^2}$

Each point represents 2 electrons (spin $\pm 1/2$)

1/8 of a sphere of radius n_{max}

Want to calculate $E_F = \text{max energy}$

$E_F = \frac{h^2}{2m} \cdot \frac{1}{(2L)^2} = \frac{h^2}{8mL^2} n_{max}^2$

Total # of electrons = 2. Volume of 1/8 sphere

$N = 2 \cdot \left[\frac{1}{8} \cdot \frac{4}{3} \pi \cdot n_{max}^3 \right]$
 $N = \frac{1}{3} \pi \left[\sqrt{n_x^2 + n_y^2 + n_z^2} \right]^3$

Solve for n_{max}

$n_{max} = \left(\frac{3N}{\pi} \right)^{1/3}$

$E_F = \frac{h^2}{2m} (n_{max})^2 \cdot \frac{1}{4L^2}$

$E_F = \frac{h^2}{8mL^2} \left(\frac{3N}{\pi} \right)^{2/3}$

Fermi energy

Since $V = L^3 \Rightarrow L^2 = V^{2/3}$

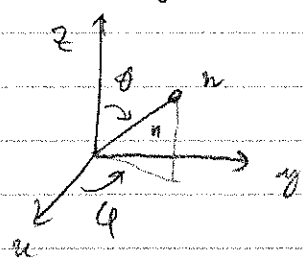
$$\epsilon_F = \frac{\hbar^2}{8m} \left(\frac{3N}{\pi V} \right)^{2/3}$$
 Fermi energy...

number density... intensive property...

Total energy of degenerate Fermi gas

$$U_{tot} = 2 \int_0^{\infty} \int_0^{\infty} \int_0^{\infty} \epsilon(n) dx dy dz \rightarrow$$
 assuming large # states...

Convert to spherical coordinates...



$$dV = dx dy dz = n^2 \sin\theta dp d\theta dn$$

$$U_{tot} = 2 \int_0^{n_{max}} \int_0^{\pi/2} \int_0^{2\pi} \epsilon(n) n^2 \sin\theta dp d\theta dn$$

$$= 2 \left(\frac{4\pi}{8} \right) \int_0^{n_{max}} \epsilon(n) n^2 dn$$

$$= \pi \int_0^{n_{max}} \epsilon(n) n^2 dn$$

$$= \pi \int_0^{n_{max}} \frac{\hbar^2 n^2}{8mL^2} n^2 dn$$

$$= \frac{\hbar^2 \pi}{8mL^2} \int_0^{n_{max}} n^4 dn$$

$$= \frac{\hbar^2 \pi}{8mL^2} \cdot \frac{1}{5} n_{max}^5 \Rightarrow U_{tot} = \frac{\hbar^2 \pi}{40mL^2} \cdot n_{max}^5$$

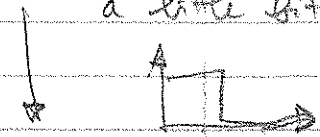
In terms of E_F : $\frac{h^2}{8\pi m k^2} n_{max}^2$, $n_{max} = \left(\frac{3N}{\pi}\right)^{1/3}$

$U_{tot} = \frac{\pi^2 E_F}{5} n_{max}^3$

temp-indep.

average energy, as expected, a little bit $> \frac{1}{2} E_F$

$U_{tot} = \frac{3}{5} N E_F$ at $T=0$



\bar{U} , average energy per particle ...

$\bar{U} = U_{tot}/N = \frac{3}{5} E_F$

IF $E_F \gg kT \rightarrow$ degenerate gas

Fermi Temperature \rightarrow temp. at which characteristic thermal energy = Fermi energy

$kT = E_F \Rightarrow T = \frac{E_F}{k}$ \rightarrow find T_F to set degenerate gas over there

Pressure of degenerate gas (due to Pauli's exclusion principle)

$dU = T dS - P dV + \mu dN$

$\left(\frac{dU}{dV}\right)_{S,N} = -P \Rightarrow P = -\left(\frac{\partial U}{\partial V}\right)_{S,N}$

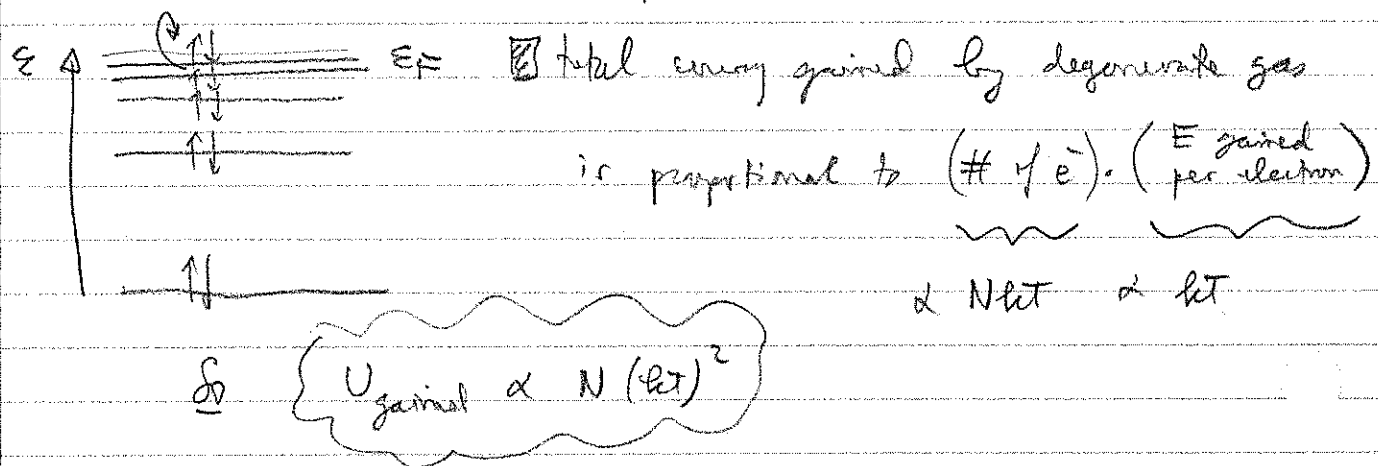
$P = -\frac{\partial}{\partial V} \left[\frac{3}{5} N \frac{h^2}{8\pi m} \left(\frac{3N}{\pi}\right)^{2/3} V^{-2/3} \right]$

$= \frac{3}{5} N \frac{h^2}{8\pi m} \left(\frac{3N}{\pi}\right)^{2/3} \cdot \left(\frac{-2}{3}\right) V^{-5/3}$ $\Rightarrow P = \frac{2}{5} \frac{N}{V} E_F$

In terms of $U_{tot} \Rightarrow$ $P = \frac{2}{3} \frac{U_{tot}}{V}$ \rightarrow $\frac{2}{3}$ of energy density of degenerate Fermi gas

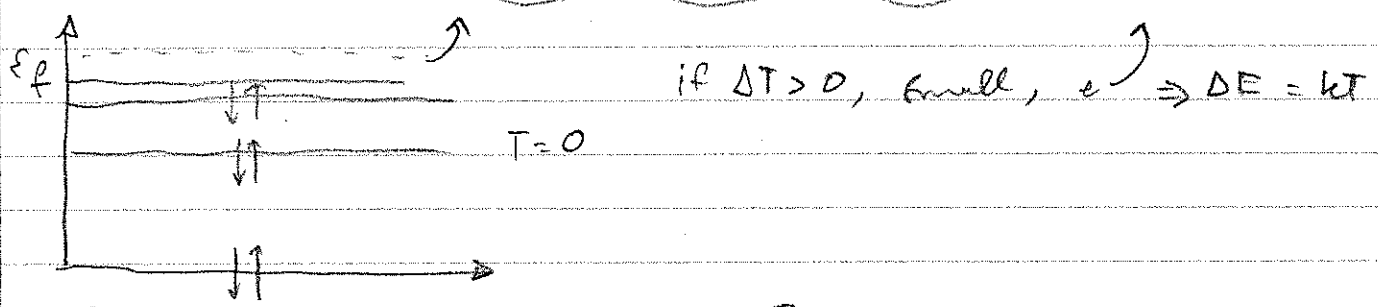
$P > 0 \rightarrow$ pushing outwards \rightarrow temperature-independent \rightarrow ex white dwarf stars prevent collapse due to gravity...

Consider small, non zero temp



May 6, 2019

Degenerate Fermi Gas at small non-zero temps



Energy gained by degenerate Fermi-gas $\propto N(kT)^2$

(# e that can jump) \times (energy gained)

$U_{gained} \sim N(kT)^2 \rightarrow$ when $\Delta T > 0$, small $(NkT) \sim (kT)$

↳, since $U_{\text{gained}} \propto N(kT)^2$

units of constants = $\left(\frac{1}{\text{energy}}\right)$

Guess $\Rightarrow \frac{1}{E_F}$

Additional constant of proportionality $\Rightarrow \frac{\pi^2}{4}$

$$U_{\text{gained}} = \frac{\pi^2}{4 E_F} N(kT)^2$$

↳

$$U_{\text{tot}} = U(t=0) + U(\Delta T)$$

$$U_{\text{tot}} = \frac{3}{5} N E_F + \frac{\pi^2}{4} \frac{N}{E_F} (kT)^2$$

→ crosses of degenerate gas...

↳ this true for any temperature...

$kT \ll E_F$

Heat capacity

↳ at constant volume $\rightarrow C_V = \left(\frac{\partial U}{\partial T}\right)_V$

$$C_V = \frac{\partial}{\partial T} \left(\frac{\pi^2}{4} \frac{N}{E_F} (kT)^2 \right)$$

$$C_V = \frac{\pi^2 N k^2 T}{2 E_F}$$

↳ as $T \rightarrow 0$, $C_V \rightarrow 0$, as expected...

↳ Note $C_V \propto T$ (linearly in temp)

Density of States

$$U = 2 \int_0^{n_{max}} n^2 \epsilon(n) dn \int_0^{\pi/2} d\phi \int_0^{\pi/2} \sin\theta d\theta$$

(↓↑)

$$U = \pi \int_0^{n_{max}} n^2 \epsilon(n) dn$$

integrating over all states...

What about integrating over all energies...

$$\epsilon = \frac{\hbar^2}{8mL^2} n^2 \Rightarrow n = \sqrt{\frac{8mL^2}{\hbar^2}} \sqrt{\epsilon}$$

$$\frac{dn}{dn} = \sqrt{\frac{8mL^2}{\hbar^2}} \frac{1}{2\sqrt{\epsilon}} d\epsilon \quad (n_{max} \sim \epsilon_F)$$

$$U = \pi \int_0^{\epsilon_F} \epsilon \left[\sqrt{\frac{8mL^2}{\hbar^2}} \frac{1}{2\sqrt{\epsilon}} \right] d\epsilon$$

$$U_{tot} = \pi \int_0^{\epsilon_F} \epsilon \left[\left(\frac{8mL^2}{\hbar^2} \right)^{1/2} \epsilon \left(\frac{8mL^2}{\hbar^2} \right)^{1/2} \frac{1}{2\sqrt{\epsilon}} \right] d\epsilon$$

Call Density of states

$$g(\epsilon) = \pi \left(\frac{8mL^2}{\hbar^2} \right)^{3/2} \cdot \frac{\sqrt{\epsilon}}{2} = \pi \left(\frac{8m}{\hbar^2} \right)^{3/2} \cdot \frac{V\sqrt{\epsilon}}{2\hbar^3}$$

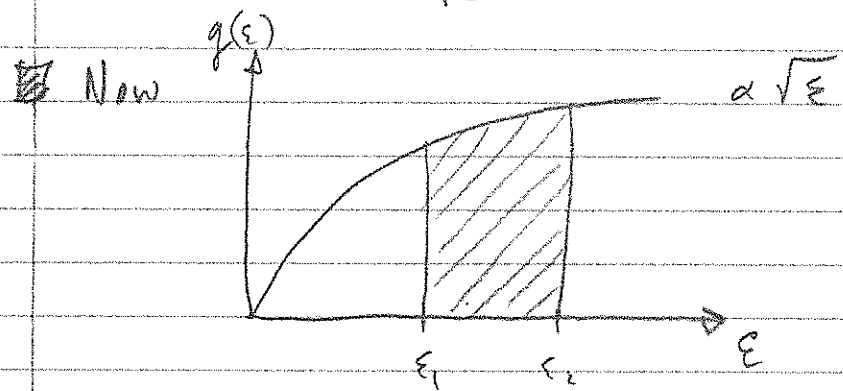
$g(\epsilon) \rightarrow$ probability density, or total # of states with energy ϵ

Now,
$$\epsilon_F = \frac{\hbar^2}{8m} \left(\frac{3N}{\pi V} \right)^{2/3}$$

$$g(\epsilon) = \frac{\pi (8m)^{3/2}}{\lambda h^3} V \sqrt{\epsilon}$$

So
$$g(\epsilon) = \frac{3N}{2\epsilon_F^{3/2}} \sqrt{\epsilon}$$

Note: $g(\epsilon) \propto V$, independent of N
 $\propto \sqrt{\epsilon}$



At $T=0$, then, all ϵ are below ϵ_F , then

$$\left\{ \begin{array}{l} P(\text{occupied} \mid \epsilon < \epsilon_F) = 1 \\ P(\text{occupied} \mid \epsilon > \epsilon_F) = 0 \end{array} \right\}$$

So
$$N(T=0) = \int_0^{\epsilon_F} g(\epsilon) d\epsilon$$

For non-zero temperature...

$$N(T=t) = \int_0^{\infty} g(\epsilon) \cdot P(\epsilon) d\epsilon$$

$\frac{-E/kT}{Z}$
 here Fermi-Dirac dist

$$N = \int_0^{\infty} g(\epsilon) P(\epsilon) d\epsilon$$

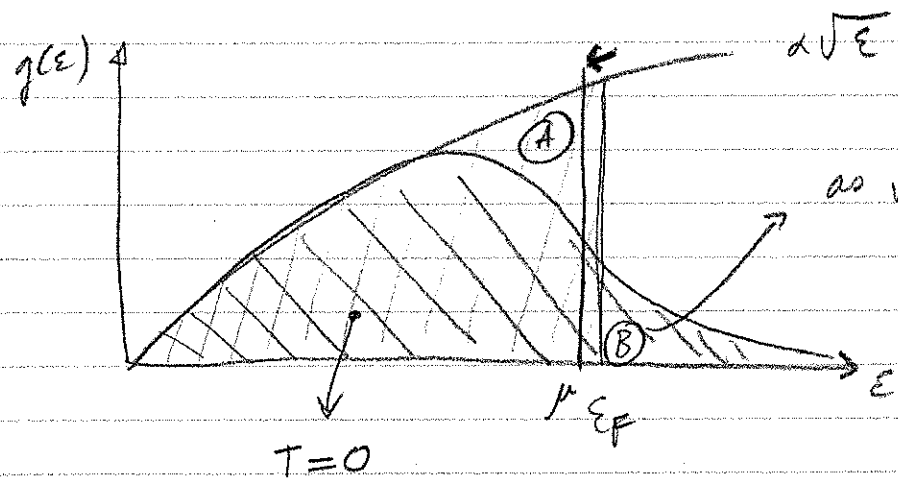
$$\bar{n}_{FP} = \frac{1}{e^{(\epsilon_F - \mu)/kT} + 1}$$

b

$$N = \int_0^{\infty} g(\epsilon) \frac{1}{e^{(\epsilon - \mu)/kT} + 1} d\epsilon$$

U_{tot} , total energy ... (..stuff)

$$U_{tot} = \int_0^{\infty} \epsilon g(\epsilon) \frac{1}{e^{(\epsilon - \mu)/kT} + 1} d\epsilon$$

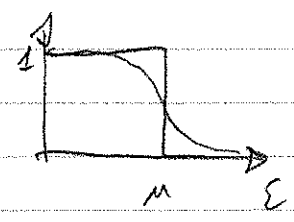


$$(Area A) = (Area B)$$

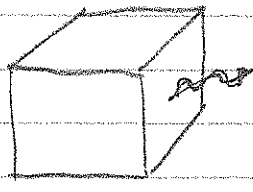
At $T=0$, $\epsilon_F = \mu$

At $T > 0$, μ decreases...

(concentration drops)



Black-body radiation



Finite box... definite energy wavefunctions

$$\lambda = \frac{2L}{n}$$

Each wave has frequency $\nu = \frac{c}{\lambda}$

Each wave has 2 dt

eq. partition

Average thermal energy = $2 \cdot \left(\frac{1}{2} kT\right) = kT$

Ultraviolet Catastrophe

→ too much radiation is predicted at short λ ...

Solution comes from QM → energy is quantized.

$$E_n = 0, h\nu, 2h\nu, 3h\nu, \dots$$

$$\begin{aligned} \text{Then } Z &= \sum_n e^{-E_n/kT} = 1 + e^{-E_1/kT} + (e^{-E_1/kT})^2 + \dots \\ &= \frac{1}{1 - e^{-\beta h\nu}} \end{aligned}$$

$$Z = \frac{1}{1 - e^{-\beta h\nu}} = \frac{e^{\beta h\nu}}{e^{\beta h\nu} - 1}$$

$$E = -\frac{1}{Z} \frac{\partial Z}{\partial \beta} = \frac{h\nu}{e^{h\nu/kT} - 1}$$

Energy comes in units of $h\nu = \epsilon$.

then average # of units = $\frac{\text{Avg. Energy}}{h\nu}$

$$\bar{n}_{PL} = \frac{\bar{E}}{h\nu} = \frac{1}{e^{+h\nu/kT} - 1}$$

Planck's distribution ...

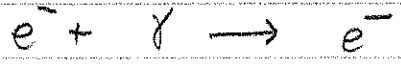
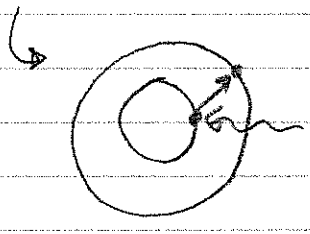
Planck ~~Not~~ NOT the same as Bose-Einstein dist where

$$\bar{n}_{BE} = \frac{1}{e^{(\epsilon - \mu)/kT} - 1}$$

So $\mu = 0$ for photons

γ not conserved ...

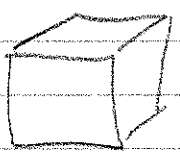
photons created + destroyed all the time



$$\mu_{e^-} + \mu_{\gamma} = \mu_{e^-} \quad \& \quad \mu_{\gamma} = 0$$

May 7, 2019

Blackbody Radiation



what is the total energy inside the box

Reminder Planck's distribution gives the average "occupancy" of an energy mode

$$\bar{n}_{PL} = \frac{1}{e^{\epsilon/kT} - 1}$$

Allowed wfn $\rightarrow \lambda = \frac{2L}{n}$, $p = \frac{h\lambda}{2L} \rightarrow$ allowed energies.?

Allowed energies, $\Rightarrow E=pc$, with $p_{\text{min}} = \frac{hcn}{2L}$ $E_n = \frac{hcn}{2L}$

In 3D, $E = cp = c \sqrt{p_x^2 + p_y^2 + p_z^2}$
 $= \frac{hc}{2L} \sqrt{n_x^2 + n_y^2 + n_z^2}$

Average energy per mode, \bar{E}_{mode}

$= E \times (\text{occupancy of mode}) =$

Planck's distribution, \bar{n}_{pl}

So, total energy $\Rightarrow \boxed{U = 2 \sum_{n_x} \sum_{n_y} \sum_{n_z} E_{\text{mode}} \cdot \bar{n}_{pl}(E)}$

2 independent polarization states for photons.

So, $\boxed{U = \sum_{n_x, n_y, n_z} \frac{hcn}{L} \cdot \frac{1}{e^{\frac{hcn}{2LkT}} - 1}}$

Convert this to an integral in spherical coordinates.

$U = \int_0^\infty n^2 \frac{hcn}{L} \frac{1}{e^{\frac{hcn}{2LkT}} - 1} dn \int_0^{\pi/2} d\phi \int_0^{\pi/2} \sin\theta d\theta$

$= \left(\frac{\pi}{2}\right) \cdot [\text{change of variable}] \rightarrow E = \frac{hcn}{2L} \Rightarrow n^2 = \frac{4E^2 L^2}{h^2 c^2}$

$dE = \frac{hc}{2L} dn$

$= \frac{\pi}{2} \int_0^\infty \frac{4L^2}{h^2 c^2} \cdot 2 \left(\frac{E}{2}\right) \cdot \frac{1}{e^{E/kT} - 1} \left(\frac{2L}{hc}\right) dE$

So,
$$U = \frac{8\pi L^3}{(hc)^3} \int_0^\infty \frac{\epsilon^3}{e^{\epsilon/kT} - 1} d\epsilon$$
 Call $L^3 = V$

then
$$\frac{U}{V} = \int_0^\infty \frac{8\pi}{(hc)^3} \frac{\epsilon^3}{e^{\epsilon/kT} - 1} d\epsilon$$
 \rightarrow total energy density (per unit volume)

energy density per unit photon energy

spectrum of photons \rightarrow called $u(\epsilon)$

spectrum

$$u(\epsilon) = \frac{8\pi}{(hc)^3} \frac{\epsilon^3}{e^{\epsilon/kT} - 1}$$

PLANCK'S SPECTRUM

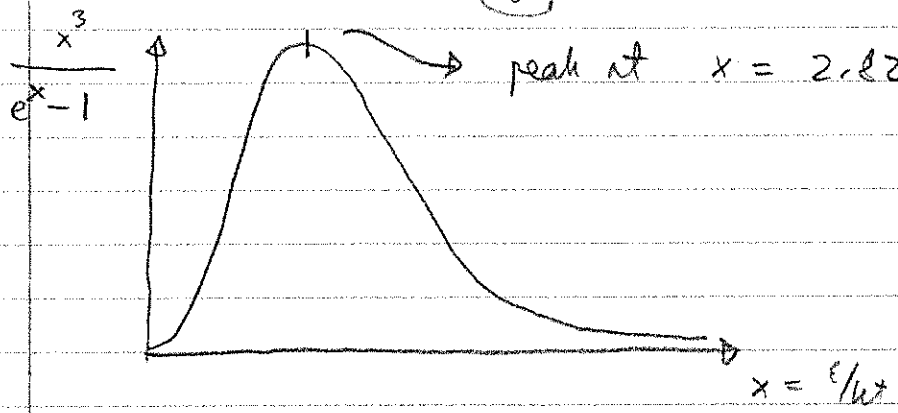
(correct when convert to λ since $d\epsilon \neq d\lambda \dots$)

Next, evaluate the integral...

$x = \epsilon/kT$, so $dx = \frac{1}{kT} d\epsilon$

$$\frac{U}{V} = \frac{8\pi}{(hc)^3} (kT)^4 \int_0^\infty \frac{x^3}{e^x - 1} dx$$

peak energy of spectrum of γ



$\epsilon = 2.82 kT$

(one version of Wien's law)

$\lambda = 2.9 \times 10^{-3} [m] / T [K]$

$$\int_0^{\infty} \frac{x^3}{e^x - 1} dx = \frac{\pi^4}{15} \quad (\text{Appendix B})$$

$$\frac{U}{V} = \frac{8\pi^5 (kT)^4}{15 (hc)^3} \rightarrow \text{electromagnetic energy density}$$

Entropy of Photon gas

First calculate heat capacity, C_v

$$C_v = \left(\frac{\partial U}{\partial T} \right)_V = 4aT^3 \quad \text{where } a = \frac{8\pi^5 k^4 V}{15 (hc)^3}$$

Entropy

$$S = \int_0^T \frac{C_v}{T'} dT' = \int_0^T 4a \frac{(T')^3}{T'} dT' = \int_0^T 4a(T')^2 dT' = \frac{4}{3} aT^3$$

$$S = \frac{32\pi^5}{45} V \left(\frac{kT}{hc} \right)^3 \cdot k \rightarrow \text{entropy of photon gas...}$$

Pressure of a photon gas...

$$dU = TdS - PdV + \mu dN$$

$$\rightarrow P = - \left(\frac{\partial U}{\partial V} \right)_{S, N} \rightarrow \text{need } U = U(V, S) \text{ if } S \text{ constant, } N = \text{constant...}$$

$$\frac{U}{V} = \frac{8\pi^5}{15 (hc)^3} (kT)^4 \quad \text{and} \quad S = \frac{32\pi^5}{45} \left(\frac{kT}{hc} \right)^3 k \cdot V$$

next to eliminate temperature ...

⊗ Let $\alpha = \frac{805 k^4}{15 (hc)^3}$, then $U = \alpha V T^4$, $S = \frac{4}{3} \alpha V T^3$

→ Solve for temperature... $T = \left(\frac{3S}{4}\right)^{1/3} \cdot (\alpha V)^{-1/3}$

S $U = (\alpha V) \left(\frac{3S}{4}\right)^{4/3} \cdot (\alpha V)^{-4/3}$

$U = \left(\frac{3S}{4}\right)^{4/3} \cdot (\alpha V)^{-1/3}$

P $P = - \left(\frac{\partial U}{\partial V}\right)_{S,N} = - \frac{\partial}{\partial V} \left[\left(\frac{3S}{4}\right)^{4/3} \cdot (\alpha V)^{-1/3} \right]_{S,N}$

$= \left(\frac{3S}{4}\right)^{4/3} \cdot \frac{1}{3} \alpha^{-1/3} V^{-4/3}$
 $= \frac{1}{3} \left(\frac{\partial}{\partial V} \left[\frac{4}{3} \alpha V T^3\right]\right)^{4/3} \alpha^{-1/3} V^{-4/3}$

P $P = \frac{1}{3} \alpha T^4$

or in terms of U/V ... ⇒ $P = \frac{1}{3} \frac{U}{V}$

Compare this pressure of Ideal gas... ↗ Monatomic

$PV = NkT$ & $U = \frac{f}{2} NkT = \frac{3}{2} NkT$

P $PV = \frac{2}{3} U$

so $P = \frac{2}{3} \frac{U}{V}$

Ex CMB - Cosmic Microwave Background radiation ...

$T = 2.73K$, Peak $\lambda = \frac{2.93 \times 10^{-3}}{2.73} \approx 1mm$

Total energy density in CMB ...

$$\frac{U}{V} = \frac{8\pi^5 (kT)^4}{15(hc)^3} = \boxed{0.26 \text{ MeV/m}^3}$$

Ordinary matter 1 proton/m³ → $\boxed{1 \text{ GeV/m}^3}$

→ photon density energy, pretty low...

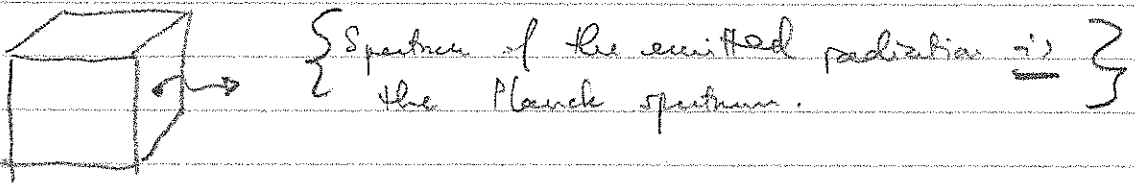
Entropy of CMB ⇒ $S = \frac{32\pi^5}{45} V \cdot \left(\frac{kT}{hc}\right)^3 k_B$

⇒ $\left| \frac{S}{V} \approx 2.89 \times 10^{23} \text{ K} \right|$ → much higher

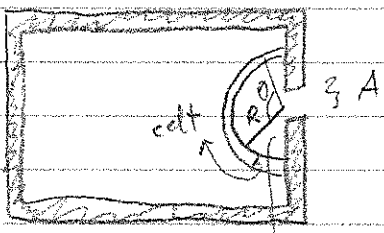
ordinary matter ... $\frac{S}{V} \sim Nk \sim k$

Nov 8, 2019

Radiation emitted by a Blackbody



How much energy escapes from hole?



Volume of chunk of radiation that could escape

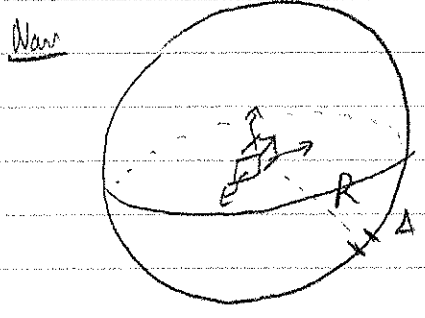
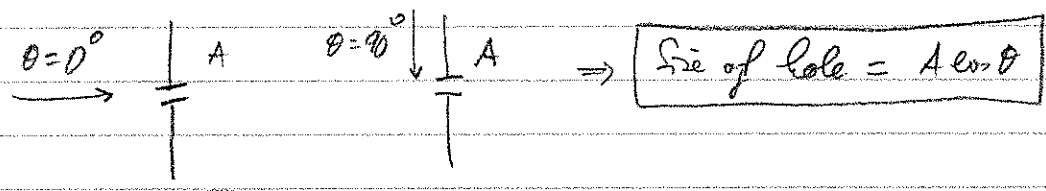
$= (Rd\theta)(R \sin\theta d\phi)(cdt)$

3D-chunk of radiation

Energy density = $\frac{u}{V} = \frac{8\pi^5 (kT)^4}{15 (hc)^3}$

$$\text{Total energy of black body} = \frac{8\pi^5 (kT)^4}{15 (hc)^3} R^2 c \sin\theta d\theta d\phi dt$$

Project hole size depend on angle of photon wrt hole...



probability of photon exiting hole } $\Rightarrow \frac{A \cos \theta}{4\pi R^2} = \frac{\text{hole size}}{\text{total area}}$

Energy that escapes hole

$$u = \frac{U}{V} \times R^2 c \sin\theta d\theta d\phi dt \cdot \frac{A \cos\theta}{4\pi R^2}$$

81

$$u_{\text{tot}} = \int_0^{\pi/2} d\phi \int_0^{\pi/2} d\theta \sin\theta \cos\theta \cdot \left(\frac{A}{4\pi}\right) \cdot c \left(\frac{u}{V}\right) dt$$

$$= \frac{2\pi \cdot A}{4\pi} \frac{u}{V} c dt \int_0^{\pi/2} \underbrace{\cos\theta \sin\theta d\theta}_{1/2}$$

$$u_{\text{tot}} = \frac{A}{4} \left(\frac{u}{V}\right) c dt$$

Energy per unit time gives power \rightarrow "luminosity"

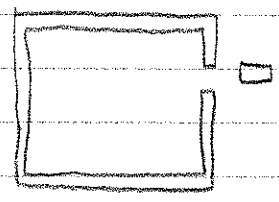
$$P = \frac{u_{\text{tot}}}{dt} \rightarrow \text{Flux} = \frac{\text{Power}}{\text{Area}} = \frac{u c}{4V}$$

B
$$\text{Flux} = \frac{c}{4} \left(\frac{u}{v} \right) = \frac{c}{4} \left(\frac{2\pi^5}{15} \right) \frac{(kT)^4}{(hc)^3} = \frac{2\pi^5}{15} \frac{(kT)^4}{h^3 c^2} = \sigma T^4$$

$$\sigma = \frac{2\pi^5 k^4}{15 h^3 c^2} = 5.67 \times 10^{-8} \text{ W/m}^2 \text{K}^4$$

Stefan-Boltzmann Constant } Stefan-Boltzmann Law

Why is this blackbody radiation?



What if our object is not black?
 Some λ are reflected rather than absorbed

Define Emissivity, e

e = amount of radiation absorbed

If $e=1 \rightarrow$ blackbody
 If $e=0 \Rightarrow$ perfect reflector

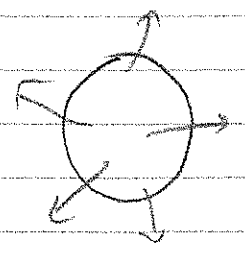
Note e is λ -dependent.

B
$$\frac{\text{Power}}{\text{Area}} = \text{Flux} = \sigma e T^4$$

$$\text{Power} = \sigma e A T^4 \rightarrow \text{luminosity}$$

Example Sun assume $e=1$

Since luminosity = $\frac{\text{Power}}{1} \Rightarrow L_0 = 3.2 \times 10^{26} \text{ W}$



$A = 4\pi R_{\odot}^2$, $F_{\text{at surface}} = \frac{L}{A} = \frac{L}{4\pi R_{\odot}^2} = F_{\odot} = \epsilon\sigma T^4$

So $T = \sqrt[4]{\frac{L}{4\pi R_{\odot}^2 \epsilon\sigma}} = \sqrt[4]{\frac{L}{4\pi R_{\odot}^2 \sigma}} \approx \boxed{5800\text{K}}$

Can do the Wein's law

$\lambda_{\text{peak}} = \frac{2.9 \times 10^{-3}}{T} \rightarrow \text{set } T \rightarrow \text{set } R \dots$

Can do the same thing for the Earth...

May 10, 2014

BOSE - EINSTEIN CONDENSATES

Now, dealing with ordinary bosons $\mu \neq 0$, $\mu = \mu(T, P)$

Phenomenon \Rightarrow a gas of bosons will abruptly "condense" into the ground state energy as T goes below critical value.

1st order under $T \rightarrow 0$ Every boson in ground state

$\epsilon_0 = \frac{h^2}{8\pi m^2 L^2} (1^2 + 1^2 + 1^2) = \frac{3h^2}{8\pi m L^2}$

Avg # of atoms, in ground state at temp T

$N_0 = \pi_{BE} = \frac{1}{e^{(\epsilon_0 - \mu)/kT} - 1}$ At low T , $N_0 \rightarrow$ large

$\frac{e^{(\epsilon_0 - \mu)/kT} - 1}{\text{close to } 1} \rightarrow$ small # hence $\frac{\epsilon_0 - \mu}{kT} \ll 1$

Now, $e^x \approx 1+x$

So $N_0 \approx \frac{1}{1 + \frac{E_0 - \mu}{kT}} \approx \frac{kT}{E_0 - \mu} \rightarrow$ large # at low T

at $T=0$, $\mu = E_0$

at $T > 0$, $\mu < E_0$ to keep $N_0 \approx$ constant

How low does T need to be for N_0 to be large?

$N_{tot} = \sum_i \frac{1}{e^{(E_i - \mu)/kT} - 1}$. If $kT \gg E_0$, convert sum to integral

$N_{tot} = \int_0^\infty g(E) \frac{1}{e^{(E - \mu)/kT} - 1} dE$

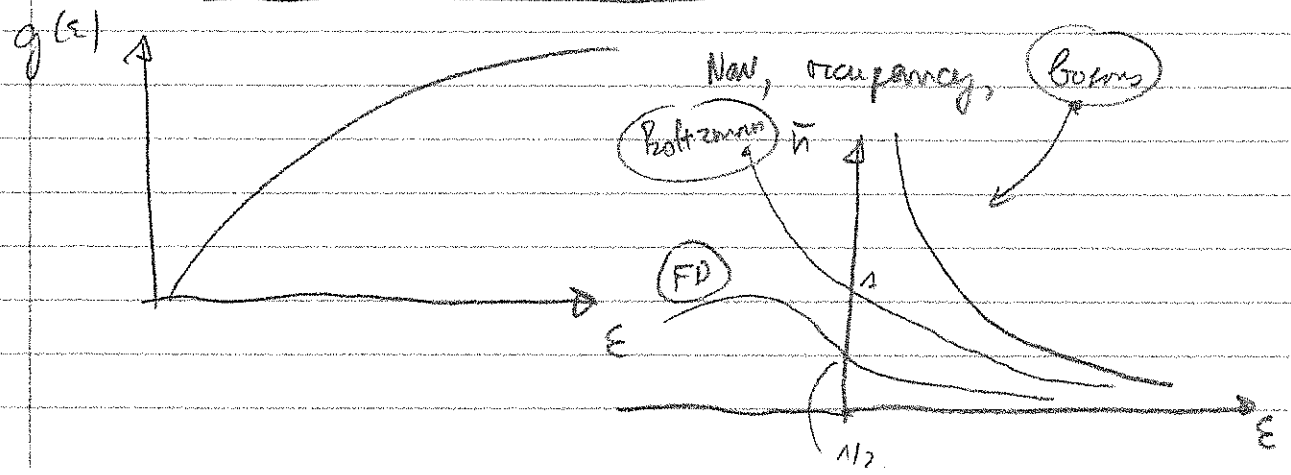
density of states - multiplicity

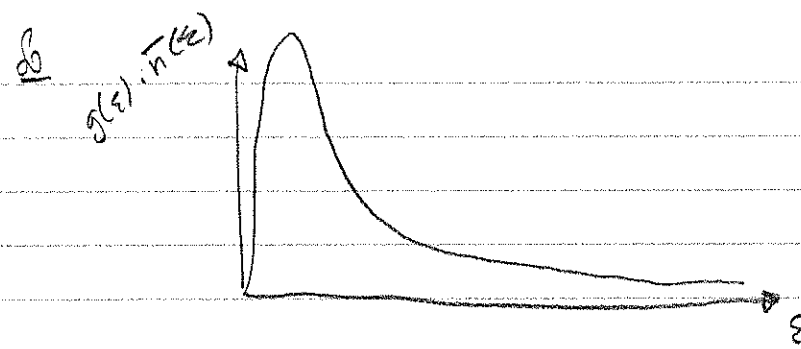
For fermions

$g(E) = \frac{\pi (2m)^{3/2}}{2h^3} V \sqrt{E}$ (fermions)

For bosons, divide by 2 (since there's only one spin)

So $g(E) = \frac{2}{\sqrt{\pi}} \left(\frac{2\pi m}{h^2} \right)^{3/2} \cdot V \sqrt{E}$ density of states for bosons





Total # of particles ...

$$N_{tot} = \int_0^{\infty} g(\epsilon) \frac{1}{e^{(\epsilon-\mu)/kT} - 1} d\epsilon$$

guess values for μ . 1st guess $\mu = 0$

$$N_{tot} = \int_0^{\infty} \frac{2}{\sqrt{\pi}} \left(\frac{2\pi m}{h^2} \right)^{3/2} V \sqrt{\epsilon} \frac{1}{e^{\epsilon/kT} - 1} d\epsilon$$

$$= \frac{2}{\sqrt{\pi}} \left(\frac{2\pi m}{h^2} \right)^{3/2} V \int_0^{\infty} \sqrt{\epsilon} \frac{1}{e^{\epsilon/kT} - 1} d\epsilon$$

change of variable $\Rightarrow x = \frac{\epsilon}{kT}$, $dx = \frac{1}{kT} d\epsilon$

$$N_{tot} = \frac{2}{\sqrt{\pi}} \left(\frac{2\pi m kT}{h^2} \right)^{3/2} V \int_0^{\infty} \frac{\sqrt{x}}{e^x - 1} dx$$

(2-315)

$$N_{tot} = (2.612) \left[\frac{2\pi m kT}{h^2} \right]^{3/2} \cdot V$$

but if $T^T, N^T \rightarrow$ wrong ...

At $T = T_c \rightarrow$ condensation temperature, this is true

$$N_{tot} = (2.612) \left[\frac{2\pi m kT_c}{h^2} \right]^{3/2} \cdot V$$

$$\lambda \quad \lambda T_c = 0.527 \left(\frac{h^2}{2m\pi} \right) \left(\frac{N}{V} \right)^{2/3} \rightarrow \text{(density)}$$

At high temperatures, i.e., $(T > T_c)$

expect very few bosons in the ground state...

$$\hookrightarrow \text{large } e^{(\epsilon_0 - \mu)/kT} \rightarrow \text{large } \frac{\epsilon_0 - \mu}{kT} \rightarrow \text{wood } \mu < 0$$

At low T, $(T < T_c)$

$\lambda T \gg \lambda T_c$, i.e. $\lambda T \gg \lambda T_c \rightarrow$ can convert the sum to an integral

is, just consider excited states where $\lambda T \gg \lambda T_c \rightarrow$ have integral again.

$$\lambda, \quad \# \text{ excited} = (2.612) \left(\frac{2\pi m k T}{h^2} \right)^{3/2} \cdot V$$

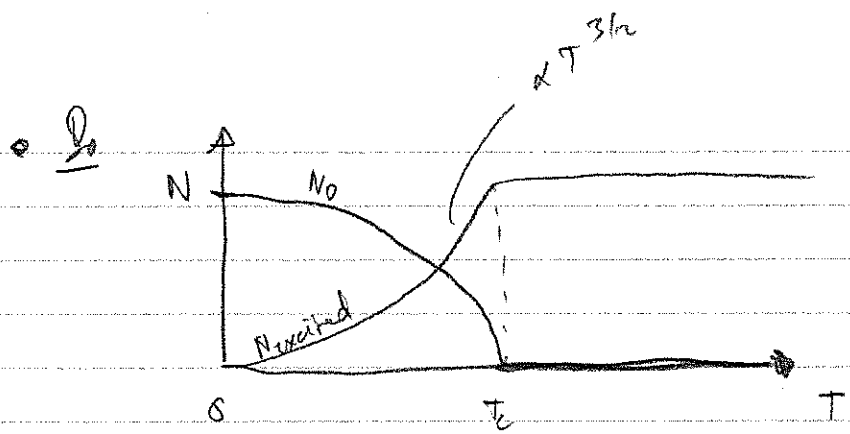
$$\text{And } N_{\text{tot}} = (2.612) \left(\frac{2\pi m k T_c}{h^2} \right)^{3/2} \cdot V$$

$$\text{And so } \left\{ N_{\text{excited}} = N_{\text{tot}} \left(\frac{T}{T_c} \right)^{3/2} \right.$$

low temp
↓
* $T < T_c$

→ the rest must be in the ground state... \nearrow low temp...

$$N_0 = N_{\text{ground}} = N_{\text{tot}} - N_{\text{excited}} = \left[1 - \left(\frac{T}{T_c} \right)^{3/2} \right] N_{\text{tot}}$$



T_c is approximately when $\frac{V}{N} \approx V_0$

$$\left(\frac{2\pi m k T_c}{h^2} \right)^{3/2} \dots$$

u

THE END